

Preliminary Storm Water Management Plan



May 27, 2022

Property Owner:

Consultant to Project Owner:

PI NEER engineering P.A.

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I hereby certify that this Specification, plan, or report was prepared by me or under my direct supervision and that I am a duly Registered Professional Engineer under the laws of the State of Minnesota.

John M. Molinaro Minn. Reg. No. 45831

Date: <u>5-27-2022</u>

I. Introduction

The following is a hydrology summary for the construction of a 80 unit single family home development to be called Creekside. The site is located east of Clementa Ave. SW at the end of Cole Avenue on the north and 7th St. N on the east boundary, in Montrose, Minnesota.

II. Existing Site Conditions

A. Current Land Use

The site consists of a 40 acre parcel of land. The site is generally divided into two areas, the western and eastern side of the creek that is a public water. The western portion is approximately 25 acres and consists of a large rolling field that was used as agricultural land for crops. The remainder of the western portion is a significant area of woods that located mostly along the creek and the southern portion of the land, there are a couple wetlands located on the western side of the creek. The eastern portion is approximately 15 acres with the majority of the upland land covered in woods, a small portion of the woods have been cleared adjacent to the eastern property boundary. There are a couple wetlands located on the eastern side of the creek.

B. Topography - Existing Hydrology

The existing topography is generally rolling with the majority of the upland areas draining to the creek. A small portion of the western area drains offsite to the west. A small portion of the eastern area drains to a wetland located on the south. All of the drainage makes it to the creek through offsite wetlands and overflows.

The Surface Waters & Wetland Areas that receive stormwater within one mile are shown in the Drainage Maps in APPENDIX A.

C. Special or Impaired Waters

A special and impaired waters search was completed using the MPCA search engine (<u>http://pca-gis02.pca.state.mn.us/CSW/index.html</u>) on November 18, 2021. The project has no discharge point within one mile of, and flows to, a special water listed in Appendix A, Part B of the NPDES Construction Site General Permit. The project does not have a discharge point within one mile of, and flows to, a water listed as impaired under Section 303(D) of the Federal Clean Water Act.

Waterbody ID	NA	-
Name of Waterbody	-	
Туре	Туре	
Special Water	No	
Impaired Water	No	
Pollutants	-	
Approved TMDL	-	
Site Discharges to	-	

D. Soils

If a geotechnical report should be available shortly, (5-20-2022).

A review of the USDA Natural Resources Conservation Services Soils Survey Map (See Appendix H) indicated the following soils on site:

Soil Symbol	Soil Name	% of Site	Hydrologic Soil Group	Kf	T factor	Repres	sentative	value	Erosion Potential
			-			% Sand	% Silt	% Clay	
106C2	Lester loam, 6 to 10 percent slopes, moderately eroded								
	Lester, moderately eroded	10.0	С	0.32	5	39	37	24	Not Rated
106D2	Lester loam, 10 to 16 percent slopes, moderately eroded								
	Lester, moderately eroded	0.7	С	0.32	5	39	37	24	Not Rated
109	Cordova clay loam, 0 to 2 percent slopes								
	Cordova	29.3	C/D	0.28	5	34.2	37.8	28	Not Rated
539	Klossner muck, 0 to 1 percent slopes								
	Klossner, drained	0.9	C/D		1				Not Rated
1080	Klossner, Okoboji and Glencoe soils, ponded, 0 to 1 percent slopes								
	Klossner, ponded	6.6	C/D		1				Not Rated
	Okoboji, ponded	6.6	C/D	0.32	5	11	53	36	Not Rated
	Glencoe, ponded	6.6	C/D	0.28	5	22	45	33	Not Rated
1362B	Angus loam, 2 to 6 percent slopes								
	Angus	6.7	С	0.28	5	39	37	24	Not Rated
1901B	Angus-Le Sueur complex, 1 to 6 percent slopes								
	Angus	45.8	С	0.28	5	39	37	24	Not Rated
	Le Sueur	45.8	C/D	0.28	5	39	37	24	Not Rated
	1	I		1	1		1		

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

III. Proposed Site Conditions & Design Considerations

A. Proposed Development

The proposed development consists of an 80-unit single family home between Cole Ave. on the northwest and 7th Street North on the east. The general internal layout is a through street that is a collector located along the extension of 7th Street N from east to west. There is also a collector street connection on Cole Ave connected to the new 7th St. N. There is a cul-de-sac located on the easterly portion and a street connection to the land lying to the south. On the western side of the creek there is a large looped street with a cul-de-sac utilizing the interior land. There is also a small cul-de-sac located on the southern portion of the property.

The table below provides information on the estimated acreage of land cover before and after project development.

Cover Types	Before Acres	After Acres	CN Value
Types 1-8 wetlands	4.11	4.04	80
Wooded/forest	17.62	4.86	79
Cropland	18.48	-	89
Brush/grassland	-	-	-
Lawn/landscaping	-	19.69	80
Impervious surfaces *	-	11.63	98
Pond	-	-	-
TOTAL **	40.22	40.22	

B. Proposed Topography

The proposed drainage patterns will be reflective of the existing drainage patterns when possible. The drainage maps are shown in Appendix A.

C. Design Requirements

The City of Montrose Stormwater Management Ordinance requires all new developments to meet quality, flow rate requirements as denoted by the City Code. The City of Montrose also required that the Stormwater Management Plan meets or exceeds the requirements of the MN MPCA NPDES permit. These requirements are summarized as follows:

1. Rate Control

Montrose: 2 year: Must not increase from Existing 10 year: Must not increase from Existing 100 year: Must not increase from Existing

2. Water Quality

To meet the NPDES Construction Stormwater Permit the permanent sedimentation basins must:

- The basin must have a permanent volume of 1800 cubic feet of storage below the outlet pipe for each acre that drains to the basin.
- The basin must be designed to provide live storage for a water quality volume (calculated as an instantaneous volume) of one (1) inch of runoff from the new impervious surfaces created by the project.
- Basin outlets shall be designed such that the water quality volume is discharged at no more than 5.66 cubic feet per second (cfs) per acre of surface area of the pond. The basin's water quality volume is calculated as 1 inch of runoff from the new impervious surfaces created by the project.

3. Volume Control

To meet the NPDES Construction Stormwater Permit the infiltration systems must:

- Be design so that the water quality volume of one (1) inch of runoff from the new impervious surfaces created by the project is retained on site (i.e. infiltration or other volume reduction practices) and not discharged to a Surface Water.
- Discharge the water quality volume routed to the system through the soil surface or filter media within 48 hours or less.
- Verify soil type and to ensure a minimum of three (3) feet of separation from the seasonally saturated soils (or from bedrock) and the bottom of the proposed infiltration/filtration system.

4. Storm Sewer Design

The storm sewer must be designed to handle a 10 Year Storm Event.

5. Pad Elevations

Montrose Low Opening Elevations are to be designed to the following standards:

Low opening elevations shall be at least:

2' Above E.O.F. of adjacent ponds.

3' Above the OHW or Highest Known water level (whichever is greater) for the Public Waters of the State.

3' Above 100-yr HWL of adjacent ponds or wetlands.

D. Proposed Hydrology

Three retention basins are proposed to collect site runoff from a majority of the improved areas of the development. There are no offsite flows that will enter the stormwater treatment system. The basins are all designed as wet sedimentation basins with no infiltration BMP's. This is due to the underlying soil type being classified as Type D soils. These basins will be constructed with the initial phases of grading and operate as temporary ponding locations. The small areas that are not collected by the onsite stormwater treatment system discharge to the existing locations. The non-treated areas are rear yards of lots with the corresponding non-connected impervious areas of the structures.

Basin Sun	Basin Summary				
Basin Model Name (HydroCAD)	100P	200P	300P		
Basin Description	Pond #1	Pond #2	Pond #3		
NWL – Outlet Elevation	961.0	962.0	966.0		
100-Year HWL	964.5	964.1	967.7		
Emergency Overflow	965.0	964.6	969.0		
Top of Berm	965.5	964.6	970.0		
Surface Area at NWL (ac)	0.545	0.480	0.160		
	0.85'	1.0'	0.75'		
Structural Outlet	Weir	Weir	Weir		
Wet Volume (af)	2.752	1.681	0.317		
Live Volume (af) @ 100-Year	2.178	1.115	0.321		
Drainage Area (ac)	16.49	4.64	1.89		
Impervious Area (ac)	7.19	1.93	0.93		
Lowest Floor Elevation	-	-	_		
Lowest Opening Elevation	967.5	967.1	970.7		

The majority of onsite soils have very low infiltration rates. These low rates are not favorable to infiltration BMPs.

IV. Results

1. Rate Control

The proposed flow rate from the proposed development shall not exceed the flow rate of the existing drainage areas for the two, ten and 100-year storm events.

The following table is a summary of the results of the flow rate derived by the HydroCAD models.

Drainage Drainage		2-Year Flow Rate (cfs)		10-Year Flow Rate (cfs)		100-Year Flow Rate (cfs)	
Designation	Description	Existing	Proposed	Existing	Proposed	Existing	Proposed
West	Drainage to West Boundary	19.75	9.85	34.59	18.16	70.08	38.54
Creek	Drainage to Creek	53.17	27.36	98.97	66.46	211.64	133.87
South	Drainage to South Wetland	14.74	10.85	26.28	20.78	54.14	45.56

2. Water Quality

The basin must have a permanent volume of 1800 cubic feet of storage below the outlet pipe for each acre that drains to the basin.

NPDES Basin Treatment Volume				
Basin Model Name (HydroCAD)	Drainage Area (acre)	Requirement (cf/acre)	Treatment Volume Req. (ac*ft)	Volume Proposed (ac*ft)
100P	16.49	1800	0.681	2.752
200P	4.64	1800	0.192	1.681
300P	1.89	1800	0.078	0.317

Basin outlets shall be designed such that the water quality volume is discharged at no more than 5.66 cubic feet per second (cfs) per acre of surface area of the pond. The basin's water quality volume is calculated as $\underline{1}$ inch of runoff from the new impervious surfaces created by the project.

NPDES Basin Water Quality Volume Discharge Requirement				
Basin Model Name (HydroCAD)	Surface area (acre)	WQ Discharge (cfs)	Discharge per acre (cfs/acre)	
100P	0.545	3.00	5.50	
200P	0.480	0.62	1.29	
300P	0.160	0.77	4.81	

The basin must be designed to provide live storage for a water quality volume (calculated as an instantaneous volume) of one (1) inch of runoff from the new impervious surfaces created by the project.

Basin Live Storage Requirement					
Basin Model Name	New Imp. Surface Area (acre)	Live Storage Required (1.0")	NWL / HWL Elev.	Water Quality Volume Proposed (ac*ft)	
100P	7.19	0.599	961/964.5	2.178	
200P	4.64	0.161	962/964.1	1.115	
300P	1.89	0.077	966/967.7	0.321	

3. Volume Control

To meet the NPDES Permit the project must be design so that the water quality volume of one (1) inch of runoff from the new impervious surfaces created by the project is retained on site (i.e. infiltration or other volume reduction practices) and not discharged to a Surface Water.

Due to Type D soils Infiltration is not possible per MN NPDES (16.18).

Runoff Quantity Reduction Required				
Total New		Water Quality		
Impervious Area	Treatment Depth	Volume		
(ac)	(in/ac impervious)	(ac*ft)		
-	-	-		

	Int	Infiltration Basin Volume Provided				
Basin Name	Captured Volume Below Outlet (ac*ft)	Surface area (sf)	Infiltration Rate (in/hr)	Draw Down Time (hr)	Volume (ac*ft)	
-		-	-	-	-	
Total					-	

Appendix A: Hydrology Maps







Appendix B: Hydrology Calculations



121139-Creekside 5-27-2022-Existing

00-121186-PROPOSED- 05-26-22

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Event# Event Storm Type Curve Mode Duration B/B Depth AMC Name (inches) (hours) 1-yr MSE 24-hr 3 Default 24.00 1 2.46 2 1 2 2-yr MSE 24-hr 3 Default 24.00 1 2.81 2 3 10-yr MSE 24-hr 3 Default 24.00 1 4.19 2 4 100-yr MSE 24-hr 24.00 1 7.47 2 3 Default

Rainfall Events Listing

121139-Creekside 5-27-2022-Existing

00-121186-PROPOSED- 05-26-22

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Area Listing (selected nodes)

40.216	85	TOTAL AREA
17.625	79	Woods, Fair, HSG D (AS, BS, CS)
22.591	89	Row crops, straight row, Good, HSG D (AS, BS, CS)
(acres)		(subcatchment-numbers)
Area	CN	Description

00-121186-PROPOSED- 05-26-22

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Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
40.216	HSG D	AS, BS, CS
0.000	Other	
40.216		TOTAL AREA

121139-Creekside 5-27-2022-Existing

00-121186-PROPOSED- 05-26-22

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				•		,	
HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.000	0.000	22.591	0.000	22.591	Row crops, straight row, Good	AS, BS, CS
0.000	0.000	0.000	17.625	0.000	17.625	Woods, Fair	AS, BS, CS
0.000	0.000	0.000	40.216	0.000	40.216	TOTAL AREA	

Ground Covers (selected nodes)

		1211	39-Creekside	• 5-27-2022-	Existing
00-121186-PROPOSED- 05-26-22		M	ISE 24-hr 3	1-yr Rainfa	ll=2.46"
Prepared by {enter your company name	here}			Printed 6/	21/2022
HydroCAD® 10.10-7a s/n 00590 © 2021 Hydr	oCAD Software So	lutions LLC			Page 6
Time span=0.00-16 Runoff by SCS TF Reach routing by Sim-Route	60.00 hrs, dt=0.00 R-20 method, UH e method - Pond	01 hrs, 1600 =SCS, Weigl Frouting by S	01 points hted-CN Sim-Route me	thod	•
Subcatchment AS: West Catchment Flow Length=200	Runoff Area=27 Slope=0.0700 '/'	1,108 sf 0.0 Tc=2.7 min	0% Impervious CN=86 Rund	Runoff Dep off=16.09 cfs	oth=1.21" 0.628 af
Subcatchment BS: Central Catchment Flow Length=850'	Runoff Area=1,26 Slope=0.0310 '/'	6,338 sf 0.0 Tc=13.9 min	0% Impervious CN=84 Rund	Runoff Dep off=42.16 cfs	oth=1.09" 2.629 af
Subcatchment CS: South Catchment Flow Length=220	Runoff Area=21 Slope=0.0640 '/'	4,369 sf 0.0 Tc=3.2 min	0% Impervious CN=85 Rund	Runoff Dep off=11.91 cfs	oth=1.15" 0.470 af
Link E-Creek: Existing Creek			Inflo Prima	w=42.16 cfs ry=42.16 cfs	2.629 af 2.629 af
Link E-South: Existing South			Inflo Prima	ow=11.91 cfs ry=11.91 cfs	0.470 af 0.470 af
Link E-West: Existing West			Inflc Prima	ow=16.09 cfs ry=16.09 cfs	0.628 af 0.628 af

Total Runoff Area = 40.216 acRunoff Volume = 3.727 af
100.00% Pervious = 40.216 acAverage Runoff Depth = 1.11"
0.00% Impervious = 0.000 ac

Summary for Subcatchment AS: West Catchment

Runoff = 16.09 cfs @ 12.11 hrs, Volume= 0.628 af, Depth= 1.21" Routed to Link E-West : Existing West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

Area (sf)	CN	Description		
188,355	89	Row crops,	straight rov	w, Good, HSG D
82,753	79	Woods, Fai	r, HSG D	
271,108	86	Weighted A	verage	
271,108		100.00% Pe	ervious Are	a
Tc Lengtl	n Slop	e Velocity	Capacity	Description
(min) (feet	:) (ft/f	t) (ft/sec)	(cfs)	
2.7 200	0.070	0 1.23		Lag/CN Method,

Subcatchment AS: West Catchment



Summary for Subcatchment BS: Central Catchment

Runoff = 42.16 cfs @ 12.22 hrs, Volume= 2.629 af, Depth= 1.09" Routed to Link E-Creek : Existing Creek

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

CN	Description			
89	Row crops,	straight rov	w, Good, HSG D	
79	Woods, Fai	r, HSG D		
84	Weighted A	verage		
	100.00% Pervious Area			
Slope	Velocity	Capacity	Description	
(ft/ft)	(ft/sec)	(cfs)		
0.0310	1.02		Lag/CN Method,	
	CN 89 79 84 Slope (ft/ft) 0.0310	CNDescription89Row crops,79Woods, Fai84Weighted A100.00% PeSlopeVelocity(ft/ft)(ft/sec)0.03101.02	CNDescription89Row crops, straight rov79Woods, Fair, HSG D84Weighted Average 100.00% Pervious AreSlopeVelocityCapacity (ft/ft)(ft/sec)0.03101.02	

Subcatchment BS: Central Catchment



Summary for Subcatchment CS: South Catchment

Runoff = 11.91 cfs @ 12.11 hrs, Volume= 0.470 af, Depth= 1.15" Routed to Link E-South : Existing South

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

Area	ı (sf)	CN	Description				
131,	,049	89	Row crops,	straight rov	w, Good, HSG D		
83,	,320	79	Woods, Fai	r, HSG D			
214,	,369	85	Weighted A	verage			
214,	,369		100.00% Pervious Area				
Tc Le	ength	Slope	e Velocity	Capacity	Description		
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)			
3.2	220	0.0640) 1.16		Lag/CN Method,		

Subcatchment CS: South Catchment



Summary for Link E-Creek: Existing Creek

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Inflow A	rea =	:	29.071 ac,	0.00% Impervi	ious, Inflow D	0epth = 1.09	" for 1-yr event	
Inflow	=		42.16 cfs @	12.22 hrs, Vo	olume=	2.629 af		
Primary	=		42.16 cfs @	12.22 hrs, Vo	olume=	2.629 af, <i>A</i>	Atten= 0%, Lag= 0.1 mir	ו

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs

Link E-Creek: Existing Creek



Summary for Link E-South: Existing South

Inflow /	Area	=	4.921 ac,	0.00% Impervious	s, Inflow Depth =	1.15"	for 1-yr	event
Inflow		=	11.91 cfs @	12.11 hrs, Volum	ne= 0.470) af		
Primary	у	=	11.91 cfs @	12.11 hrs, Volum	ne= 0.470) af, At	ten= 0%, I	∟ag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link E-South: Existing South

Summary for Link E-West: Existing West

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Inflow /	Area	=	6.224 ac,	0.00% Impervious	, Inflow Depth = 1	.21" for 1-yr event
Inflow		=	16.09 cfs @	12.11 hrs, Volum	e= 0.628 at	f
Primary	у	=	16.09 cfs @	12.11 hrs, Volum	e= 0.628 at	f, Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link E-West: Existing West

