

CITY OF HUXLEY

TUESDAY ** APRIL 16, 2019 ** CITY COUNCIL ** 6:30 P.M.

A SESSION OF THE CITY OF HUXLEY'S PLANNING AND ZONING COMMISSION

PUBLIC NOTICE IS HEREBY GIVEN THAT THE PLANNING AND ZONING COMMISSION OF THE CITY OF HUXLEY, IOWA, WILL MEET IN THE HUXLEY CITY COUNCIL CHAMBERS 515 NORTH MAIN AVE., HUXLEY, IOWA AT 6:30 P.M. ON TUESDAY THE 16TH DAY OF APRIL 2019 TO CONSIDER THE MATTERS ENUMERATED IN THE AGENDA BELOW:

1.0) ROLL CALL

COMMISSION AGENDA ITEMS:

2.0) MOTION TO APPROVE THE MINUTES FROM THE FOLLOWING MEETINGS:

2.1) April 8, 2019 – Meeting

2.0) PUBLIC HEARING: NONE

4.0) DISCUSSION AND RECOMMENATION ITEMS:

4.01) DISCUSSION AND POSSIBLE ACTION REGARDING MINI STORAGE SITE PLAN AT 508 EAST FIRST STREET.

4.02) DISCUSSION OF THE KUM AND GO TRAFFIC STUDY AND STORM WATER MANAGEMENT PLAN.

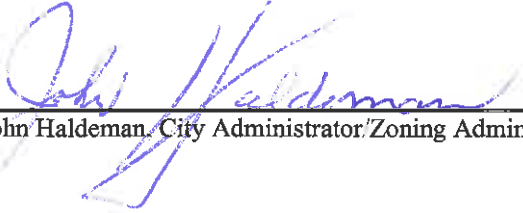
4.03) DISCUSSION AND POSSIBLE ACTION REGARDING THE KUM AND GO SITE PLAN.

5.0) MISCELLANEOUS

6.0) COMMENTS

7.0) ADJOURNMENT

THIS NOTICE IS HEREBY GIVEN AT LEAST 24 HOURS PRIOR TO THE COMMENCEMENT OF THE MEETING SPECIFIED ABOVE. THIS WAS DONE BY ADVISING THE NEWS MEDIA WHO HAVE FILED A REQUEST FOR NOTICE AND BY POSTING THE NOTICE ON THE FRONT WINDOW IN THE LOBBY AREA IN CITY HALL THAT IS ACCESSIBLE TO THE PUBLIC. THIS WAS ALL PURSUANT TO CHAPTER 21 OF THE CODE OF IOWA.



John Haldeman, City Administrator/Zoning Administrator

Planning and Zoning Commission Minutes

Monday, April 8, 2019

Huxley Safe Room, 6:30pm

1.0) Call to Order and Roll Call:

P & Z members present: Larry Wilson, Cheryl Patterson, Joe Scott, Mike Schonhorst

Staff present: John Haldeman – City Administrator, Jolene Lettow – City Clerk

Consultants present: Mike Heilman – city attorney

Guests present: Keith Weggen, Britni Andreassen – Kum 'N Go representatives, Roger Wheeler, Henry Hauptert, Matthew Hawes, Alissa Hawes, Wes James, Jill Riedemann, Jeff Barnwell, Shawna Murphy, Jesse Sommerfeld, Randy Schmerbach, T.J. Trav, Kelsey Trav, Dennis Hoke, Adam Walters, Amanda DeMaris, Lisa Ditenford, Jamie Dailey, Molly Mollman, Todd Nelson, Clifford DeMaris

Mike Schonhorst, Acting Chairman, called the meeting to order at 6:38pm.

Commission Agenda Items:

2.0) Motion – Scott, Second – Wilson to Approve Minutes from the Following Meeting: March 25, 2019. 4 ayes. Motion carried.

3.0) Public Hearing: None

4.01) Motion – Patterson, Second – Wilson to Recommend Approval to Council the Annexation Request from Leonard and Jaqueline Larson for Property at SE Corner of I-35 and Highway 210. Kum 'N Go representatives explained that a 5,975 square foot facility would be built on the five acre lot. Roll Call: Wilson, Patterson, Scott, Schonhorst voted yes. Motion carried.

4.02) Motion – Patterson, Second – Scott to Recommend Approval to Council the Rezoning Request from Leonard and Jaqueline Larson for Property at SE Corner of I-35 and Highway 210. The zoning will be changed from Agricultural to R-2. Roll Call: Patterson, Scott, Schonhorst, Wilson voted yes. Motion carried.

4.03) Motion – Scott, Second – Wilson