		121139-C	reekside 5-27-2022-Existing
00-121186-PROPOSED- 05-26-22		MSE 2	24-hr 3 2-yr Rainfall=2.81"
Prepared by {enter your company name	here}		Printed 6/21/2022
HydroCAD® 10.10-7a s/n 00590 © 2021 Hydro	oCAD Software Solu	utions LLC	Page 13
Time span=0.00-16 Runoff by SCS TF Reach routing by Sim-Route SubcatchmentAS: West Catchment Flow Length=200'	60.00 hrs, dt=0.001 R-20 method, UH=8 method - Pond r Runoff Area=271 Slope=0.0700 '/'	1 hrs, 160001 pc SCS, Weighted- routing by Sim-R ,108 sf 0.00% In Tc=2.7 min CN=	ints CN oute method npervious Runoff Depth=1.50" 86 Runoff=19.75 cfs 0.778 af
Subcatchment BS: Central Catchment Flow Length=850'	Runoff Area=1,266 Slope=0.0310 '/' T	i,338 sf 0.00% Im ic=13.9 min CN=	npervious Runoff Depth=1.36" 84 Runoff=53.17 cfs 3.298 af
Subcatchment CS: South Catchment Flow Length=220'	Runoff Area=214 Slope=0.0640 '/'	,369 sf 0.00% In Tc=3.2 min CN=	npervious Runoff Depth=1.43" 85 Runoff=14.74 cfs 0.586 af
Link E-Creek: Existing Creek			Inflow=53.17 cfs 3.298 af Primary=53.17 cfs 3.298 af
Link E-South: Existing South			Inflow=14.74 cfs 0.586 af Primary=14.74 cfs 0.586 af
Link E-West: Existing West			Inflow=19.75 cfs 0.778 af Primary=19.75 cfs 0.778 af

Total Runoff Area = 40.216 acRunoff Volume = 4.663 af
100.00% Pervious = 40.216 acAverage Runoff Depth = 1.39"
0.00% Impervious = 0.000 ac

Summary for Subcatchment AS: West Catchment

Runoff = 19.75 cfs @ 12.11 hrs, Volume= 0.778 af, Depth= 1.50" Routed to Link E-West : Existing West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

Area (s	sf)	CN	Description				
188,35	55	89	Row crops,	straight rov	w, Good, HSG D		
82,75	53	79	Woods, Fai	r, HSG D			
271,10)8	86	Weighted A	verage			
271,10)8		100.00% Pervious Area				
Tc Leng	gth	Slope	Velocity	Capacity	Description		
(min) (fe	et)	(ft/ft)	(ft/sec)	(cfs)			
2.7 2	200	0.0700	1.23		Lag/CN Method,		

Subcatchment AS: West Catchment



Summary for Subcatchment BS: Central Catchment

Runoff = 53.17 cfs @ 12.22 hrs, Volume= 3.298 af, Depth= 1.36" Routed to Link E-Creek : Existing Creek

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

Area (sf)	CN	Description		
664,670	89	Row crops,	straight rov	w, Good, HSG D
601,668	79	Woods, Fai	r, HSG D	
1,266,338	84	Weighted A	verage	
1,266,338		100.00% Pe	ervious Are	a
Tc Length	Slope	e Velocity	Capacity	Description
(min) (feet)	(ft/ft)) (ft/sec)	(cfs)	
13.9 850	0.0310	1.02		Lag/CN Method,

Subcatchment BS: Central Catchment



Summary for Subcatchment CS: South Catchment

Runoff = 14.74 cfs @ 12.11 hrs, Volume= 0.586 af, Depth= 1.43" Routed to Link E-South : Existing South

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

Area (sf)	CN	Description		
131,04	49	89	Row crops,	straight rov	w, Good, HSG D
83,32	20	79	Woods, Fai	r, HSG D	
214,3	69	85	Weighted A	verage	
214,3	69		100.00% Pe	ervious Are	a
Tc Len	gth	Slope	Velocity	Capacity	Description
(min) (fe	eet)	(ft/ft)	(ft/sec)	(cfs)	
3.2 2	220	0.0640	1.16		Lag/CN Method,

Subcatchment CS: South Catchment



Summary for Link E-Creek: Existing Creek

Inflow /	Area	=	29.071 ac,	0.00% Impervious,	Inflow Depth = 1	.36" for 2-yr event
Inflow		=	53.17 cfs @	12.22 hrs, Volume	= 3.298 af	:
Primary	У	=	53.17 cfs @	12.22 hrs, Volume	= 3.298 af	² , Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link E-Creek: Existing Creek

Summary for Link E-South: Existing South

Inflow /	Area	=	4.921 ac,	0.00% Impervious	, Inflow Depth =	1.43"	for 2-yr event
Inflow		=	14.74 cfs @	12.11 hrs, Volum	e= 0.586	af	
Primar	у	=	14.74 cfs @	12.11 hrs, Volum	e= 0.586	af, Atte	n= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link E-South: Existing South

Summary for Link E-West: Existing West

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Inflow A	Area	=	6.224 ac,	0.00% Impe	ervious,	Inflow Depth =	1.5	50" for 2	-yr event
Inflow		=	19.75 cfs @	12.11 hrs,	Volume	= 0.778	af		
Primary	у	=	19.75 cfs @	12.11 hrs,	Volume	= 0.778	af,	Atten= 0%	6, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs

Hydrograph 22 21 - Inflow 19.75 cfs - Primary 20 19 Inflow Area=6.224 ac 18-17 16-15-14 13 Flow (cfs) 12 11 10-9-8-7. 6-5-4-3-2-1-0-Ó 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 Time (hours)

Link E-West: Existing West

	121139-Creekside 5-27-2022-Existing
00-121186-PROPOSED- 05-26-22	MSE 24-hr 3 10-yr Rainfall=4.19"
Prepared by {enter your company name here}	Printed 6/21/2022
HydroCAD® 10.10-7a s/n 00590 © 2021 HydroCAD Software Solution	ns LLC Page 20
Time span=0.00-160.00 hrs, dt=0.001 hr Runoff by SCS TR-20 method, UH=SCS Reach routing by Sim-Route method - Pond rout	s, 160001 points S, Weighted-CN ing by Sim-Route method
SubcatchmentAS: West CatchmentRunoff Area=271,108Flow Length=200'Slope=0.0700 '/' Tc=1	8 sf 0.00% Impervious Runoff Depth=2.72" 2.7 min CN=86 Runoff=34.59 cfs 1.410 af
Subcatchment BS: Central Catchment Runoff Area=1,266,338 Flow Length=850' Slope=0.0310 '/' Tc=1	8 sf 0.00% Impervious Runoff Depth=2.54" 3.9 min CN=84 Runoff=98.97 cfs 6.152 af
Subcatchment CS: South Catchment Runoff Area=214,369 Flow Length=220' Slope=0.0640 '/' Tc=	9 sf 0.00% Impervious Runoff Depth=2.63" 3.2 min CN=85 Runoff=26.28 cfs 1.078 af
Link E-Creek: Existing Creek	Inflow=98.97 cfs 6.152 af Primary=98.97 cfs 6.152 af
Link E-South: Existing South	Inflow=26.28 cfs 1.078 af Primary=26.28 cfs 1.078 af
Link E-West: Existing West	Inflow=34.59 cfs 1.410 af Primary=34.59 cfs 1.410 af

Total Runoff Area = 40.216 acRunoff Volume = 8.640 af
100.00% Pervious = 40.216 acAverage Runoff Depth = 2.58"
0.00% Impervious = 0.000 ac
Summary for Subcatchment AS: West Catchment

Runoff = 34.59 cfs @ 12.11 hrs, Volume= 1.410 af, Depth= 2.72" Routed to Link E-West : Existing West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

Area (sf)	CN	Description		
188,355	89	Row crops,	straight rov	w, Good, HSG D
82,753	79	Woods, Fai	r, HSG D	
271,108	86	Weighted A	verage	
271,108		100.00% Pe	ervious Are	a
Tc Length	Slope	e Velocity	Capacity	Description
(min) (feet)	(ft/ft) (ft/sec)	(cfs)	
2.7 200	0.0700) 1.23		Lag/CN Method,

Subcatchment AS: West Catchment



Summary for Subcatchment BS: Central Catchment

Runoff = 98.97 cfs @ 12.22 hrs, Volume= 6.152 af, Depth= 2.54" Routed to Link E-Creek : Existing Creek

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

Area (sf) CN	N D	escription		
664,670) 89	9 R	low crops,	straight rov	w, Good, HSG D
601,668	3 79	9 V	∕oods, Faiı	r, HSG D	
1,266,338	3 84	4 W	Veighted A	verage	
1,266,338	3	1	00.00% Pe	ervious Are	a
Tc Leng	th S	lope	Velocity	Capacity	Description
(min) (fee	et) ((ft/ft)	(ft/sec)	(cfs)	
13.9 85	50 0.0)310	1.02		Lag/CN Method,

Subcatchment BS: Central Catchment



Summary for Subcatchment CS: South Catchment

Runoff = 26.28 cfs @ 12.11 hrs, Volume= 1.078 af, Depth= 2.63" Routed to Link E-South : Existing South

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

Area	(sf)	CN	Description		
131,0)49	89	Row crops,	straight rov	w, Good, HSG D
83,3	320	79	Woods, Fai	r, HSG D	
214,3	869	85	Weighted A	verage	
214,3	869		100.00% Pe	ervious Are	ea
Tc Lei	ngth	Slope	e Velocity	Capacity	Description
(min) (f	eet)	(ft/ft) (ft/sec)	(cfs)	
3.2	220	0.0640	0 1.16		Lag/CN Method,

Subcatchment CS: South Catchment

- Runoff

Slope=0.0640 '/'

Tc=3.2 min

140

130

CN=85

150

160



100

110

120

10

8-6-

4-2-0-

0

10

20

30

40

60

70

80

Time (hours)

90

50

Summary for Link E-Creek: Existing Creek

Inflow /	Area	=	29.071 ac,	0.00% Impervious,	Inflow Depth = 2	2.54" for 10	0-yr event
Inflow		=	98.97 cfs @	12.22 hrs, Volume	= 6.152 a	ıf	
Primary	У	=	98.97 cfs @	12.22 hrs, Volume	= 6.152 a	if, Atten= 0%	o, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link E-Creek: Existing Creek

Summary for Link E-South: Existing South

Inflow /	Area	=	4.921 ac,	0.00% Impervious,	Inflow Depth =	2.63" for	10-yr event
Inflow		=	26.28 cfs @	12.11 hrs, Volume	e 1.078 a	af	
Primary	у	=	26.28 cfs @	12.11 hrs, Volume	e= 1.078 a	af, Atten= 0	%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link E-South: Existing South

Summary for Link E-West: Existing West

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Inflow /	Area	. =	6.224 ac,	0.00% Impervious,	Inflow Depth =	2.72"	for 10-y	r event
Inflow		=	34.59 cfs @	12.11 hrs, Volume	= 1.410	af		
Primar	у	=	34.59 cfs @	12.11 hrs, Volume	e= 1.410 a	af, Atte	n= 0%, I	_ag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link E-West: Existing West

	121139-Creekside 5-27-2022-Existing
00-121186-PROPOSED- 05-26-22	MSE 24-hr 3 100-yr Rainfall=7.47"
Prepared by {enter your company name here}	Printed 6/21/2022
HydroCAD® 10.10-7a s/n 00590 © 2021 HydroCAD Software Solution	s LLC Page 27
Time span=0.00-160.00 hrs, dt=0.001 hrs Runoff by SCS TR-20 method, UH=SCS Reach routing by Sim-Route method - Pond routi	s, 160001 points 5, Weighted-CN ng by Sim-Route method
Subcatchment AS: West CatchmentRunoff Area=271,108Flow Length=200'Slope=0.0700 '/' Tc=2	sf 0.00% Impervious Runoff Depth=5.82" 2.7 min CN=86 Runoff=70.08 cfs 3.018 af
Subcatchment BS: Central Catchment Runoff Area=1,266,338 Flow Length=850' Slope=0.0310 '/' Tc=13.9	sf 0.00% Impervious Runoff Depth=5.59" min CN=84 Runoff=211.64 cfs 13.537 af
Subcatchment CS: South CatchmentRunoff Area=214,369Flow Length=220'Slope=0.0640 '/' Tc=3	sf 0.00% Impervious Runoff Depth=5.70" 3.2 min CN=85 Runoff=54.14 cfs 2.339 af
Link E-Creek: Existing Creek	Inflow=211.64 cfs 13.537 af Primary=211.64 cfs 13.537 af
Link E-South: Existing South	Inflow=54.14 cfs 2.339 af Primary=54.14 cfs 2.339 af
Link E-West: Existing West	Inflow=70.08 cfs 3.018 af Primary=70.08 cfs 3.018 af

Total Runoff Area = 40.216 acRunoff Volume = 18.893 afAverage Runoff Depth = 5.64"100.00% Pervious = 40.216 ac0.00% Impervious = 0.000 ac

Summary for Subcatchment AS: West Catchment

Runoff = 70.08 cfs @ 12.11 hrs, Volume= 3.018 af, Depth= 5.82" Routed to Link E-West : Existing West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

Area (s	sf)	CN [Description		
188,35	55	89 F	Row crops,	straight rov	w, Good, HSG D
82,75	53	79 V	Voods, Fai	r, HSG D	
271,10	28	86 V	Veighted A	verage	
271,10	28	1	100.00% Pe	ervious Are	a
Tc Len	gth	Slope	Velocity	Capacity	Description
(min) (fe	et)	(ft/ft)	(ft/sec)	(cfs)	
2.7 2	200	0.0700	1.23		Lag/CN Method,

Subcatchment AS: West Catchment





Summary for Subcatchment BS: Central Catchment

Runoff = 211.64 cfs @ 12.22 hrs, Volume= 13.537 af, Depth= 5.59" Routed to Link E-Creek : Existing Creek

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

Area (sf)	CN	Description		
664,670	89	Row crops,	straight rov	w, Good, HSG D
601,668	79	Woods, Fai	r, HSG D	
1,266,338	84	Weighted A	verage	
1,266,338		100.00% Pe	ervious Are	a
Tc Length	Slope	Velocity	Capacity	Description
(min) (feet)	(ft/ft)	(ft/sec)	(cfs)	
13.9 850	0.0310	1.02		Lag/CN Method,

Subcatchment BS: Central Catchment



Summary for Subcatchment CS: South Catchment

Runoff = 54.14 cfs @ 12.11 hrs, Volume= 2.339 af, Depth= 5.70" Routed to Link E-South : Existing South

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

Area	a (sf)	CN	Description		
131	,049	89	Row crops,	straight rov	w, Good, HSG D
83	3,320	79	Woods, Fai	r, HSG D	
214	,369	85	Weighted A	verage	
214	,369		100.00% Pe	ervious Are	a
Tc L	ength	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
3.2	220	0.0640	1.16		Lag/CN Method,

Subcatchment CS: South Catchment



Summary for Link E-Creek: Existing Creek

Inflow /	Area	=	29.071 ac,	0.00% Impervious,	Inflow Depth =	5.5	9" for 100-yr event
Inflow		=	211.64 cfs @	12.22 hrs, Volume	= 13.537	af	
Primar	у	=	211.64 cfs @	12.22 hrs, Volume	= 13.537	af,	Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Time (hours)

Summary for Link E-South: Existing South

Inflow /	Area	a =	4.921 ac,	0.00% Impervious,	Inflow Depth = 5	.70" for 100-yr event
Inflow		=	54.14 cfs @	12.11 hrs, Volume	= 2.339 af	
Primar	у	=	54.14 cfs @	12.11 hrs, Volume	= 2.339 af	, Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link E-South: Existing South

Summary for Link E-West: Existing West

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Inflow /	Area	=	6.224 ac,	0.00% Impervious,	Inflow Depth = 5.8	82" for 100-yr event
Inflow		=	70.08 cfs @	12.11 hrs, Volume	= 3.018 af	
Primar	у	=	70.08 cfs @	12.11 hrs, Volume	= 3.018 af,	Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link E-West: Existing West



121139-Creekside 5-27-2022-Proposed

00-121186-PROPOSED- 05-26-22

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Event# Event Storm Type Curve Mode Duration B/B Depth AMC Name (inches) (hours) 1-yr MSE 24-hr 3 Default 24.00 1 2.46 2 1 2 2-yr MSE 24-hr 3 Default 24.00 1 2.81 2 3 10-yr MSE 24-hr 3 Default 24.00 1 4.19 2 4 100-yr MSE 24-hr 24.00 1 7.47 2 3 Default

Rainfall Events Listing

121139-Creekside 5-27-2022-Proposed

00-121186-PROPOSED- 05-26-22

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Area Listing (selected nodes)

Area	CN	Description
 (acres)		(subcatchment-numbers)
22.522	80	>75% Grass cover, Good, HSG D (1S, 2S, 3S, 4S, 5S, 6S, 7S)
11.631	98	Paved parking, HSG D (1S, 2S, 3S, 4S, 5S, 6S, 7S)
6.063	79	Woods, Fair, HSG D (4S, 5S, 6S, 7S)
40.216	85	TOTAL AREA

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Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.000	HSG C	
40.216	HSG D	1S, 2S, 3S, 4S, 5S, 6S, 7S
0.000	Other	
40.216		TOTAL AREA

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		_		(- /	
HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment
 (acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers
0.000	0.000	0.000	22.522	0.000	22.522	>75% Grass cover, Good	1S, 2S,
							3S, 4S,
							5S, 6S,
							7S
0.000	0.000	0.000	11.631	0.000	11.631	Paved parking	1S, 2S,
							3S, 4S,
							5S, 6S,
							7S
0.000	0.000	0.000	6.063	0.000	6.063	Woods, Fair	4S, 5S,
							6S, 7S
0.000	0.000	0.000	40.216	0.000	40.216	TOTAL AREA	

Ground Covers (selected nodes)

00-121186-PROPOSED- 05-26-22 Prepared by {enter your company name here}	121139-Creekside 5-27-2022-Proposed MSE 24-hr 3 1-yr Rainfall=2.46" Printed 6/21/2022
HydroCAD® 10.10-7a s/n 00590 © 2021 HydroCAD Software	Solutions LLC Page 6
Time span=0.00-160.00 hrs, dt=0	0.001 hrs, 160001 points
Runoff by SCS TR-20 method, L	JH=SCS, Weighted-CN
Reach routing by Sim-Route method - Po	ond routing by Sim-Route method
Subcatchment 1S: N-C Catchment Runoff Area=7	718,098 sf 43.62% Impervious Runoff Depth=1.35"
Flow Length=975' Slope=0.0240 '	'/' Tc=15.3 min CN=88 Runoff=28.61 cfs 1.851 af
Subcatchment 2S: East Catchment Flow Length=670' Runoff Area=2	202,210 sf 41.66% Impervious Runoff Depth=1.28"
Flow Length=670' Slope=0.0310) '/' Tc=10.3 min CN=87 Runoff=9.12 cfs 0.494 af
Subcatchment 3S: South Catchment Runoff Area=	=82,515 sf 48.85% Impervious Runoff Depth=1.42"
Flow Length=442' Slope=0.018	30 '/' Tc=9.0 min CN=89 Runoff=4.39 cfs 0.224 af
Subcatchment 4S: West Catchment Runoff Area=1	156,360 sf 18.01% Impervious Runoff Depth=1.03"
Flow Length=200' Slope=0.065	50 '/' Tc=3.1 min CN=83 Runoff=7.85 cfs 0.307 af
Subcatchment 5S: S-C Catchment Flow Length=150' Runoff Area	a=75,496 sf 9.11% Impervious Runoff Depth=0.91"
Flow Length=150' Slope=0.093	30 '/' Tc=2.2 min CN=81 Runoff=3.51 cfs 0.132 af
Subcatchment 6S: South Catchment Flow Length=220' Runoff Area=	=193,325 sf 7.41% Impervious Runoff Depth=0.91" 40 '/' Tc=3.6 min CN=81 Runoff=8.49 cfs 0.338 af
Subcatchment7S: Creek Catchment Runoff Area=	=323,811 sf 6.02% Impervious Runoff Depth=0.86"
Flow Length=850' Slope=0.0260) '/' Tc=17.3 min CN=80 Runoff=7.50 cfs 0.534 af
Pond 100P: Basin 100Peak Elev=9Primary=7.35 cfs1.681 afSecondary=3.33 cfs0.165 afTer	962.40' Storage=3.557 af Inflow=28.61 cfs 1.851 af rtiary=0.00 cfs 0.000 af Outflow=10.68 cfs 1.846 af
Pond 200P: Basin 200 Peak Elev=	=962.52' Storage=1.939 af Inflow=9.12 cfs 0.494 af
Primary=1.24 cfs 0.490 af Seco	ondary=0.00 cfs 0.000 af Outflow=1.24 cfs 0.490 af
Pond 300P: Basin 300 Peak Elev=	=966.57' Storage=0.413 af Inflow=4.39 cfs 0.224 af
Primary=1.27 cfs 0.224 af Seco	ondary=0.00 cfs 0.000 af Outflow=1.27 cfs 0.224 af
Link P-Creek: Proposed Creek	Inflow=17.76 cfs 3.225 af Primary=17.76 cfs 3.225 af
Link P-South: Proposed South	Inflow=8.49 cfs 0.338 af Primary=8.49 cfs 0.338 af
Link P-West: Proposed West	Inflow=7.85 cfs 0.307 af Primary=7.85 cfs 0.307 af

Total Runoff Area = 40.216 ac Runoff Volume = 3.880 af Average Runoff Depth = 1.16" 71.08% Pervious = 28.585 ac 28.92% Impervious = 11.631 ac

Summary for Subcatchment 1S: N-C Catchment

Runoff = 28.61 cfs @ 12.24 hrs, Volume= 1.851 af, Depth= 1.35" Routed to Pond 100P : Basin 100

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

A	rea (sf)	CN	Description					
4	04,877	80	>75% Gras	s cover, Go	ood, HSG D			
3	13,221	98	Paved park	ing, HSG D)			
	0	79	Woods, Fai	r, HSG D				
718,098 88 Weighted Average				verage				
4	04,877		56.38% Pervious Area					
3	13,221		43.62% Imp	pervious Ar	rea			
Тс	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
15.3	975	0.0240	1.06		Lag/CN Method,			
					-			

Subcatchment 1S: N-C Catchment



Summary for Subcatchment 2S: East Catchment

Runoff = 9.12 cfs @ 12.18 hrs, Volume= 0.494 af, Depth= 1.28" Routed to Pond 200P : Basin 200

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

Α	rea (sf)	CN	Description		
1	17,965	80	>75% Gras	s cover, Go	ood, HSG D
	84,245	98	Paved park	ing, HSG D	
	0	79	Woods, Fai	r, HSG D	
2	02,210	87	Weighted A	verage	
1	117,965 58.34% Pervious Area				3
	84,245		41.66% Imp	pervious Are	rea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
10.3	670	0.0310	1.08		Lag/CN Method,
					-

Subcatchment 2S: East Catchment



Summary for Subcatchment 3S: South Catchment

Runoff = 4.39 cfs @ 12.17 hrs, Volume= 0.224 af, Depth= 1.42" Routed to Pond 300P : Basin 300

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

A	rea (sf)	CN	Description				
	42,205	80	>75% Gras	s cover, Go	ood, HSG D		
	40,310	98	Paved park	ing, HSG D			
	0	79	Woods, Fai	r, HSG D			
	82,515	89	Weighted Average				
	42,205		51.15% Pervious Area				
	40,310		48.85% Imp				
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)			
9.0	442	0.0180	0.82		Lag/CN Method,		
					-		

Subcatchment 3S: South Catchment



Summary for Subcatchment 4S: West Catchment

Runoff = 7.85 cfs @ 12.11 hrs, Volume= 0.307 af, Depth= 1.03" Routed to Link P-West : Proposed West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

A	rea (sf)	CN	Description				
1	09,417	80	>75% Gras	s cover, Go	od, HSG D		
	28,163	98	Paved park	ing, HSG D			
	18,780	79	Woods, Fai	r, HSG D			
1	56,360	83	83 Weighted Average				
1	28,197		81.99% Pei	vious Area			
	28,163		18.01% Imp	pervious Are	ea		
Тс	Length	Slope	Velocity	Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
3.1	200	0.0650	1.07		Lag/CN Method,		
					-		

Subcatchment 4S: West Catchment



Summary for Subcatchment 5S: S-C Catchment

Runoff = 3.51 cfs @ 12.11 hrs, Volume= 0.132 Routed to Link P-Creek : Proposed Creek

0.132 af, Depth= 0.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

Α	rea (sf)	CN	Description					
	37,344	80	>75% Gras	s cover, Go	bod, HSG D			
	6,876	98	Paved park	ing, HSG D)			
	31,276	79	Woods, Fai	r, HSG D				
	75,496	81	31 Weighted Average					
	68,620	9	90.89% Per	rvious Area	1			
	6,876	9	9.11% Impe	ervious Area	a			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
2.2	150	0.0930	1.13		Lag/CN Method,			
					-			

Subcatchment 5S: S-C Catchment



Summary for Subcatchment 6S: South Catchment

Runoff = 8.49 cfs @ 12.12 hrs, Volume= 0.338 af, Depth= 0.91" Routed to Link P-South : Proposed South

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

A	rea (sf)	CN	Description					
1	54,331	80	>75% Gras	s cover, Go	ood, HSG D			
	14,333	98	Paved park	ing, HSG D)			
	24,661	79	Noods, Fai	r, HSG D				
1	193.325 81 Weighted Average							
178,992			92.59% Pervious Area					
	14,333		7.41% Impe	ervious Area	a			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
3.6	220	0.0640	1.01		Lag/CN Method,			
					-			

Subcatchment 6S: South Catchment



Summary for Subcatchment 7S: Creek Catchment

Runoff = 7.50 cfs @ 12.28 hrs, Volume= 0.534 af, Depth= 0.86" Routed to Link P-Creek : Proposed Creek

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 1-yr Rainfall=2.46"

Α	rea (sf)	CN	Description					
1	14,917	80	>75% Gras	s cover, Go	bod, HSG D			
	19,500	98	Paved park	ing, HSG D)			
1	89,394	79	Woods, Fai	r, HSG D				
3	323,811 80 Weighted Average							
3	304,311		93.98% Pervious Area					
	19,500		6.02% Impervious Area					
Tc	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
17.3	850	0.0260	0.82		Lag/CN Method,			
					-			

Subcatchment 7S: Creek Catchment



Summary for Pond 100P: Basin 100

Inflow Area =	16.485 ac,	43.62% Impervious, Inf	low Depth = 1.35" for 1-yr event
Inflow =	28.61 cfs @	12.24 hrs, Volume=	1.851 af
Outflow =	10.68 cfs @	12.53 hrs, Volume=	1.846 af, Atten= 63%, Lag= 17.5 min
Primary =	7.35 cfs @	12.53 hrs, Volume=	1.681 af
Routed to	Link P-Creek : Pr	oposed Creek	
Secondary =	3.33 cfs @	12.53 hrs, Volume=	0.165 af
Routed to	Link P-Creek : Pr	oposed Creek	
Tertiary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af
Routed to	Link P-Creek : Pr	oposed Creek	

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 961.00' Surf.Area= 0.545 ac Storage= 2.752 af Peak Elev= 962.40' @ 12.53 hrs Surf.Area= 0.609 ac Storage= 3.557 af (0.805 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 178.9 min (990.2 - 811.3)

Volume	Inve	rt Avail.S	torage S	Storage Description
#1	951.0)' 7.	.655 af (Custom Stage Data (Prismatic)Listed below (Recalc)
	0	r ,		
Elevatio	n Sur	f.Area	Inc.Stor	e Cum.Store
(fee	t) (a	acres)	(acre-feet	t) (acre-feet)
951.0	0	0.119	0.00	0 0.000
952.0	0	0.145	0.13	2 0.132
954.0	0	0.201	0.34	7 0.479
956.0	0	0.263	0.46	5 0.944
958.0	0	0.332	0.59	5 1.539
960.0	0	0.406	0.73	8 2.277
961.0	0	0.545	0.47	6 2.752
962.0	0	0.590	0.56	8 3.320
964.0	0	0.685	1.27	5 4.595
965.0	0	0.735	0.71	0 5.305
966.0	0	0.786	0.76	0 6.065
968.0	0	0.803	1.58	9 7.655
Device	Routing	Inve	ert Outle	at Devices
#1	Primary	961.0	00' 30.0'	' Round RCP Round 30"
	,		L= 50	0.0' RCP, groove end projecting, Ke= 0.200
			Inlet	/ Outlet Invert= 961.00' / 960.50' S= 0.0100 '/' Cc= 0.900
			n= 0.	.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf
#2	Device 1	961.0	00' Cust	om Weir/Orifice, Cv= 2.62 (C= 3.28)
			Head	l (feet) 0.00 1.05 1.05 8.00
			Width	n (feet) 0.85 0.85 5.00 5.00
#3	Device 2	957.5	50' 30.0'	' Round RCP_Round 30"
			L= 25	5.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet	/ Outlet Invert= 957.50' / 957.50' S= 0.0000 '/' Cc= 0.900
			n= 0.	.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf
#4	Tertiary	966.0	00' 15.0'	long x 10.0' breadth Broad-Crested Rectangular Weir
			Head	l (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60

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			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64
#5	Secondary	961.00'	30.0" Round RCP_Round 30"
	-		L= 50.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 961.00' / 960.50' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf
#6	Device 5	962.05'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28)
			Head (feet) 0.00 5.00
			Width (feet) 5.00 5.00
#7	Device 6	957.50'	30.0" Round RCP_Round 30"
			L= 25.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 957.50' / 957.50' S= 0.0000 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections. Flow Area= 4.91 sf

Primary OutFlow Max=7.35 cfs @ 12.53 hrs HW=962.40' TW=0.00' (Dynamic Tailwater)

- -1=RCP_Round 30" (Passes 7.35 cfs of 10.91 cfs potential flow)
 - **2=Custom Weir/Orifice** (Weir Controls 7.35 cfs @ 2.81 fps)

3=RCP_Round 30" (Passes 7.35 cfs of 27.92 cfs potential flow)

Secondary OutFlow Max=3.33 cfs @ 12.53 hrs HW=962.40' TW=0.00' (Dynamic Tailwater)
5=RCP_Round 30" (Passes 3.33 cfs of 10.91 cfs potential flow)
6=Custom Weir/Orifice (Weir Controls 3.33 cfs @ 1.93 fps)
7=RCP_Round 30" (Passes 3.33 cfs of 13.90 cfs potential flow)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=961.00' TW=0.00' (Dynamic Tailwater) **4=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 100P: Basin 100



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 121139-Creekside 5-27-2022-Proposed

 MSE 24-hr 3
 1-yr Rainfall=2.46"

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Summary for Pond 200P: Basin 200

Inflow Are	a =	4.642 ac, 4	1.66% Imp	ervious,	Inflow Dept	:h = 1.	28" fo	or 1-yr	event	
Inflow	=	9.12 cfs @	12.18 hrs,	Volume=	= 0.	.494 af		-		
Outflow	=	1.24 cfs @	12.70 hrs,	Volume=	= 0.	.490 af,	Atten	= 86%,	Lag= :	31.4 min
Primary	=	1.24 cfs @	12.70 hrs,	Volume=	= 0.	.490 af			•	
Routed	to Link F	P-Creek : Pro	posed Cree	ek						
Secondary	/ =	0.00 cfs @	0.00 hrs,	Volume=	= 0.	.000 af				
Routed	to Link F	P-Creek : Pro	posed Cree	ek						

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 962.00' Surf.Area= 0.480 ac Storage= 1.681 af Peak Elev= 962.52' @ 12.70 hrs Surf.Area= 0.509 ac Storage= 1.939 af (0.258 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 297.8 min (1,107.4 - 809.6)

Volume	Invert	Avail.Stora	age Stora	age Description
#1	952.00'	4.760	af Cus t	tom Stage Data (Prismatic)Listed below (Recalc)
Elevatio	n Surf.Ar	ea In	c.Store	Cum.Store
(fee	t) (acre	es) (ac	re-feet)	(acre-feet)
952.0	0.0	23	0.000	0.000
954.0	0.0	59	0.081	0.081
956.0	0 0.1	10	0.168	0.250
958.0	0 0.1	83	0.293	0.543
960.0	0 0.2	67	0.451	0.994
961.0	0 0.3	13	0.290	1.284
962.0	0 0.4	80	0.397	1.681
964.0	0 0.5	89	1.069	2.750
965.0	0 0.6	46	0.618	3.367
966.0	0 0.7	02	0.674	4.042
967.0	0 0.73	35	0.719	4.760
Device	Routing	Invert	Outlet De	evices
#1	Primary	962.00'	15.0" Ro	ound RCP Round 15"
			L= 25.0'	RCP, groove end projecting, Ke= 0.200
			Inlet / Ou	Itlet Invert= 962.00' / 961.50' S= 0.0200 '/' Cc= 0.900
			n= 0.013	Concrete pipe, bends & connections, Flow Area= 1.23 sf
#2	Device 1	962.00'	Custom	Weir/Orifice, Cv= 2.62 (C= 3.28)
			Head (fe	et) 0.00 1.00 1.00 8.00
			Width (fe	et) 1.00 1.00 5.00 5.00
#3	Device 2	959.75'	15.0" Ro	ound RCP_Round 15"
			L= 25.0'	RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Ou	itlet Invert= 959.75' / 959.75' S= 0.0000 '/' Cc= 0.900
	• •		n= 0.013	Concrete pipe, bends & connections, Flow Area= 1.23 sf
#4	Secondary	966.00'	25.0' lon	g x 10.0' breadth Broad-Crested Rectangular Weir
			Head (fe	et) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coet. (Er	nglisn) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=1.24 cfs @ 12.70 hrs HW=962.52' TW=0.00' (Dynamic Tailwater) 1=RCP_Round 15" (Passes 1.24 cfs of 1.44 cfs potential flow) 2=Custom Weir/Orifice (Weir Controls 1.24 cfs @ 2.37 fps) 3=RCP_Round 15" (Passes 1.24 cfs of 4.27 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=962.00' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)



Pond 200P: Basin 200

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 MSE 24-hr 3
 1-yr Rainfall=2.46"

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Summary for Pond 300P: Basin 300

1.894 ac, 48.85% Impervious, Inflow Depth = 1.42" for 1-yr event Inflow Area = Inflow 4.39 cfs @ 12.17 hrs, Volume= 0.224 af = 1.27 cfs @ 12.41 hrs, Volume= Outflow 0.224 af, Atten= 71%, Lag= 14.5 min = Primary = 1.27 cfs @ 12.41 hrs, Volume= 0.224 af Routed to Link P-Creek : Proposed Creek Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Routed to Link P-Creek : Proposed Creek

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 966.00' Surf.Area= 0.160 ac Storage= 0.317 af Peak Elev= 966.57' @ 12.41 hrs Surf.Area= 0.181 ac Storage= 0.413 af (0.096 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 132.3 min (934.7 - 802.4)

Volume	Invert A	vail.Stora	ge Stor	rage Description
#1	958.00'	1.594	af Cus	stom Stage Data (Prismatic)Listed below (Recalc)
Elevatio	on Surf.Area	In	c.Store	Cum.Store
(fee	et) (acres)	(acı	e-feet)	(acre-feet)
958.0	0.003	1	0.000	0.000
960.0	0.012		0.015	0.015
962.0	0.029		0.041	0.056
964.0	0 0.053		0.083	0.139
965.0	0.071		0.062	0.201
966.0	0.160		0.116	0.317
968.0	0 0.234		0.394	0.711
970.0	0.316		0.550	1.261
971.0	0 0.351		0.333	1.594
Device	Routing	Invert	Outlet D	evices
#1	Primary	966.00'	15.0" R	cound RCP_Round 15"
			L= 25.0'	RCP, groove end projecting, Ke= 0.200
			Inlet / O	utlet Invert= 966.00' / 965.50' S= 0.0200 '/' Cc= 0.900
			n= 0.013	3 Concrete pipe, bends & connections, Flow Area= 1.23 sf
#2	Device 1	966.00'	Custom	1 Weir/Orifice, Cv= 2.62 (C= 3.28)
			Head (fe	eet) 0.00 0.50 0.50 5.00
			Width (fe	eet) 0.75 0.75 5.00 5.00
#3	Device 2	963.75'	15.0" R	cound RCP_Round 15"
			L= 30.0'	RCP, end-section conforming to fill, Ke= 0.500
			Inlet / O	utlet Invert= 963.75' / 963.75' S= 0.0000 '/' Cc= 0.900
	- ·		n= 0.013	3 Concrete pipe, bends & connections, Flow Area= 1.23 st
#4	Secondary	970.00'	25.0' lor	ng x 10.0' breadth Broad-Crested Rectangular Weir
			Head (fe	eet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coet. (E	nglish) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=1.27 cfs @ 12.41 hrs HW=966.57' TW=0.00' (Dynamic Tailwater) 1=RCP_Round 15" (Passes 1.27 cfs of 1.65 cfs potential flow) 2=Custom Weir/Orifice (Weir Controls 1.27 cfs @ 1.82 fps) -3=RCP_Round 15" (Passes 1.27 cfs of 4.44 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=966.00' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)



Pond 300P: Basin 300

Summary for Link P-Creek: Proposed Creek

Inflow Are	a =	32.188 ac, 3	3.10% Impervious	, Inflow Depth = 1	.20" for 1-yr event
Inflow	=	17.76 cfs @	12.46 hrs, Volum	e= 3.225 af	
Primary	=	17.76 cfs @	12.46 hrs, Volume	e= 3.225 af	, Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link P-Creek: Proposed Creek

Summary for Link P-South: Proposed South

Inflow A	Area	=	4.438 ac,	7.41% Impervious,	Inflow Depth = 0	.91" for 1-yr event
Inflow		=	8.49 cfs @	12.12 hrs, Volume	= 0.338 af	:
Primary	у	=	8.49 cfs @	12.12 hrs, Volume	≔ 0.338 af	, Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link P-South: Proposed South

Summary for Link P-West: Proposed West

Inflow /	Area	=	3.590 ac,	18.01% Impe	ervious,	Inflow Dep	oth =	1.03"	for 1-	yr event	
Inflow		=	7.85 cfs @	12.11 hrs,	Volume	= 0).307 a	af			
Primar	у	=	7.85 cfs @	12.11 hrs,	Volume	= 0).307 a	af, Att	en= 0%	,Lag= 0.1 mi	n

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link P-West: Proposed West
00-121186-PROPOS	ED- 05-26-22		1211: /	39-Creeks MSE 24-h	ide 5-27-202 or 3_2-yr Ra	22-Proposed ainfall=2.81"
Prepared by {enter you HydroCAD® 10.10-7a s/n 0	r company name 00590 © 2021 Hydr	here} oCAD Software S	olutions LLC		Printe	d 6/21/2022 Page 23
Reach rou	Time span=0.00-16 Runoff by SCS TF uting by Sim-Route	60.00 hrs, dt=0.0 R-20 method, UF e method - Pon	001 hrs, 1600 I=SCS, Weig d routing by	001 points ghted-CN Sim-Route	e method	
Subcatchment1S: N-C (Catchment Flow Length=975'	Runoff Area=71 Slope=0.0240 '/'	8,098 sf 43. Tc=15.3 mir	62% Imper 0 CN=88	vious Runof Runoff=34.96	f Depth=1.65" 5 cfs 2.267 af
Subcatchment2S: East	Catchment Flow Length=670'	Runoff Area=20 Slope=0.0310 '/'	2,210 sf 41. Tc=10.3 mir	66% Imper 0 CN=87	vious Runof Runoff=11.21	f Depth=1.57" I cfs_0.609 af
Subcatchment3S: Sout	h Catchment Flow Length=442	Runoff Area=8 2' Slope=0.0180	2,515 sf 48. '/' Tc=9.0 m	85% Imper in CN=89	vious Runof Runoff=5.3 ²	f Depth=1.73" I cfs_0.273 af
Subcatchment4S: West	Catchment Flow Length=200	Runoff Area=15)' Slope=0.0650	6,360 sf 18. '/' Tc=3.1 m	01% Imper in CN=83	vious Runof Runoff=9.8	f Depth=1.30" 5 cfs_0.387 af
Subcatchment5S: S-C (Catchment Flow Length=150	Runoff Area=)' Slope=0.0930	75,496 sf 9. '/' Tc=2.2 m	11% Imper in CN=81	vious Runof Runoff=4.47	f Depth=1.17" ′ cfs 0.169 af
Subcatchment6S: Sout	h Catchment Flow Length=220'	Runoff Area=1 Slope=0.0640 '/	93,325 sf 7. ' Tc=3.6 mir	41% Imper 0 CN=81	vious Runof Runoff=10.85	f Depth=1.17" 5 cfs 0.432 af
Subcatchment7S: Cree	k Catchment Flow Length=850'	Runoff Area=3 Slope=0.0260 '/	23,811 sf 6. ' Tc=17.3 m	02% Imper in CN=80	vious Runof Runoff=9.79	f Depth=1.11") cfs 0.687 af
Pond 100P: Basin 100 Primary=10.47 cfs 1.963 af	Secondary=6.05 cf	Peak Elev=96 s 0.299 af Tertia	2.56' Storage ary=0.00 cfs	e=3.661 af 0.000 af _C	Inflow=34.96 Dutflow=16.51	6 cfs 2.267 af cfs 2.262 af
Pond 200P: Basin 200	Primary=1.67 cfs	Peak Elev=96 0.605 af Secon	2.64' Storage dary=0.00 cfs	e=1.998 af 0.000 af	Inflow=11.27 Outflow=1.67	l cfs 0.609 af ′ cfs 0.605 af
Pond 300P: Basin 300	Primary=2.00 cfs	Peak Elev=9 0.272 af Secon	66.64' Storaç dary=0.00 cfs	ge=0.427 af 0.000 af	f Inflow=5.3 ² Outflow=2.00	l cfs 0.273 af) cfs 0.272 af
Link P-Creek: Proposed	Creek			F	Inflow=27.36 Primary=27.36	6 cfs 3.996 af 6 cfs 3.996 af
Link P-South: Proposed	South			F	Inflow=10.8 Primary=10.8	5 cfs 0.432 af 5 cfs 0.432 af
Link P-West: Proposed	West				Inflow=9.88 Primary=9.88	5 cfs 0.387 af 5 cfs 0.387 af

Total Runoff Area = 40.216 ac Runoff Volume = 4.825 af Average Runoff Depth = 1.44" 71.08% Pervious = 28.585 ac 28.92% Impervious = 11.631 ac

Summary for Subcatchment 1S: N-C Catchment

Runoff = 34.96 cfs @ 12.24 hrs, Volume= 2.267 af, Depth= 1.65" Routed to Pond 100P : Basin 100

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

A	rea (sf)	CN	Description				
4	04,877	80	>75% Gras	s cover, Go	ood, HSG D		
3	13,221	98	Paved park	ing, HSG D)		
	0	79	Woods, Fair, HSG D				
7	18,098	88	Weighted A	verage			
4	04,877		56.38% Pei	vious Area	3		
3	13,221		43.62% Imp	pervious Are	rea		
Тс	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
15.3	975	0.0240	1.06		Lag/CN Method,		
					-		

Subcatchment 1S: N-C Catchment



Summary for Subcatchment 2S: East Catchment

Runoff = 11.21 cfs @ 12.18 hrs, Volume= 0.609 af, Depth= 1.57" Routed to Pond 200P : Basin 200

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

A	rea (sf)	CN	Description				
1	17,965	80	>75% Gras	s cover, Go	ood, HSG D		
	84,245	98	Paved park	ing, HSG D)		
	0	79	Woods, Fai	r, HSG D			
2	02,210	87	Weighted A	verage			
1	17,965		58.34% Pervious Area				
	84,245		41.66% Imp	pervious Are	ea		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
10.3	670	0.0310	1.08		Lag/CN Method,		
					•		

Subcatchment 2S: East Catchment



Summary for Subcatchment 3S: South Catchment

Runoff = 5.31 cfs @ 12.17 hrs, Volume= 0.273 af, Depth= 1.73" Routed to Pond 300P : Basin 300

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

A	rea (sf)	CN	Description			
	42,205	80	>75% Gras	s cover, Go	ood, HSG D	
	40,310	98	Paved park	ing, HSG D)	
	0	79	Woods, Fai	r, HSG D		
	82,515	89	Weighted A	verage		
	42,205		51.15% Pe	rvious Area		
	40,310		48.85% Imp	pervious Ar	ea	
Tc	Length	Slope	e Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)) (ft/sec)	(cfs)		
9.0	442	0.0180	0.82		Lag/CN Method,	

Subcatchment 3S: South Catchment



Summary for Subcatchment 4S: West Catchment

Runoff = 9.85 cfs @ 12.11 hrs, Volume= 0.387 af, Depth= 1.30" Routed to Link P-West : Proposed West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

A	rea (sf)	CN	Description				
1	09,417	80	>75% Gras	s cover, Go	bod, HSG D		
	28,163	98	Paved park	ing, HSG D)		
	18,780	79	Woods, Fai	r, HSG D			
1	56,360	83	Weighted A	verage			
1	28,197		81.99% Pervious Area				
	28,163		18.01% Imp	pervious Are	ea		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
3.1	200	0.0650	1.07		Lag/CN Method,		
					-		

Subcatchment 4S: West Catchment



Summary for Subcatchment 5S: S-C Catchment

Runoff = 4.47 cfs @ 12.11 hrs, Volume= Routed to Link P-Creek : Proposed Creek 0.169 af, Depth= 1.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

A	rea (sf)	CN	Description				
	37,344	80	>75% Gras	s cover, Go	ood, HSG D		
	6,876	98	Paved park	ing, HSG D)		
	31,276	79	Woods, Fai	r, HSG D			
	75,496	81	Weighted A	verage			
	68,620	1	90.89% Pervious Area				
	6,876		9.11% Impe	ervious Are	a		
Тс	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
2.2	150	0.0930	1.13		Lag/CN Method,		

Subcatchment 5S: S-C Catchment



Summary for Subcatchment 6S: South Catchment

Runoff = 10.85 cfs @ 12.12 hrs, Volume= 0.432 af, Depth= 1.17" Routed to Link P-South : Proposed South

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

Α	rea (sf)	CN	Description				
1	54,331	80	>75% Gras	s cover, Go	ood, HSG D		
	14,333	98	Paved park	ing, HSG D)		
	24,661	79	Woods, Fai	r, HSG D			
1	93,325	81	Weighted A	verage		_	
1	78,992	1	92.59% Pervious Area				
	14,333		7.41% Impe	ervious Area	a		
Тс	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
3.6	220	0.0640	1.01		Lag/CN Method,	_	
					-		

Subcatchment 6S: South Catchment



Summary for Subcatchment 7S: Creek Catchment

Runoff = 9.79 cfs @ 12.28 hrs, Volume= 0.687 af, Depth= 1.11" Routed to Link P-Creek : Proposed Creek

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 2-yr Rainfall=2.81"

Α	rea (sf)	CN	Description		
1	14,917	80	>75% Gras	s cover, Go	bod, HSG D
	19,500	98	Paved park	ing, HSG D)
1	89,394	79	Woods, Fai	r, HSG D	
3	23,811	80	Weighted A	verage	
3	04,311		93.98% Pei	vious Area	1
	19,500		6.02% Impe	ervious Area	a
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
17.3	850	0.0260	0.82		Lag/CN Method,
					-

Subcatchment 7S: Creek Catchment



Summary for Pond 100P: Basin 100

Inflow Area	=	16.485 ac,	43.62% Ir	npervious,	Inflow	Depth =	1.65"	for 2-yr	event	
Inflow	=	34.96 cfs @	🖻 12.24 hi	s, Volume	e=	2.267	af	-		
Outflow	=	16.51 cfs @	َفَ 12.46 hı	s, Volume	e=	2.262	af, Atte	n= 53%,	Lag= 13.3	min
Primary	=	10.47 cfs @	12.46 hi	s, Volume	e=	1.963	af		-	
Routed t	to Link	P-Creek : F	Proposed C	reek						
Secondary	=	6.05 cfs @	🕑 12.46 hi	s, Volume) =	0.299	af			
Routed t	to Link	P-Creek : F	Proposed C	reek						
Tertiary	=	0.00 cfs @	🕑 0.00 hi	s, Volume) =	0.000	af			
Routed t	to Link	P-Creek : F	Proposed C	reek						

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 961.00' Surf.Area= 0.545 ac Storage= 2.752 af Peak Elev= 962.56' @ 12.46 hrs Surf.Area= 0.617 ac Storage= 3.661 af (0.908 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 156.4 min (963.6 - 807.2)

Volume	Inve	rt Avail.	Storage	Storage Description
#1	951.0	O' ·	7.655 af	Custom Stage Data (Prismatic)Listed below (Recalc)
Flevatio	n Sur	f Area	Inc Sto	re Cum Store
(fee	et) (a	acres)	(acre-fee	et) (acre-feet)
951 0)()	0 110		$\frac{1}{100} \qquad 0.000$
952.0	0	0.145	0.00	32 0 132
954 0	0	0 201	0.34	47 0 479
956.0	0	0.263	0.46	65 0.944
958.0	0	0.332	0.59	95 1.539
960.0	00	0.406	0.73	38 2.277
961.0	00	0.545	0.47	76 2.752
962.0	00	0.590	0.56	68 3.320
964.0	00	0.685	1.27	75 4.595
965.0	00	0.735	0.7	10 5.305
966.0	00	0.786	0.76	6.065
968.0	00	0.803	1.58	39 7.655
Device	Routing	In	vert Outl	let Devices
#1	Primarv	961	.00' 30.0	" Round RCP Round 30"
	,		L= 5	50.0' RCP, groove end projecting, Ke= 0.200
			Inlet	/ Outlet Invert= 961.00' / 960.50' S= 0.0100 '/' Cc= 0.900
			n= 0	0.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf
#2	Device 1	961	.00' Cus	tom Weir/Orifice, Cv= 2.62 (C= 3.28)
			Hea	d (feet) 0.00 1.05 1.05 8.00
			Wid	th (feet) 0.85 0.85 5.00 5.00
#3	Device 2	957	.50' 30.0)" Round RCP_Round 30"
			L= 2	25.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet	t / Outlet Invert= 957.50' / 957.50' S= 0.0000 '/' Cc= 0.900
			n= C	0.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf
#4	Tertiary	966	.00' 15.0 Hea	I' long x 10.0' breadth Broad-Crested Rectangular Weir Id (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60

121139-Creekside 5-27-2022-Proposed *MSE 24-hr 3 2-yr Rainfall=2.81"* Printed 6/21/2022

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			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64
#5	Secondary	961.00'	30.0" Round RCP_Round 30"
	-		L= 50.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 961.00' / 960.50' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf
#6	Device 5	962.05'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28)
			Head (feet) 0.00 5.00
			Width (feet) 5.00 5.00
#7	Device 6	957.50'	30.0" Round RCP_Round 30"
			L= 25.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 957.50' / 957.50' S= 0.0000 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections. Flow Area= 4.91 sf

Primary OutFlow Max=10.47 cfs @ 12.46 hrs HW=962.56' TW=0.00' (Dynamic Tailwater)

- -1=RCP_Round 30" (Passes 10.47 cfs of 13.19 cfs potential flow)
 - **2=Custom Weir/Orifice** (Weir Controls 10.47 cfs @ 3.02 fps)

3=RCP_Round 30" (Passes 10.47 cfs of 29.57 cfs potential flow)

Secondary OutFlow Max=6.05 cfs @ 12.46 hrs HW=962.56' TW=0.00' (Dynamic Tailwater)
5=RCP_Round 30" (Passes 6.05 cfs of 13.19 cfs potential flow)
6=Custom Weir/Orifice (Weir Controls 6.05 cfs @ 2.35 fps)
7=RCP Round 30" (Passes 6.05 cfs of 16.96 cfs potential flow)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=961.00' TW=0.00' (Dynamic Tailwater) **4=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 100P: Basin 100



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 121139-Creekside 5-27-2022-Proposed

 MSE 24-hr 3
 2-yr Rainfall=2.81"

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Summary for Pond 200P: Basin 200

Inflow Are	a =	4.642 ac, 4	1.66% Impervious,	Inflow Depth = 1.57" for 2-yr event
Inflow	=	11.21 cfs @	12.18 hrs, Volume	= 0.609 af
Outflow	=	1.67 cfs @	12.66 hrs, Volume	= 0.605 af, Atten= 85%, Lag= 28.7 min
Primary	=	1.67 cfs @	12.66 hrs, Volume	= 0.605 af
Routed	d to Link	P-Creek : Pro	posed Creek	
Secondar	y =	0.00 cfs @	0.00 hrs, Volume	= 0.000 af
Routed	to Link	P-Creek : Pro	posed Creek	

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 962.00' Surf.Area= 0.480 ac Storage= 1.681 af Peak Elev= 962.64' @ 12.66 hrs Surf.Area= 0.515 ac Storage= 1.998 af (0.318 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 266.3 min (1,071.6 - 805.4)

Volume	Invert	Avail.Stora	age Stora	age Description
#1	952.00'	4.760	af Cust	tom Stage Data (Prismatic)Listed below (Recalc)
Elevatio	on Surf.Ar	ea In	c.Store	Cum.Store
(fee	et) (acre	es) (ac	re-feet)	(acre-feet)
952.0	0.0	23	0.000	0.000
954.0	0.0	59	0.081	0.081
956.0	0.1	10	0.168	0.250
958.0	0.1	83	0.293	0.543
960.0	0.20	67	0.451	0.994
961.0	0.3	13	0.290	1.284
962.0	0 0.4	80	0.397	1.681
964.0	0 0.5	89	1.069	2.750
965.0	0.6	46	0.618	3.367
966.0	0 0.7	02	0.674	4.042
967.0	0 0.73	35	0.719	4.760
Device	Routing	Invert	Outlet De	evices
#1	Primary	962.00'	15.0" Ro	ound RCP Round 15"
	,		L= 25.0'	RCP, groove end projecting, Ke= 0.200
			Inlet / Ou	itlet Invert= 962.00' / 961.50' S= 0.0200 '/' Cc= 0.900
			n= 0.013	Concrete pipe, bends & connections, Flow Area= 1.23 sf
#2	Device 1	962.00'	Custom	Weir/Orifice, Cv= 2.62 (C= 3.28)
			Head (fee	et) 0.00 1.00 1.00 8.00
			Width (fe	et) 1.00 1.00 5.00 5.00
#3	Device 2	959.75'	15.0" Ro	ound RCP_Round 15"
			L= 25.0'	RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Ou	itlet Invert= 959.75' / 959.75' S= 0.0000 '/' Cc= 0.900
			n= 0.013	Concrete pipe, bends & connections, Flow Area= 1.23 sf
#4	Secondary	966.00'	25.0' lon	g x 10.0' breadth Broad-Crested Rectangular Weir
			Head (fee	et) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (Er	nglish) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=1.67 cfs @ 12.66 hrs HW=962.64' TW=0.00' (Dynamic Tailwater) 1=RCP_Round 15" (Passes 1.67 cfs of 2.02 cfs potential flow) 2=Custom Weir/Orifice (Weir Controls 1.67 cfs @ 2.62 fps) 3=RCP_Round 15" (Passes 1.67 cfs of 4.72 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=962.00' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Hydrograph 12 - Inflow 11.21 cfs - Outflow 11 Primary Inflow Area=4.642 ac Secondary 10 Peak Elev=962.64' 9 Storage=1.998 af 8 7 Flow (cfs) 6 5-4-3-1.67 cfs 2 1-0.00 cfs 0 -Ó 10 20 30 40 50 60 70 80 90 100 110 120 130 140 150 160 Time (hours)

Pond 200P: Basin 200

00-121186-PROPOSED- 05-26-22 121139-Creekside 5-27-2022-Proposed MSE 24-hr 3 2-yr Rainfall=2.81" Prepared by {enter your company name here} Printed 6/21/2022 HydroCAD® 10.10-7a s/n 00590 © 2021 HydroCAD Software Solutions LLC Page 35

Summary for Pond 300P: Basin 300

Inflow Area	a =	1.894 ac, 4	18.85% Imp	ervious,	Inflow	Depth =	1.73"	for 2-yr	event	
Inflow	=	5.31 cfs @	12.17 hrs,	Volume	=	0.273	af			
Outflow	=	2.00 cfs @	12.35 hrs,	Volume	=	0.272	af, Att	en= 62%,	Lag=	10.6 min
Primary	=	2.00 cfs @	12.35 hrs,	Volume	=	0.272	af		-	
Routed	to Link F	P-Creek : Pro	posed Cree	ek						
Secondary	=	0.00 cfs @	0.00 hrs,	Volume	=	0.000	af			
Routed	to Link F	P-Creek : Pro	posed Cree	ek						

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 966.00' Surf.Area= 0.160 ac Storage= 0.317 af Peak Elev= 966.64' @ 12.35 hrs Surf.Area= 0.184 ac Storage= 0.427 af (0.110 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 117.3 min (915.8 - 798.5)

)
0.900
= 1.23 sf
0.900
= 1.23 sf
Neir

Primary OutFlow Max=2.00 cfs @ 12.35 hrs HW=966.64' TW=0.00' (Dynamic Tailwater) 1=RCP_Round 15" (Passes 2.00 cfs of 2.03 cfs potential flow) 2=Custom Weir/Orifice (Weir Controls 2.00 cfs @ 1.85 fps) 3=RCP_Round 15" (Passes 2.00 cfs of 4.73 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=966.00' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)



Pond 300P: Basin 300

Summary for Link P-Creek: Proposed Creek

Inflow A	rea =	32.188 ac, 3	3.10% Imper	vious, Inflow	Depth = 1.49"	for 2-yr event
Inflow	=	27.36 cfs @	12.40 hrs, V	/olume=	3.996 af	
Primary	=	27.36 cfs @	12.40 hrs, V	/olume=	3.996 af, At	ten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link P-Creek: Proposed Creek

Summary for Link P-South: Proposed South

Inflow A	Area	=	4.438 ac,	7.41% Impervious	, Inflow Depth = 1	.17" for 2-yr event
Inflow		=	10.85 cfs @	12.12 hrs, Volum	e= 0.432 af	-
Primary	у	=	10.85 cfs @	12.12 hrs, Volum	e= 0.432 af	, Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link P-South: Proposed South

Summary for Link P-West: Proposed West

Inflow A	Area	=	3.590 ac,	18.01% Impe	ervious,	Inflow Dep	oth =	1.30"	' for 2	2-yr event	
Inflow	:	=	9.85 cfs @	12.11 hrs,	Volume	= (0.387 a	af			
Primary	y :	=	9.85 cfs @	12.11 hrs,	Volume	= (0.387	af, A	tten= 09	%, Lag= 0.′	1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link P-West: Proposed West

00-121186-PROPOS Prepared by {enter yo	SED- 05-26-22 ur company name	here}	1	121139- MSE	-Creeks E 24-hr	side 5- 3 10	27-2022 - <i>yr Rail</i> Printed	2-Pro <i>nfall=</i> 6/2 <i>^</i>	posed =4.19" 1/2022
<u>HydroCAD® 10.10-7a_s/n</u>	00590 © 2021 Hydro	oCAD Software	e Solutions	LLC				Pa	<u>age 40</u>
Reach ro	Time span=0.00-16 Runoff by SCS TF outing by Sim-Route	80.00 hrs, dt= R-20 method, e method - P	0.001 hrs, UH=SCS, ond routin	16000 ² Weight g by Sii	1 points ed-CN m-Rout	s e metł	nod		
Subcatchment1S: N-C	Catchment Flow Length=975'	Runoff Area= Slope=0.0240	718,098 sf '/' Tc=15.:	43.629 3 min (% Imper CN=88	vious Runof	Runoff f=60.65	Depth cfs 3	⊧=2.91" .992 af
Subcatchment2S: Eas	t Catchment Flow Length=670'	Runoff Area= Slope=0.0310	202,210 sf '/' Tc=10.3	41.669 3 min (% Imper CN=87	vious Runof	Runoff f=19.69	Depth cfs 1	=2.81" .088 af
Subcatchment3S: Sou	th Catchment Flow Length=442	Runoff Area 2' Slope=0.01	=82,515 sf 30 '/' Tc=9	48.859 9.0 min	% Imper CN=89	vious Runc	Runoff	Depth cfs 0	=3.00" .474 af
Subcatchment4S: Wes	St Catchment Flow Length=200'	Runoff Area= Slope=0.065	156,360 sf) '/' Tc=3.	18.019 1 min (% Imper CN=83	vious Runof	Runoff f=18.16	Depth cfs 0	⊧=2.45" .733 af
Subcatchment 5S: S-C	Catchment Flow Length=150	Runoff Are)' Slope=0.09	a=75,496 s 30 '/' Tc=2	sf 9.119 2.2 min	% Imper CN=81	vious Runc	Runoff	Depth cfs 0	⊧=2.28" .330 af
Subcatchment6S: Sou	th Catchment Flow Length=220'	Runoff Area Slope=0.064	=193,325 s) '/' Tc=3.0	sf 7.419 6 min (% Imper CN=81	vious Runof	Runoff f=20.78	Depth cfs 0	=2.28" .844 af
Subcatchment7S: Cre	ek Catchment Flow Length=850'	Runoff Area Slope=0.0260	=323,811 s '/' Tc=17.:	sf 6.029 3 min (% Imper CN=80	vious Runof	Runoff f=19.75	Depth cfs 1	⊧=2.20" .363 af
Pond 100P: Basin 100 Primary=21.64 cfs 3.066 af	Secondary=18.72 cf	Peak Elev= s 0.921 af Te	963.14' St rtiary=0.00	orage=4 cfs 0.0	.026 af 00 af (Inflow Dutflow	/=60.65 /=40.36	cfs 3 cfs 3	.992 af .987 af
Pond 200P: Basin 200	Primary=4.00 cfs	Peak Elev= 1.084 af Sec	963.08' St ondary=0.0	orage=2)0 cfs 0.	2.232 af .000 af	Inflow Outflo	v=19.69 w=4.00	cfs 1 cfs 1	.088 af .084 af
Pond 300P: Basin 300	Primary=3.90 cfs	Peak Elev 0.473 af Sec	=966.97' S ondary=0.0	Storage= 00 cfs 0.	0.489 a .000 af	f Inflo Outflo	w=9.00 w=3.90	cfs 0 cfs 0	.474 af .473 af
Link P-Creek: Propose	d Creek				F	Inflow Primary	/=66.46 /=66.46	cfs 7 cfs 7	.236 af .236 af
Link P-South: Propose	d South				F	Inflow Primary	/=20.78 /=20.78	cfs 0 cfs 0	.844 af .844 af
Link P-West: Proposed	lWest				F	Inflow Primary	/=18.16 /=18.16	cfs 0 cfs 0	.733 af .733 af

Total Runoff Area = 40.216 ac Runoff Volume = 8.823 af Average Runoff Depth = 2.63" 71.08% Pervious = 28.585 ac 28.92% Impervious = 11.631 ac

Summary for Subcatchment 1S: N-C Catchment

Runoff = 60.65 cfs @ 12.22 hrs, Volume= 3.992 af, Depth= 2.91" Routed to Pond 100P : Basin 100

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

Ar	rea (sf)	CN	Description					
4	04,877	80	>75% Grass cover, Good, HSG D					
3	13,221	98	Paved parking, HSG D					
	0	79	Woods, Fair, HSG D					
7	18,098	88	Weighted A	verage				
404,877 56.38% Pervious Area								
3	13,221		43.62% Imp	pervious Ar	ea			
Tc	Length	Slope	e Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)				
15.3	975	0.0240) 1.06		Lag/CN Method,			
					· J			

Subcatchment 1S: N-C Catchment



Hydrograph

Summary for Subcatchment 2S: East Catchment

Runoff = 19.69 cfs @ 12.18 hrs, Volume= 1.088 af, Depth= 2.81" Routed to Pond 200P : Basin 200

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

Α	rea (sf)	CN	Description						
1	17,965	80	>75% Grass cover, Good, HSG D						
	84,245	98	Paved parking, HSG D						
	0	79	<u>Noods, Fai</u>	r, HSG D					
2	02,210	87	Neighted A	verage					
1	17,965		58.34% Pei	vious Area	3				
	84,245		41.66% Imp	pervious Are	rea				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
10.3	670	0.0310	1.08		Lag/CN Method,				
					-				

Subcatchment 2S: East Catchment



Summary for Subcatchment 3S: South Catchment

Runoff = 9.00 cfs @ 12.16 hrs, Volume= 0.474 af, Depth= 3.00" Routed to Pond 300P : Basin 300

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

rea (sf)	CN	Description						
42,205	80	>75% Grass cover, Good, HSG D						
40,310	98	Paved parking, HSG D						
0	79	Woods, Fair, HSG D						
82,515 89 Weighted Average								
42,205 51.15% Pervious Area								
40,310		48.85% Imp	pervious Ar	ea				
Length	Slope	e Velocity	Capacity	Description				
(feet)	(ft/ft	(ft/sec)	(cfs)					
442	0.0180	0.82		Lag/CN Method,				
	rea (sf) 42,205 40,310 0 82,515 42,205 40,310 Length (feet) 442	trea (sf) CN 42,205 80 40,310 98 0 79 82,515 89 42,205 40,310 Length Slope (feet) (ft/ft) 442 0.0180	trea (sf) CN Description 42,205 80 >75% Gras 40,310 98 Paved park 0 79 Woods, Fai 82,515 89 Weighted A 42,205 51.15% Per 40,310 48.85% Imp Length Slope Velocity (feet) (ft/ft) (ft/sec) 442 0.0180 0.82	trea (sf)CNDescription42,20580>75% Grass cover, Go40,31098Paved parking, HSG D079Woods, Fair, HSG D82,51589Weighted Average42,20551.15% Pervious Area40,31048.85% Impervious Area40,310SlopeVelocityLengthSlopeVelocity(feet)(ft/ft)(ft/sec)4420.01800.82	trea (sf)CNDescription42,20580>75% Grass cover, Good, HSG D40,31098Paved parking, HSG D079Woods, Fair, HSG D82,51589Weighted Average42,20551.15% Pervious Area40,31048.85% Impervious AreaLengthSlopeVelocity(feet)(ft/ft)(ft/sec)4420.01800.82Lag/CN Method,			

Subcatchment 3S: South Catchment



Summary for Subcatchment 4S: West Catchment

Runoff = 18.16 cfs @ 12.11 hrs, Volume= 0.733 af, Depth= 2.45" Routed to Link P-West : Proposed West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

Area	sf) (CN E	Description						
109,4	17	80 >	>75% Grass cover, Good, HSG D						
28,1	63	98 F	Paved parking, HSG D						
18,7	80	79 V	Woods, Fair, HSG D						
156,3	60	83 V	Weighted Average						
128,1	128,197 81.99% Pervious Area								
28,1	63	1	8.01% Imp	ervious Are	ea				
Tc Lei	ngth	Slope	Velocity	Capacity	Description				
<u>(min)</u> (f	eet)	(ft/ft)	(ft/sec)	(cfs)					
3.1	200 0	0.0650	1.07		Lag/CN Method,				
					-				

Subcatchment 4S: West Catchment



Summary for Subcatchment 5S: S-C Catchment

8.47 cfs @ 12.11 hrs, Volume= 0.330 af, Depth= 2.28" Runoff = Routed to Link P-Creek : Proposed Creek

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

Α	rea (sf)	CN	Description						
	37,344	80	>75% Grass cover, Good, HSG D						
	6,876	98	Paved parking, HSG D						
	31,276	79	Woods, Fair, HSG D						
	75,496	81	Weighted A	verage					
	68,620		90.89% Pei	vious Area					
	6,876		9.11% Impe	ervious Area	a				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
2.2	150	0.0930	1.13		Lag/CN Method,				
					-				

Subcatchment 5S: S-C Catchment



Hydrograph

Summary for Subcatchment 6S: South Catchment

Runoff = 20.78 cfs @ 12.12 hrs, Volume= 0.844 af, Depth= 2.28" Routed to Link P-South : Proposed South

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

Α	rea (sf)	CN	Description								
1	54,331	80	>75% Gras	s cover, Go	od, HSG D						
	14,333	98	Paved park	ived parking, HSG D							
	24,661	79	Woods, Fai	ods, Fair, HSG D							
1	93,325	81	Weighted Average								
1	78,992	9	92.59% Pei	vious Area							
	14,333		7.41% Impe	ervious Area	a						
Tc	Length	Slope	Velocity	Capacity	Description						
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
3.6	220	0.0640	1.01		Lag/CN Method,						
					-						

Subcatchment 6S: South Catchment



Summary for Subcatchment 7S: Creek Catchment

Runoff = 19.75 cfs @ 12.26 hrs, Volume= 1.363 af, Depth= 2.20" Routed to Link P-Creek : Proposed Creek

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 10-yr Rainfall=4.19"

A	rea (sf)	CN	Description								
1	14,917	80	>75% Gras	5% Grass cover, Good, HSG D							
	19,500	98	Paved park	aved parking, HSG D							
1	89,394	79	Woods, Fai	ods, Fair, HSG D							
3	23,811	80	Weighted Average								
3	04,311		93.98% Per	vious Area	1						
	19,500		6.02% Impe	ervious Area	a						
Тс	Length	Slope	Velocity	Capacity	Description						
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
17.3	850	0.0260	0.82		Lag/CN Method,						
					-						

Subcatchment 7S: Creek Catchment



 00-121186-PROPOSED- 05-26-22
 121139-Creekside 5-27-2022-Proposed MSE 24-hr 3

 Prepared by {enter your company name here}
 MSE 24-hr 3
 10-yr Rainfall=4.19"

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Summary for Pond 100P: Basin 100

Inflow Area	=	16.485 ad	c, 43.62	2% Imp	ervious,	Inflow	Depth =	2.91"	for	10-yr	event	
Inflow	=	60.65 cfs	@ 12.	22 hrs,	Volume	=	3.992	af		-		
Outflow	=	40.36 cfs		37 hrs,	Volume	=	3.987	af, Atte	en= 3	3%, I	Lag= 8.7	min
Primary	=	21.64 cfs		37 hrs,	Volume	=	3.066	af				
Routed	to Link	P-Creek :	Propos	ed Cre	ek							
Secondary	=	18.72 cfs	@ 12.	37 hrs,	Volume	;=	0.921	af				
Routed	to Link	P-Creek :	Propos	ed Cre	ek							
Tertiary	=	0.00 cfs	@ 0.	00 hrs,	Volume	=	0.000	af				
Routed	to Link	P-Creek :	Propos	ed Cre	ek							

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 961.00' Surf.Area= 0.545 ac Storage= 2.752 af Peak Elev= 963.14' @ 12.37 hrs Surf.Area= 0.644 ac Storage= 4.026 af (1.273 af above start)

Plug-Flow detention time= 517.5 min calculated for 1.234 af (31% of inflow) Center-of-Mass det. time= 109.9 min (905.8 - 795.9)

Volume	Inver	Avail.Stor	age Stora	age Description
#1	951.00	7.65	5 af Cust	tom Stage Data (Prismatic)Listed below (Recalc)
Elovatio	n Surf	Aroa li	no Storo	Cum Store
	t) (a	ree) (a	re_feet)	(acre_feet)
051.0	<u>(a</u>	<u>(au</u>		
951.0).119).145	0.000	0.000
952.0), 140), 201	0.132	0.132
904.0		0.201	0.347	0.479
950.0		1.200	0.405	1 530
950.0 960 0		1.332	0.393	2 277
961.0) 545	0.730	2.217
962.0) 590	0.568	3 320
964.0	0 0) 685	1 275	4 595
965.0	0 0) 735	0 710	5 305
966.0	0 0	0.786	0.760	6.065
968.0	0 0	0.803	1.589	7.655
Device	Routing	Invert	Outlet De	evices
#1	Drimony	061.00'	30.0" Po	ound PCP. Bound 30"
π I	тппату	301.00	J = 50.0'	RCP groove end projecting $Ke= 0.200$
			Inlet / Our	itlet Invert= $961\ 00' / 960\ 50'$ S= $0\ 0100\ '/$ Cc= $0\ 900$
			n = 0.013	Concrete pipe, bends & connections Flow Area= 4.91 sf
#2	Device 1	961 00'	Custom	Weir/Orifice $Cv = 2.62$ ($C = 3.28$)
=			Head (fee	et) 0.00 1.05 1.05 8.00
			Width (fee	eet) 0.85 0.85 5.00 5.00
#3	Device 2	957.50'	30.0" Ro	ound RCP Round 30"
			L= 25.0'	RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Ou	utlet Invert= 957.50' / 957.50' S= 0.0000 '/' Cc= 0.900
			n= 0.013	Concrete pipe, bends & connections, Flow Area= 4.91 sf
#4	Tertiary	966.00'	15.0' long	ig x 10.0' breadth Broad-Crested Rectangular Weir
	-		Head (fee	et) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60

121139-Creekside 5-27-2022-Proposed MSE 24-hr 3 10-yr Rainfall=4.19" Printed 6/21/2022

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			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64
#5	Secondary	961.00'	30.0" Round RCP_Round 30"
	-		L= 50.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 961.00' / 960.50' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf
#6	Device 5	962.05'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28)
			Head (feet) 0.00 5.00
			Width (feet) 5.00 5.00
#7	Device 6	957.50'	30.0" Round RCP_Round 30"
			L= 25.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 957.50' / 957.50' S= 0.0000 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf

Primary OutFlow Max=21.64 cfs @ 12.37 hrs HW=963.14' TW=0.00' (Dynamic Tailwater) 1=RCP_Round 30" (Barrel Controls 21.64 cfs @ 6.49 fps) -2=Custom Weir/Orifice (Passes 21.64 cfs of 24.28 cfs potential flow)

3=RCP_Round 30" (Passes 21.64 cfs of 34.60 cfs potential flow)

Secondary OutFlow Max=18.72 cfs @ 12.37 hrs HW=963.14' TW=0.00' (Dynamic Tailwater) 5=RCP_Round 30" (Passes 18.72 cfs of 21.64 cfs potential flow) **6=Custom Weir/Orifice** (Weir Controls 18.72 cfs @ 3.42 fps) **7=RCP Round 30**" (Passes 18.72 cfs of 24.71 cfs potential flow)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=961.00' TW=0.00' (Dynamic Tailwater) -4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 100P: Basin 100



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 121139-Creekside 5-27-2022-Proposed MSE 24-hr 3 10-yr Rainfall=4.19"

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Summary for Pond 200P: Basin 200

4.642 ac, 41.66% Impervious, Inflow Depth = 2.81" for 10-yr event Inflow Area = Inflow 19.69 cfs @ 12.18 hrs, Volume= = 1.088 af 4.00 cfs @ 12.55 hrs, Volume= Outflow 1.084 af, Atten= 80%, Lag= 22.2 min = Primary = 4.00 cfs @ 12.55 hrs, Volume= 1.084 af Routed to Link P-Creek : Proposed Creek Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Routed to Link P-Creek : Proposed Creek

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 962.00' Surf.Area= 0.480 ac Storage= 1.681 af Peak Elev= 963.08' @ 12.55 hrs Surf.Area= 0.539 ac Storage= 2.232 af (0.552 af above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 199.0 min (992.8 - 793.8)

Volume	Invert	Avail.Stora	age Stora	age Description
#1	952.00'	4.760) af Cus	tom Stage Data (Prismatic)Listed below (Recalc)
Elevatio	n Surf.Are	ea In	c.Store	Cum.Store
(feet	t) (acre	s) (ac	re-feet)	(acre-feet)
952.0	0 0.02	23	0.000	0.000
954.0	0 0.05	59	0.081	0.081
956.0	0 0.11	10	0.168	0.250
958.0	0 0.18	33	0.293	0.543
960.0	0 0.26	67	0.451	0.994
961.0	0 0.31	13	0.290	1.284
962.0	0 0.48	30	0.397	1.681
964.0	0 0.58	39	1.069	2.750
965.0	0 0.64	16	0.618	3.367
966.0	0 0.70)2	0.674	4.042
967.0	0 0.73	35	0.719	4.760
Device	Routing	Invert	Outlet D	evices
	Drimonu			evices
<i>#</i> I	Primary	962.00	1 5.0 K	PCP groove and projecting. Ke= 0.200
			L- 23.0 Inlet / Or	(1000) (1000) (100) $(1$
			n = 0.013	Concrete nine, bends & connections, Flow Area = 1.23 sf
#2	Device 1	962 00'	Custom	Weir/Orifice $C_{v=2}$ 62 (C= 3.28)
<i>"'</i>	Device 1	002.00	Head (fe	$et = 0.00 \pm 0.00 \pm 0.00 \pm 0.000$
			Width (fe	et) 1.00 1.00 5.00 5.00
#3	Device 2	959.75'	15.0" R	ound RCP Round 15"
			L= 25.0'	RCP, end-section conforming to fill. Ke= 0.500
			Inlet / Ou	utlet Invert= 959.75' / 959.75' S= 0.0000 '/' Cc= 0.900
			n= 0.013	3 Concrete pipe, bends & connections, Flow Area= 1.23 sf
#4	Secondary	966.00'	25.0' lon	ng x 10.0' breadth Broad-Crested Rectangular Weir
	,		Head (fe	et) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (Ei	nglish) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=4.00 cfs @ 12.55 hrs HW=963.08' TW=0.00' (Dynamic Tailwater) 1=RCP_Round 15" (Passes 4.00 cfs of 4.58 cfs potential flow) 2=Custom Weir/Orifice (Weir Controls 4.00 cfs @ 2.83 fps) -3=RCP_Round 15" (Passes 4.00 cfs of 6.15 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=962.00' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 200P: Basin 200



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Summary for Pond 300P: Basin 300

Inflow Area	a =	1.894 ac, 4	48.85% Impe	ervious,	Inflow Depth =	3.00"	for 1	10-yr eve	ent		
Inflow	=	9.00 cfs @	12.16 hrs,	Volume	= 0.474	af		-			
Outflow	=	3.90 cfs @	12.31 hrs,	Volume	= 0.473	af, Atte	en= 57	7%, Lag	= 9.1 min		
Primary	=	3.90 cfs @	12.31 hrs,	Volume	= 0.473	af		-			
Routed	to Link	P-Creek : Pro	oposed Cree	k							
Secondary	=	0.00 cfs @	0.00 hrs,	Volume	= 0.000	af					
Routed	Routed to Link P-Creek : Proposed Creek										

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 966.00' Surf.Area= 0.160 ac Storage= 0.317 af Peak Elev= 966.97' @ 12.31 hrs Surf.Area= 0.196 ac Storage= 0.489 af (0.172 af above start)

Plug-Flow detention time= 418.8 min calculated for 0.157 af (33% of inflow) Center-of-Mass det. time= 86.9 min (874.3 - 787.5)

Volume	Invert A	vail.Stora	ge Stora	ge Description
#1	958.00'	1.594	af Custo	om Stage Data (Prismatic)Listed below (Recalc)
Elevatio	n Surf.Area	Inc	c.Store	Cum.Store
(feet) (acres)	(acr	e-feet)	(acre-feet)
958.00	0.003		0.000	0.000
960.00	0.012		0.015	0.015
962.00	0.029	1	0.041	0.056
964.00	0.053	1	0.083	0.139
965.00	0.071		0.062	0.201
966.00	0.160	1	0.116	0.317
968.00	0.234		0.394	0.711
970.00	0.316		0.550	1.261
971.00	0.351		0.333	1.594
Device	Routing	Invert	Outlet Dev	vices
#1	Primary	966.00'	15.0" Ro	und RCP_Round 15"
			L= 25.0'	RCP, groove end projecting, Ke= 0.200
			Inlet / Out	let Invert= 966.00' / 965.50' S= 0.0200 '/' Cc= 0.900
			n= 0.013	Concrete pipe, bends & connections, Flow Area= 1.23 sf
#2	Device 1	966.00'	Custom V	Neir/Orifice, Cv= 2.62 (C= 3.28)
			Head (fee	t) 0.00 0.50 0.50 5.00
			Width (fee	et) 0.75 0.75 5.00 5.00
#3	Device 2	963.75	15.0" Ro	und RCP_Round 15"
			$L= 30.0^{\circ}$	RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Out	let Invert= 963.75' / 963.75' S= 0.0000 7' Cc= 0.900
	0	070 001	n= 0.013	Concrete pipe, bends & connections, Flow Area= 1.23 st
#4	Secondary	970.00	25.0° IONG	
			∪oer. (Ehg	glish) 2.49 2.50 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=3.90 cfs @ 12.31 hrs HW=966.97' TW=0.00' (Dynamic Tailwater) 1=RCP_Round 15" (Barrel Controls 3.90 cfs @ 5.27 fps) 2=Custom Weir/Orifice (Passes 3.90 cfs of 6.81 cfs potential flow)

Gases of the second se

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=966.00' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)



Pond 300P: Basin 300

Summary for Link P-Creek: Proposed Creek

Inflow Are	a =	32.188 ac, 3	3.10% Impe	ervious,	Inflow Depth =	2.7	'0" for	10-yr event	
Inflow	=	66.46 cfs @	12.32 hrs,	Volume	= 7.236	af			
Primary	=	66.46 cfs @	12.32 hrs,	Volume	= 7.236	af,	Atten= 0	%, Lag= 0.1 mir	า

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link P-Creek: Proposed Creek

Summary for Link P-South: Proposed South

Inflow /	Area	=	4.438 ac,	7.41% Impervious,	Inflow Depth = 2.	28" for 10-yr event
Inflow		=	20.78 cfs @	12.12 hrs, Volume	e 0.844 af	
Primary	у	=	20.78 cfs @	12.12 hrs, Volume	e= 0.844 af,	Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs

Link P-South: Proposed South



Summary for Link P-West: Proposed West

Inflow /	Area	=	3.590 ac,	18.01% Impe	ervious,	Inflow Depth	= 2.4	5" for	10-yr event
Inflow		=	18.16 cfs @	12.11 hrs,	Volume	= 0.7	'33 af		
Primar	у	=	18.16 cfs @	12.11 hrs,	Volume	= 0.7	'33 af, .	Atten= C)%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link P-West: Proposed West

00-121186-PROPO	SED- 05-26-22			12	21139-0 MSE 2	Creeks 24-hr (side 5-2 3 100	27-202: -yr Rai	2-Pro <i>nfall=</i>	posed =7.47"
Prepared by {enter yo	ur company name	here}	0					Printed	6/21	1/2022
HydroCAD® 10.10-7a s/r	1 00590 © 2021 Hydr	OCAD SOTT	vare So	iutions L	LC				Pa	<u>age 57</u>
Reach ro	Time span=0.00-10 Runoff by SCS TF outing by Sim-Route	60.00 hrs, R-20 metho e method	dt=0.00 od, UH= - Pond)1 hrs, 1 =SCS, V routing	60001 Veighte by Sin	points ed-CN n-Rout	s te metł	nod		
Subcatchment1S: N-C	Catchment Flow Length=975'	Runoff Ar Slope=0.024	ea=718 40 '/' T	,098 sf c=15.3 m	43.62% nin CN	impei I=88 I	rvious Runoff=	Runoff 122.12	Depth cfs 8	1=6.05" .312 af
Subcatchment2S: Eas	t Catchment Flow Length=670'	Runoff Ar Slope=0.03	ea=202 310 '/'	,210 sf Tc=10.3	41.66% min C	b Impei N=87	rvious Runofi	Runoff f=39.98	Depth cfs 2	1=5.93" 296 af
Subcatchment 3S: Sou	Ith Catchment Flow Length=442'	Runoff A Slope=0.0	vrea=82 0180 '/'	,515 sf Tc=9.0	48.85% min C	₀ Impei N=89	rvious Runof	Runoff f=17.73	Depth cfs 0	1=6.17" .974 af
Subcatchment4S: We	st Catchment Flow Length=200'	Runoff Ar Slope=0.0	ea=156 0650 '/'	,360 sf Tc=3.1	18.01% min C	₀ Impei N=83	rvious Runof	Runoff f=38.54	Depth cfs 1	1=5.47" .637 af
Subcatchment 5S: S-C	Catchment Flow Length=150	Runoff Slope=0.0	Area=7)930 '/'	5,496 sf Tc=2.2	9.11% min C	₀ Impei N=81	rvious Runof	Runoff f=18.38	Depth cfs 0	n=5.24" .757 af
Subcatchment6S: Sou	ith Catchment Flow Length=220'	Runoff A Slope=0.0	vrea=19 0640 '/'	3,325 sf Tc=3.6	7.41% min C	₀ Impei N=81	rvious Runof	Runoff f=45.56	Depth cfs 1	1=5.24" .939 af
Subcatchment7S: Cre	ek Catchment Flow Length=850'	Runoff A Slope=0.02	vrea=32 260 '/'	3,811 sf Tc=17.3	6.02% min C	₀ Impei N=80	rvious Runofi	Runoff f=45.38	Depth cfs 3	1=5.13" .178 af
Pond 100P: Basin 100 Primary=37.17 cfs 5.617 af	Secondary=36.85 c	Peak Ele fs 2.690 af	v=964.4 Tertiar	8' Stora y=0.00 c	age=4.9 cfs 0.00	30 af)0 af (Inflow= Outflow	=122.12 =74.01	cfs 8 cfs 8	.312 af .307 af
Pond 200P: Basin 200	Primary=8.50 cfs	Peak El 2.292 af	ev=964 Seconda	.08' Stor ary=0.00	rage=2. cfs 0.0	796 af 000 af	Inflow Outflo	/=39.98 w=8.50	cfs 2 cfs 2	296 af .292 af
Pond 300P: Basin 300	Primary=7.13 cfs	Peak El 0.973 af	ev=967 Seconda	.68' Stor ary=0.00	rage=0. cfs 0.0	638 af 000 af	Inflow Outflo	/=17.73 w=7.13	cfs 0 cfs 0	.974 af .973 af
Link P-Creek: Propose	d Creek					lı Pri	nflow=1 mary=1	33.87 c 33.87 c	fs 15 fs 15	.507 af .507 af
Link P-South: Propose	ed South					I	Inflow Primary	/=45.56 /=45.56	cfs 1 cfs 1	.939 af .939 af
Link P-West: Proposed	dWest					I	Inflow Primary	/=38.54 /=38.54	cfs 1 cfs 1	.637 af .637 af

Total Runoff Area = 40.216 ac Runoff Volume = 19.094 af Average Runoff Depth = 5.70" 71.08% Pervious = 28.585 ac 28.92% Impervious = 11.631 ac

Summary for Subcatchment 1S: N-C Catchment

Runoff = 122.12 cfs @ 12.22 hrs, Volume= 8.312 af, Depth= 6.05" Routed to Pond 100P : Basin 100

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

Area (sf)		CN	Description			
404,877		80	>75% Grass cover, Good, HSG D			
313,221		98	Paved parking, HSG D			
0		79	Woods, Fair, HSG D			
718,098		88	Weighted Average			
404,877			56.38% Pervious Area			
313,221			43.62% Imp	pervious Are		
_						
Tc	Length	Slope	Velocity	Capacity	Description	
<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)		
15.3	975	0.0240	1.06		Lag/CN Method,	

Subcatchment 1S: N-C Catchment


Summary for Subcatchment 2S: East Catchment

Runoff = 39.98 cfs @ 12.18 hrs, Volume= 2.296 af, Depth= 5.93" Routed to Pond 200P : Basin 200

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

A	rea (sf)	CN	Description							
1	17,965	80	>75% Gras	s cover, Go	ood, HSG D					
	84,245	98	Paved park	aved parking, HSG D						
	0	79	Woods, Fai	ods, Fair, HSG D						
2	02,210	87	Weighted A	verage						
1	17,965	:	58.34% Pei	vious Area						
	84,245		41.66% Imp	pervious Are	ea					
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
10.3	670	0.0310	1.08		Lag/CN Method,					

Subcatchment 2S: East Catchment



Summary for Subcatchment 3S: South Catchment

Runoff = 17.73 cfs @ 12.16 hrs, Volume= 0.974 af, Depth= 6.17" Routed to Pond 300P : Basin 300

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

Α	rea (sf)	CN	Description						
	42,205	80	>75% Gras	s cover, Go	ood, HSG D				
	40,310	98	Paved park	aved parking, HSG D					
	0	79	Woods, Fai	/oods, Fair, HSG D					
	82,515	89	Weighted A	verage					
	42,205		51.15% Pei	vious Area					
	40,310 48.85% Impervious Are				ea				
Тс	Length	Slope	e Velocity	Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft) (ft/sec)	(cfs)					
9.0	442	0.0180	0.82		Lag/CN Method,				

Subcatchment 3S: South Catchment



Hydrograph

Summary for Subcatchment 4S: West Catchment

Runoff = 38.54 cfs @ 12.11 hrs, Volume= 1.637 af, Depth= 5.47" Routed to Link P-West : Proposed West

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

Area (sf)	CN	Description	Description						
109,417	80	>75% Gras	s cover, Go	ood, HSG D					
28,163	98	Paved park	aved parking, HSG D						
18,780	79	Woods, Fai	oods, Fair, HSG D						
156,360	83	Weighted A	verage						
128,197 81.99% Pervious Area									
28,163 18.01% Impervious Area				ea					
Tc Length	Slop	e Velocity	Capacity	Description					
(min) (feet)	(ft/f	t) (ft/sec)	(cfs)						
3.1 200	0.065	0 1.07		Lag/CN Method,					

Subcatchment 4S: West Catchment



Summary for Subcatchment 5S: S-C Catchment

Runoff = 18.38 cfs @ 12.11 hrs, Volume= 0.75 Routed to Link P-Creek : Proposed Creek

0.757 af, Depth= 5.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

A	rea (sf)	CN	Description							
	37,344	80	80 >75% Grass cover, Good, HSG D							
	6,876	98	Paved park	aved parking, HSG D						
	31,276	79	Woods, Fai	oods, Fair, HSG D						
	75,496	81	Weighted A	verage						
	1									
	6,876	9	9.11% Impe	ervious Area	a					
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
2.2	150	0.0930	1.13		Lag/CN Method,					
					-					

Subcatchment 5S: S-C Catchment



Summary for Subcatchment 6S: South Catchment

Runoff = 45.56 cfs @ 12.11 hrs, Volume= 1.939 af, Depth= 5.24" Routed to Link P-South : Proposed South

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

Α	rea (sf)	CN	Description							
1	54,331	80	>75% Gras	s cover, Go	od, HSG D					
	14,333	98	Paved park	ing, HSG D						
	24,661	79	Woods, Fai	oods, Fair, HSG D						
193,325 81 Weighted Average										
178,992 92.59% Pervious Area			vious Area							
	14,333 7.41% Impervious Area				a					
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
3.6	220	0.0640	1.01		Lag/CN Method,					
					=					

Subcatchment 6S: South Catchment



Summary for Subcatchment 7S: Creek Catchment

Runoff = 45.38 cfs @ 12.25 hrs, Volume= Routed to Link P-Creek : Proposed Creek

3.178 af, Depth= 5.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs MSE 24-hr 3 100-yr Rainfall=7.47"

Α	rea (sf)	CN I	Description							
1	14,917	80 :	>75% Gras	s cover, Go	bod, HSG D					
	19,500	98	Paved park	ing, HSG D)					
1	89,394	79	Noods, Fai	oods, Fair, HSG D						
323,811 80 Weighted Average										
304,311			93.98% Pervious Area							
	19,500 6.02% Impervious Area				а					
Тс	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
17.3	850	0.0260	0.82		Lag/CN Method,					
					-					

Subcatchment 7S: Creek Catchment



Hydrograph

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Summary for Pond 100P: Basin 100

Inflow Area	ı =	16.485 ac,	43.62% Imp	ervious,	Inflow Dept	th =	6.05"	for	100-yı	event	
Inflow	=	122.12 cfs @) 12.22 hrs,	Volume	= 8.	.312 a	af		-		
Outflow	=	74.01 cfs @) 12.39 hrs,	Volume	= 8.	.307 a	af, Atte	n= 3	9%, L	_ag= 9.7	min
Primary	=	37.17 cfs @) 12.39 hrs,	Volume	= 5.	.617 a	af				
Routed	to Linł	< P-Creek : P	roposed Cre	ek							
Secondary	=	36.85 cfs @) 12.39 hrs,	Volume	= 2.	.690 a	af				
Routed	to Linł	P-Creek : P	roposed Cre	ek							
Tertiary	=	0.00 cfs @) 0.00 hrs,	Volume	= 0.	.000 a	af				
Routed	to Linł	< P-Creek : P	roposed Cre	ek							

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 961.00' Surf.Area= 0.545 ac Storage= 2.752 af Peak Elev= 964.48' @ 12.39 hrs Surf.Area= 0.709 ac Storage= 4.930 af (2.178 af above start)

Plug-Flow detention time= 212.2 min calculated for 5.555 af (67% of inflow) Center-of-Mass det. time= 74.5 min (855.9 - 781.5)

Volume	Invert	Avail.Stora	ge Stora	age Description
#1	951.00'	7.655	af Cust	tom Stage Data (Prismatic)Listed below (Recalc)
		I	0	0
Elevation	Surt.Al	rea in	c.Store	Cum.Store
(teet)	(acr	es) (ac	re-teet)	(acre-teet)
951.00	0.1	19	0.000	0.000
952.00	0.1	45	0.132	0.132
954.00	0.2	201	0.347	0.479
956.00	0.2	263	0.465	0.944
958.00	0.3	332	0.595	1.539
960.00	0.4	-06	0.738	2.277
961.00	0.5	545	0.476	2.752
962.00	0.5	590	0.568	3.320
964.00	0.6	685	1.275	4.595
965.00	0.7	'35	0.710	5.305
966.00	0.7	'86	0.760	6.065
968.00	0.8	803	1.589	7.655
Device F	Routina	Invert	Outlet De	evices
#1 F	Primary	961 00'	30.0" Ro	ound RCP Round 30"
	·····		L = 50.0'	RCP, aroove end projecting. Ke= 0.200
			Inlet / Ou	utlet Invert= 961.00' / 960.50' S= 0.0100 '/' Cc= 0.900
			n= 0.013	Concrete pipe, bends & connections. Flow Area= 4.91 sf
#2 [Device 1	961.00'	Custom	Weir/Orifice. Cv= 2.62 (C= 3.28)
			Head (fee	et) 0.00 1.05 1.05 8.00
			Width (fe	eet) 0.85 0.85 5.00 5.00
#3 [Device 2	957.50'	30.0" Ro	ound RCP Round 30"
			l = 25.0'	RCP end-section conforming to fill Ke= 0.500
			Inlet / Ou	itlet Invert= 957 50' / 957 50' S= 0 0000 '/' Cc= 0 900
			n = 0.013	Concrete pipe, bends & connections. Flow Area= 4 91 sf
#4 -	Tertiary	966 00'	15.0' lon	ig x 10.0' breadth Broad-Crested Rectangular Weir
		000.00	Head (fee	et) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60

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			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64
#5	Secondary	961.00'	30.0" Round RCP_Round 30"
	-		L= 50.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 961.00' / 960.50' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf
#6	Device 5	962.05'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28)
			Head (feet) 0.00 5.00
			Width (feet) 5.00 5.00
#7	Device 6	957.50'	30.0" Round RCP_Round 30"
			L= 25.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 957.50' / 957.50' S= 0.0000 '/' Cc= 0.900
			n= 0.013 Concrete pipe, bends & connections, Flow Area= 4.91 sf

Primary OutFlow Max=37.17 cfs @ 12.39 hrs HW=964.48' TW=0.00' (Dynamic Tailwater) -1=RCP_Round 30" (Barrel Controls 37.17 cfs @ 7.57 fps) -2=Custom Weir/Orifice (Dasses 27.17 cfs @ 7.57 fps)

-2=Custom Weir/Orifice (Passes 37.17 cfs of 69.56 cfs potential flow)

-3=RCP_Round 30" (Passes 37.17 cfs of 44.09 cfs potential flow)

Secondary OutFlow Max=36.85 cfs @ 12.39 hrs HW=964.48' TW=0.00' (Dynamic Tailwater) 5=RCP_Round 30" (Passes 36.85 cfs of 37.17 cfs potential flow) 6=Custom Weir/Orifice (Passes 36.85 cfs of 62.03 cfs potential flow) 7=RCP_Round 30" (Inlet Controls 36.85 cfs @ 7.51 fps)

Tertiary OutFlow Max=0.00 cfs @ 0.00 hrs HW=961.00' TW=0.00' (Dynamic Tailwater) **4=Broad-Crested Rectangular Weir** (Controls 0.00 cfs)

Pond 100P: Basin 100



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 121139-Creekside 5-27-2022-Proposed MSE 24-hr 3
 100-yr Rainfall=7.47"

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Summary for Pond 200P: Basin 200

Inflow Area	a =	4.642 ac, 4	1.66% Impervious,	Inflow Depth = 5.	93" for 100-yr event
Inflow	=	39.98 cfs @	12.18 hrs, Volume	= 2.296 af	
Outflow	=	8.50 cfs @	12.52 hrs, Volume	= 2.292 af,	Atten= 79%, Lag= 20.5 min
Primary	=	8.50 cfs @	12.52 hrs, Volume	= 2.292 af	-
Routed	to Link	P-Creek : Pro	posed Creek		
Secondary	/ =	0.00 cfs @	0.00 hrs, Volume	= 0.000 af	
Routed	to Link	P-Creek : Pro	posed Creek		

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 962.00' Surf.Area= 0.480 ac Storage= 1.681 af Peak Elev= 964.08' @ 12.52 hrs Surf.Area= 0.594 ac Storage= 2.796 af (1.115 af above start)

Plug-Flow detention time= 605.1 min calculated for 0.611 af (27% of inflow) Center-of-Mass det. time= 144.7 min (923.6 - 779.0)

Volume	Invert	Avail.Stora	ige Stor	age Description
#1	952.00'	4.760	af Cus	tom Stage Data (Prismatic)Listed below (Recalc)
Elevatio	n Surf.Are	a In	c.Store	Cum.Store
(fee	t) (acres	s) (ac	re-feet)	(acre-feet)
952.0	0 0.02	3	0.000	0.000
954.0	0 0.05	9	0.081	0.081
956.0	0 0.11	0	0.168	0.250
958.0	0 0.18	3	0.293	0.543
960.0	0 0.26	7	0.451	0.994
961.0	0 0.31	3	0.290	1.284
962.0	0 0.48	0	0.397	1.681
964.0	0 0.58	9	1.069	2.750
965.0	0 0.64	6	0.618	3.367
966.0	0 0.70	2	0.674	4.042
967.0	0 0.73	5	0.719	4.760
Device	Routina	Invert	Outlet D	evices
#1	Primary	962 00'	15.0" R	ound RCP Round 15"
	i iiiidi y	002.00	L= 25.0'	RCP, aroove end projecting. Ke= 0.200
			Inlet / Ou	utlet Invert= 962.00' / 961.50' S= 0.0200 '/' Cc= 0.900
			n= 0.013	3 Concrete pipe, bends & connections, Flow Area= 1.23 sf
#2	Device 1	962.00'	Custom	Weir/Orifice, Cv= 2.62 (C= 3.28)
			Head (fe	eet) 0.00 1.00 1.00 8.00
			Width (fe	eet) 1.00 1.00 5.00 5.00
#3	Device 2	959.75'	15.0" R	ound RCP_Round 15"
			L= 25.0'	RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Ou	utlet Invert= 959.75' / 959.75' S= 0.0000 '/' Cc= 0.900
			n= 0.013	3 Concrete pipe, bends & connections, Flow Area= 1.23 sf
#4	Secondary	966.00'	25.0' lon	ng x 10.0' breadth Broad-Crested Rectangular Weir
			Head (fe	eet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (E	nglish) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=8.50 cfs @ 12.52 hrs HW=964.08' TW=0.00' (Dynamic Tailwater) 1=RCP_Round 15" (Barrel Controls 8.50 cfs @ 6.93 fps) 2=Custom Weir/Orifice (Passes 8.50 cfs of 24.48 cfs potential flow)

3=RCP_Round 15" (Passes 8.50 cfs of 8.52 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=962.00' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 200P: Basin 200



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Summary for Pond 300P: Basin 300

Inflow Area =		1.894 ac, 4	48.85% Imp	ervious,	Inflow Dep	th =	6.17	7" for 100-yr event			
Inflow	=	17.73 cfs @	12.16 hrs,	Volume	= 0).974	af		-		
Outflow	=	7.13 cfs @	12.40 hrs,	Volume	= 0).973	af, A	tten= 60)%,	Lag= 14	.4 min
Primary	=	7.13 cfs @	12.40 hrs,	Volume	= 0).973	af			•	
Routed	to Link	P-Creek : Pro	oposed Cree	ek							
Secondary	=	0.00 cfs @	0.00 hrs,	Volume	= 0	000.	af				
Routed	to Link	P-Creek : Pro	posed Cree	ek							

Routing by Sim-Route method, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs Starting Elev= 966.00' Surf.Area= 0.160 ac Storage= 0.317 af Peak Elev= 967.68' @ 12.32 hrs Surf.Area= 0.222 ac Storage= 0.638 af (0.321 af above start)

Plug-Flow detention time= 195.0 min calculated for 0.656 af (67% of inflow) Center-of-Mass det. time= 63.9 min (837.3 - 773.4)

Volume	Invert A	Avail.Stora	ge Storag	ge Description
#1	958.00'	1.594	af Custo	om Stage Data (Prismatic)Listed below (Recalc)
Elevatio	n Surf.Area	i In	c.Store	Cum.Store
(feet	i) (acres)) (acı	re-feet)	(acre-feet)
958.00	0.003		0.000	0.000
960.00	0.012		0.015	0.015
962.00	0 0.029		0.041	0.056
964.00	0 0.053	5	0.083	0.139
965.00	0 0.071		0.062	0.201
966.00	0 0.160		0.116	0.317
968.00	0 0.234		0.394	0.711
970.00	0 0.316	6	0.550	1.261
971.00	0 0.351		0.333	1.594
Device	Routing	Invert	Outlet Dev	vices
#1	Primary	966.00'	15.0" Ro	und RCP_Round 15"
			L= 25.0'	RCP, groove end projecting, Ke= 0.200
			Inlet / Out	let Invert= 966.00' / 965.50' S= 0.0200 '/' Cc= 0.900
			n= 0.013	Concrete pipe, bends & connections, Flow Area= 1.23 sf
#2	Device 1	966.00'	Custom V	Veir/Orifice, Cv= 2.62 (C= 3.28)
			Head (fee	t) 0.00 0.50 0.50 5.00
	-		Width (fee	et) 0.75 0.75 5.00 5.00
#3	Device 2	963.75	15.0" Roi	und RCP_Round 15"
			L= 30.0'	RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Out	let Invert= 963.75' / 963.75' S= 0.0000 /' Cc= 0.900
	o 1	070 001	n= 0.013	Concrete pipe, bends & connections, Flow Area= 1.23 st
#4	Secondary	970.00	25.0 long	
				() 0.20 0.40 0.00 0.80 1.00 1.20 1.40 1.00
			Uoer. (Eng	JIISTI) 2.49 2.30 2.70 2.09 2.08 2.09 2.07 2.04

Primary OutFlow Max=7.13 cfs @ 12.40 hrs HW=967.64' TW=0.00' (Dynamic Tailwater) 1=RCP_Round 15" (Barrel Controls 7.13 cfs @ 5.83 fps) 2=Custom Weir/Orifice (Passes 7.13 cfs of 22.18 cfs potential flow) 3=RCP_Round 15" (Passes 7.13 cfs of 7.57 cfs potential flow)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=966.00' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Pond 300P: Basin 300



Summary for Link P-Creek: Proposed Creek

Inflow Are	ea =	32.188 ac, 3	3.10% Impervious	, Inflow Depth =	5.78	3" for 100-yr event
Inflow	=	133.87 cfs @	12.28 hrs, Volum	e= 15.507	af	
Primary	=	133.87 cfs @	12.28 hrs, Volum	e= 15.507	af, /	Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs



Link P-Creek: Proposed Creek

Summary for Link P-South: Proposed South

Inflow /	Area	=	4.438 ac,	7.41% Impervious,	Inflow Depth = 5.1	24" for 100-yr event
Inflow		=	45.56 cfs @	12.11 hrs, Volume	= 1.939 af	
Primary	у	=	45.56 cfs @	12.11 hrs, Volume	= 1.939 af,	Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs

Link P-South: Proposed South



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Summary for Link P-West: Proposed West

Inflow A	\rea =	3.590 ac, 1	18.01% Impervious,	Inflow Depth = 5.	47" for 100-yr event
Inflow	=	38.54 cfs @	12.11 hrs, Volume	= 1.637 af	
Primary	· =	38.54 cfs @	12.11 hrs, Volume	= 1.637 af,	Atten= 0%, Lag= 0.1 min

Primary outflow = Inflow, Time Span= 0.00-160.00 hrs, dt= 0.001 hrs

Link P-West: Proposed West



Appendix C: NRCS Soils Report



United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Wright County, Minnesota



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND				MAP INFORMATION		
Area of Interest (AOI)			Spoil Area	The soil surveys that comprise your AOI were mapped at		
	Area of Interest (AOI)	٥	Stony Spot	1:12,000.		
Soils		60	Very Stony Spot	Warning: Soil Man may not be valid at this scale		
	Soil Map Unit Polygons	Ŷ	Wet Spot			
~	Soil Map Unit Lines	~	Other	Enlargement of maps beyond the scale of mapping can cause		
	Soil Map Unit Points	-	Special Line Features	line placement. The maps do not show the small areas of		
Special	Point Features	Water Features		contrasting soils that could have been shown at a more detailed		
ø	Blowout	~	Streams and Canals	scale.		
\boxtimes	Borrow Pit	Transport	ation	Please rely on the bar scale on each map sheet for map		
Ж	Clay Spot	+++	Rails	measurements.		
\diamond	Closed Depression	~	Interstate Highways	Course of Man. Natural Descurses Concernation Service		
¥	Gravel Pit	~	US Routes	Web Soil Survey URL:		
	Gravelly Spot	~	Major Roads	Coordinate System: Web Mercator (EPSG:3857)		
0	Landfill	-	Local Roads	Maps from the Web Soil Survey are based on the Web Mercator		
A.	Lava Flow	Backgrou	nd	projection, which preserves direction and shape but distorts		
عليه	Marsh or swamp	- Geo	Aerial Photography	distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more		
~	Mine or Quarry			accurate calculations of distance or area are required.		
0	Miscellaneous Water			This product is generated from the USDA-NRCS certified data as		
õ	Perennial Water			of the version date(s) listed below.		
Š	Rock Outcrop			Coil Currey Areas Wright County Minnageta		
Saline Snot				Survey Area Data: Version 15, Sep 10, 2021		
T	Sandy Spot					
**	Soverely Freded Spot			Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.		
÷						
				Date(s) aerial images were photographed: Data not available.		
∌	Slide or Slip			The orthophoto or other base map on which the soil lines were		
ø	Sodic Spot			compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.		

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI				
106C2	Lester loam, 6 to 10 percent slopes, moderately eroded	4.2	10.0%				
106D2	Lester loam, 10 to 16 percent slopes, moderately eroded	0.3	0.7%				
109	Cordova clay loam, 0 to 2 percent slopes	12.3	29.3%				
539	Klossner muck, 0 to 1 percent slopes	0.4	0.9%				
1080	Klossner, Okoboji and Glencoe soils, ponded, 0 to 1 percent slopes	2.8	6.6%				
1362B	Angus loam, 2 to 6 percent slopes	2.8	6.7%				
1901B	Angus-Le Sueur complex, 1 to 6 percent slopes	19.2	45.8%				
Totals for Area of Interest		42.0	100.0%				

Map Unit Legend (Creekside)

Map Unit Descriptions (Creekside)

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit

descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Wright County, Minnesota

106C2—Lester loam, 6 to 10 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: 2ttc4 Elevation: 690 to 1,840 feet Mean annual precipitation: 24 to 37 inches Mean annual air temperature: 43 to 52 degrees F Frost-free period: 140 to 180 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Lester, moderately eroded, and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lester, Moderately Eroded

Setting

Landform: Ground moraines, hillslopes Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, rise Down-slope shape: Convex Across-slope shape: Linear, convex Parent material: Fine-loamy till

Typical profile

Ap - 0 to 6 inches: loam *Bt - 6 to 38 inches:* clay loam *C - 38 to 79 inches:* loam

Properties and qualities

Slope: 6 to 10 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)
Depth to water table: About 47 to 63 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 10.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: C Ecological site: R103XY020MN - Loamy Upland Savannas Forage suitability group: Sloping Upland, Acid (G103XS006MN) Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

Minor Components

Storden, moderately eroded

Percent of map unit: 10 percent Landform: Ground moraines Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Rise Down-slope shape: Convex, linear Across-slope shape: Linear, convex Ecological site: R103XY020MN - Loamy Upland Savannas Other vegetative classification: Sloping Upland, Calcareous (G103XS010MN) Hydric soil rating: No

Le sueur

Percent of map unit: 3 percent Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve, talf Down-slope shape: Convex, linear Across-slope shape: Linear Ecological site: R103XY020MN - Loamy Upland Savannas Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

Hamel

Percent of map unit: 2 percent Landform: Ground moraines Landform position (three-dimensional): Dip Down-slope shape: Concave, linear Across-slope shape: Linear, concave Ecological site: F103XY030MN - Wet Footslope/Drainageway Forests Other vegetative classification: Level Swale, Neutral (G103XS001MN) Hydric soil rating: Yes

106D2—Lester loam, 10 to 16 percent slopes, moderately eroded

Map Unit Setting

National map unit symbol: 2ttc8 Elevation: 690 to 1,840 feet Mean annual precipitation: 24 to 37 inches Mean annual air temperature: 43 to 52 degrees F Frost-free period: 140 to 180 days Farmland classification: Not prime farmland

Map Unit Composition

Lester, moderately eroded, and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Lester, Moderately Eroded

Setting

Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, rise Down-slope shape: Convex Across-slope shape: Convex, linear Parent material: Fine-loamy till

Typical profile

Ap - 0 to 6 inches: loam *Bt - 6 to 38 inches:* clay loam *C - 38 to 79 inches:* loam

Properties and qualities

Slope: 10 to 16 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)
Depth to water table: About 55 to 71 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 10.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4e Hydrologic Soil Group: C Ecological site: R103XY020MN - Loamy Upland Savannas Forage suitability group: Sloping Upland, Acid (G103XS006MN) Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

Minor Components

Storden, moderately eroded

Percent of map unit: 10 percent Landform: Ground moraines Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Rise Down-slope shape: Convex, linear Across-slope shape: Linear, convex Ecological site: R103XY020MN - Loamy Upland Savannas Other vegetative classification: Sloping Upland, Calcareous (G103XS010MN) Hydric soil rating: No

Lester, moderately eroded

Percent of map unit: 3 percent Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, rise Down-slope shape: Convex Across-slope shape: Convex, linear Ecological site: R103XY020MN - Loamy Upland Savannas Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

Le sueur

Percent of map unit: 2 percent Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve, talf Down-slope shape: Convex, linear Across-slope shape: Linear Ecological site: R103XY020MN - Loamy Upland Savannas Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

109—Cordova clay loam, 0 to 2 percent slopes

Map Unit Setting

National map unit symbol: 2vvdk Elevation: 690 to 1,840 feet Mean annual precipitation: 24 to 37 inches Mean annual air temperature: 43 to 52 degrees F Frost-free period: 140 to 180 days Farmland classification: Prime farmland if drained

Map Unit Composition

Cordova and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Cordova

Setting

Landform: Ground moraines Landform position (three-dimensional): Talf Down-slope shape: Linear Across-slope shape: Linear Parent material: Fine-loamy till

Typical profile

Ap - 0 to 10 inches: clay loam A - 10 to 18 inches: clay loam Btg - 18 to 38 inches: clay loam Cg - 38 to 79 inches: loam

Properties and qualities

Slope: 0 to 2 percent *Depth to restrictive feature:* More than 80 inches *Drainage class:* Poorly drained

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Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)
Depth to water table: About 0 to 8 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 10.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: C/D Ecological site: F103XY027MN - Loamy Wet Forests Forage suitability group: Level Swale, Neutral (G103XS001MN) Other vegetative classification: Level Swale, Neutral (G103XS001MN) Hydric soil rating: Yes

Minor Components

Le sueur

Percent of map unit: 10 percent Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve, talf Down-slope shape: Convex, linear Across-slope shape: Linear Ecological site: R103XY020MN - Loamy Upland Savannas Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

Glencoe

Percent of map unit: 5 percent Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave Ecological site: R103XY015MN - Depressional Marsh Other vegetative classification: Ponded If Not Drained (G103XS013MN) Hydric soil rating: Yes

539—Klossner muck, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2s8wz Elevation: 690 to 1,840 feet Mean annual precipitation: 24 to 37 inches Mean annual air temperature: 43 to 52 degrees F Frost-free period: 140 to 180 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Klossner, drained, and similar soils: 90 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Klossner, Drained

Setting

Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave Parent material: Organic material over alluvium

Typical profile

Oap - 0 to 9 inches: muck *Oa - 9 to 27 inches:* muck *2A - 27 to 46 inches:* silty clay loam *2Cg - 46 to 79 inches:* silty clay loam

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.06 to 2.00 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: Occasional
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Very high (about 17.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: C/D Ecological site: R103XY016MN - Organic Marsh Forage suitability group: Organic (G103XS014MN) Other vegetative classification: Organic (G103XS014MN) Hydric soil rating: Yes

Minor Components

Canisteo

Percent of map unit: 5 percent Landform: Rims on depressions, ground moraines Landform position (three-dimensional): Talf Down-slope shape: Concave, linear Across-slope shape: Linear Ecological site: R103XY001MN - Loamy Wet Prairies Other vegetative classification: Level Swale, Calcareous (G103XS009MN) Hydric soil rating: Yes

Okoboji

Percent of map unit: 5 percent Landform: Depressions

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Down-slope shape: Concave Across-slope shape: Concave Ecological site: R103XY015MN - Depressional Marsh Other vegetative classification: Ponded If Not Drained (G103XS013MN) Hydric soil rating: Yes

1080—Klossner, Okoboji and Glencoe soils, ponded, 0 to 1 percent slopes

Map Unit Setting

National map unit symbol: 2t3ny Elevation: 690 to 1,840 feet Mean annual precipitation: 24 to 37 inches Mean annual air temperature: 43 to 52 degrees F Frost-free period: 140 to 180 days Farmland classification: Not prime farmland

Map Unit Composition

Klossner, ponded, and similar soils: 35 percent Okoboji, ponded, and similar soils: 30 percent Glencoe, ponded, and similar soils: 25 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Klossner, Ponded

Setting

Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave Parent material: Organic material over alluvium

Typical profile

Oa1 - 0 to 9 inches: muck *Oa2 - 9 to 27 inches:* muck *2A - 27 to 46 inches:* silty clay loam *2Cg - 46 to 79 inches:* silty clay loam

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.06 to 2.00 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Very high (about 17.7 inches)
Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8w Hydrologic Soil Group: C/D Ecological site: R103XY016MN - Organic Marsh Forage suitability group: Not Suited (G103XS024MN) Other vegetative classification: Not Suited (G103XS024MN) Hydric soil rating: Yes

Description of Okoboji, Ponded

Setting

Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave Parent material: Local alluvium over till

Typical profile

A1 - 0 to 8 inches: silty clay loam A2 - 8 to 33 inches: silty clay loam Bg - 33 to 38 inches: silty clay loam Cg - 38 to 79 inches: silty clay loam

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.06 to 2.00 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: Very high (about 12.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8w Hydrologic Soil Group: C/D Ecological site: R103XY016MN - Organic Marsh Forage suitability group: Not Suited (G103XS024MN) Other vegetative classification: Not Suited (G103XS024MN) Hydric soil rating: Yes

Description of Glencoe, Ponded

Setting

Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave Parent material: Local alluvium over till

Typical profile

A1 - 0 to 9 inches: clay loam

- A2 9 to 39 inches: clay loam
- Bg 39 to 50 inches: clay loam

Cg - 50 to 79 inches: clay loam

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Very poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.06 to 2.00 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: None
Frequency of ponding: Frequent
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 10.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 8w Hydrologic Soil Group: C/D Ecological site: R103XY015MN - Depressional Marsh Forage suitability group: Not Suited (G103XS024MN) Other vegetative classification: Not Suited (G103XS024MN) Hydric soil rating: Yes

Minor Components

Glencoe

Percent of map unit: 5 percent Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave Ecological site: R103XY015MN - Depressional Marsh Other vegetative classification: Ponded If Not Drained (G103XS013MN) Hydric soil rating: Yes

Canisteo

Percent of map unit: 3 percent Landform: Rims on depressions, ground moraines Landform position (three-dimensional): Talf Down-slope shape: Concave, linear Across-slope shape: Linear Ecological site: R103XY001MN - Loamy Wet Prairies Other vegetative classification: Level Swale, Calcareous (G103XS009MN) Hydric soil rating: Yes

Houghton, ponded

Percent of map unit: 2 percent Landform: Marshes Down-slope shape: Concave Across-slope shape: Concave Ecological site: R103XY016MN - Organic Marsh Other vegetative classification: Not Suited (G103XS024MN) Hydric soil rating: Yes

1362B—Angus loam, 2 to 6 percent slopes

Map Unit Setting

National map unit symbol: 2syrq Elevation: 690 to 1,840 feet Mean annual precipitation: 24 to 37 inches Mean annual air temperature: 43 to 52 degrees F Frost-free period: 140 to 180 days Farmland classification: All areas are prime farmland

Map Unit Composition

Angus and similar soils: 80 percent Minor components: 20 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Angus

Setting

Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve, rise Down-slope shape: Convex Across-slope shape: Convex, linear Parent material: Fine-loamy till

Typical profile

Ap - 0 to 7 inches: loam Bt - 7 to 37 inches: clay loam BC - 37 to 50 inches: clay loam C - 50 to 79 inches: loam

Properties and qualities

Slope: 2 to 6 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)
Depth to water table: About 39 to 51 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 10.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: C Ecological site: R103XY020MN - Loamy Upland Savannas Forage suitability group: Sloping Upland, Acid (G103XS006MN) Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

Minor Components

Angus, moderately eroded

Percent of map unit: 10 percent Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve, rise Down-slope shape: Convex Across-slope shape: Convex, linear Ecological site: R103XY020MN - Loamy Upland Savannas Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

Cordova

Percent of map unit: 5 percent Landform: Ground moraines Landform position (three-dimensional): Dip Down-slope shape: Concave Across-slope shape: Linear Ecological site: F103XY027MN - Loamy Wet Forests Other vegetative classification: Level Swale, Neutral (G103XS001MN) Hydric soil rating: Yes

Le sueur

Percent of map unit: 5 percent Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit Landform position (three-dimensional): Interfluve, talf Down-slope shape: Convex, linear Across-slope shape: Linear Ecological site: R103XY020MN - Loamy Upland Savannas Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

1901B—Angus-Le Sueur complex, 1 to 6 percent slopes

Map Unit Setting

National map unit symbol: 2vvgs Elevation: 690 to 1,840 feet Mean annual precipitation: 24 to 37 inches Mean annual air temperature: 43 to 52 degrees F Frost-free period: 140 to 180 days Farmland classification: All areas are prime farmland

Map Unit Composition

Angus and similar soils: 55 percent Le sueur and similar soils: 35 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Angus

Setting

Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit, backslope Landform position (three-dimensional): Interfluve, rise Down-slope shape: Convex Across-slope shape: Convex, linear Parent material: Fine-loamy till

Typical profile

Ap - 0 to 7 inches: loam Bt - 7 to 37 inches: clay loam BC - 37 to 50 inches: clay loam C - 50 to 79 inches: loam

Properties and qualities

Slope: 2 to 6 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)
Depth to water table: About 39 to 51 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 10.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2e Hydrologic Soil Group: C Ecological site: F103XY025MN - Loamy Upland Forests Forage suitability group: Sloping Upland, Acid (G103XS006MN) Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

Description of Le Sueur

Setting

Landform: Hillslopes, ground moraines Landform position (two-dimensional): Summit, backslope, footslope Landform position (three-dimensional): Interfluve, talf Down-slope shape: Convex, linear Across-slope shape: Linear Parent material: Fine-loamy till

Typical profile

Ap - 0 to 8 inches: loam

A - 8 to 14 inches: loam

Btg - 14 to 52 inches: clay loam

Cg - 52 to 79 inches: loam

Properties and qualities

Slope: 1 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.20 to 2.00 in/hr)
Depth to water table: About 12 to 24 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 20 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water supply, 0 to 60 inches: High (about 10.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 1 Hydrologic Soil Group: C/D Ecological site: F103XY025MN - Loamy Upland Forests Forage suitability group: Sloping Upland, Acid (G103XS006MN) Other vegetative classification: Sloping Upland, Acid (G103XS006MN) Hydric soil rating: No

Minor Components

Cordova

Percent of map unit: 10 percent Landform: Ground moraines Landform position (three-dimensional): Dip Down-slope shape: Concave, linear Across-slope shape: Concave Ecological site: F103XY027MN - Loamy Wet Forests Other vegetative classification: Level Swale, Neutral (G103XS001MN) Hydric soil rating: Yes

Soil Information for All Uses

Suitabilities and Limitations for Use

The Suitabilities and Limitations for Use section includes various soil interpretations displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each interpretation.

Land Management

Land management interpretations are tools designed to guide the user in evaluating existing conditions in planning and predicting the soil response to various land management practices, for a variety of land uses, including cropland, forestland, hayland, pastureland, horticulture, and rangeland. Example interpretations include suitability for a variety of irrigation practices, log landings, haul roads and major skid trails, equipment operability, site preparation, suitability for hand and mechanical planting, potential erosion hazard associated with various practices, and ratings for fencing and waterline installation.

Erosion Hazard (Off-Road, Off-Trail) (Creekside)

As of 9/30/2021, this rating is not working as intended. All components appear as not rated. This rating will be fixed on 10/01/2022.

The ratings in this interpretation indicate the hazard of soil loss from off-road and off-trail areas after disturbance activities that expose the soil surface. The ratings are based on slope, soil erosion factor K, and an index of rainfall erosivity (R). The soil loss is caused by sheet or rill erosion in off-road or off-trail areas where 50 to 75 percent of the surface has been exposed by logging, grazing, mining, or other kinds of disturbance.

The ratings are both verbal and numerical. The hazard is described as "slight," "moderate," "severe," or "very severe." A rating of "slight" indicates that erosion is unlikely under ordinary climatic conditions; "moderate" indicates that some erosion is likely and that erosion-control measures may be needed; "severe" indicates that erosion is very likely and that erosion-control measures, including revegetation of bare areas, are advised; and "very severe" indicates that significant erosion is expected, loss of soil productivity and off-site damage are likely, and erosion-control measures are costly and generally impractical.

Numerical ratings indicate the severity of individual limitations. The ratings are shown as decimal fractions ranging from 0.01 to 1.00. They indicate gradations between the point at which a soil feature has the greatest negative impact on the specified aspect of forestland management (1.00) and the point at which the soil feature is not a limitation (0.00).

The map unit components listed for each map unit in the accompanying Summary by Map Unit table in Web Soil Survey or the Aggregation Report in Soil Data Viewer are determined by the aggregation method chosen. An aggregated rating class is shown for each map unit. The components listed for each map unit are only those that have the same rating class as listed for the map unit. The percent composition of each component in a particular map unit is presented to help the user better understand the percentage of each map unit that has the rating presented.

Other components with different ratings may be present in each map unit. The ratings for all components, regardless of the map unit aggregated rating, can be viewed by generating the equivalent report from the Soil Reports tab in Web Soil Survey or from the Soil Data Mart site. Onsite investigation may be needed to validate these interpretations and to confirm the identity of the soil on a given site.

Custom Soil Resource Report



	MAP LEGEN)	MAP INFORMATION				
Area of Interes	ea of Interest (AOI)	US Routes Major Roads	The soil surveys that comprise your AOI were mapped at 1:12,000.				
Soils Soil Rating F	Polygons Zevere Backgro	Local Roads und	Warning: Soil Map may not be valid at this scale.				
Se	evere evere	Aerial Photography	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contracting soils that could have been shown at a more detailed				
Sli	ght ot rated or not available		scale.				
Soil Rating I	-ines ry severe		Please rely on the bar scale on each map sheet for map measurements.				
🫹 Se	oderate		Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)				
Sli	ght t rated or not available		Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts				
Soil Rating F	Points ry severe		distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.				
Se	oderate		This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.				
Sli	ght ot rated or not available		Soil Survey Area: Wright County, Minnesota Survey Area Data: Version 15, Sep 10, 2021				
Water Features	s reams and Canals n		Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.				
Ra	ills erstate Highways		Date(s) aerial images were photographed: Data not available.				
			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.				

Tables—Erosion Hazard (Off-Road, Off-Trail) (Creekside)

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Map unit symbol	Map unit name	Rating	Component name (percent)	Rating reasons (numeric values)	Acres in AOI	Percent of AOI
106C2	Lester loam, 6 to 10 percent slopes,	Not rated	Lester, moderately eroded (85%)		4.2	10.0%
	moderately eroded		Storden, moderately eroded (10%)			
			Le Sueur (3%)			
			Hamel (2%)			
106D2	Lester loam, 10 to 16 percent slopes,	Not rated	Lester, moderately eroded (85%)		0.3	0.7%
	moderately eroded		Storden, moderately eroded (10%)			
			Lester, moderately eroded (3%)			
			Le Sueur (2%)			
109	Cordova clay	Not rated	Cordova (85%)		12.3	29.3%
	loam, 0 to 2 percent slopes		Le Sueur (10%)			
			Glencoe (5%)			
539 KI	Klossner muck, 0 to 1 percent	Not rated	Klossner, drained (90%)		0.4	0.9%
	siopes		Canisteo (5%)			
			Okoboji (5%)			
1080	Klossner, Okoboji and Glencoe	Not rated	Klossner, ponded (35%)		2.8	6.6%
	0 to 1 percent slopes		Okoboji, ponded (30%)			
			Glencoe, ponded (25%)			
			Glencoe (5%)			
			Canisteo (3%)			
			Houghton, ponded (2%)			
1362B	Angus loam, 2 to	Not rated	Angus (80%)		2.8	6.7%
	6 percent slopes		Angus, moderately eroded (10%)			
			Cordova (5%)			
			Le Sueur (5%)			

Map unit symbol	Map unit name	Rating	Component name (percent)	Rating reasons (numeric values)	Acres in AOI	Percent of AOI
1901B	Angus-Le Sueur complex, 1 to 6 percent slopes	Not rated	Angus (55%)		19.2	45.8%
			Le Sueur (35%)			
			Cordova (10%)			
Totals for Area of Interest					42.0	100.0%

Rating	Acres in AOI	Percent of AOI		
Null or Not Rated	42.0	100.0%		
Totals for Area of Interest	42.0	100.0%		

Rating Options—Erosion Hazard (Off-Road, Off-Trail) (Creekside)

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

Soil Reports

The Soil Reports section includes various formatted tabular and narrative reports (tables) containing data for each selected soil map unit and each component of each unit. No aggregation of data has occurred as is done in reports in the Soil Properties and Qualities and Suitabilities and Limitations sections.

The reports contain soil interpretive information as well as basic soil properties and qualities. A description of each report (table) is included.

Soil Erosion

This folder contains a collection of tabular reports that present soil erosion factors and groupings. The reports (tables) include all selected map units and components for each map unit. Soil erosion factors are soil properties and interpretations used in evaluating the soil for potential erosion. Example soil erosion factors can include K factor for the whole soil or on a rock free basis, T factor, wind erodibility group and wind erodibility index.

RUSLE2 Related Attributes (Creekside)

This report summarizes those soil attributes used by the Revised Universal Soil Loss Equation Version 2 (RUSLE2) for the map units in the selected area. The report includes the map unit symbol, the component name, and the percent of the component in the map unit. Soil property data for each map unit component include the hydrologic soil group, erosion factor Kf for the surface horizon, erosion factor T, and the representative percentage of sand, silt, and clay in the mineral surface horizon. Missing surface data may indicate the presence of an organic layer.

Report—RUSLE2 Related Attributes (Creekside)

Soil properties and interpretations for erosion runoff calculations. The surface mineral horizon properties are displayed or the first mineral horizon below an organic surface horizon. Organic horizons are not displayed.

RUSLE2 Related Attributes–Wright County, Minnesota								
Map symbol and soil name	Pct. of	Slope	Hydrologic group	Kf	T factor	Representative value		
	map unit	(ft)				% Sand	% Silt	% Clay
106C2—Lester loam, 6 to 10 percent slopes, moderately eroded								
Lester, moderately eroded	85	98	С	.32	5	39.0	37.0	24.0
106D2—Lester loam, 10 to 16 percent slopes, moderately eroded								
Lester, moderately eroded	85	98	С	.32	5	39.0	37.0	24.0

RUSLE2 Related Attributes–Wright County, Minnesota								
Map symbol and soil name	Pct. of	Slope	Hydrologic group	Kf	T factor	Representative value		
	map unit	length (ft)				% Sand	% Silt	% Clay
109—Cordova clay loam, 0 to 2 percent slopes								
Cordova	85	82	C/D	.28	5	34.2	37.8	28.0
539—Klossner muck, 0 to 1 percent slopes								
Klossner, drained	90	689	C/D	—	1	—	_	_
1080—Klossner, Okoboji and Glencoe soils, ponded, 0 to 1 percent slopes								
Klossner, ponded	35	689	C/D	—	1	—	_	_
Okoboji, ponded	30	82	C/D	.32	5	11.0	53.0	36.0
Glencoe, ponded	25	82	C/D	.28	5	22.0	45.0	33.0
1362B—Angus loam, 2 to 6 percent slopes								
Angus	80	98	С	.28	5	39.0	37.0	24.0
1901B—Angus-Le Sueur complex, 1 to 6 percent slopes								
Angus	55	98	С	.28	5	39.0	37.0	24.0
Le Sueur	35	82	C/D	.28	5	39.0	37.0	24.0

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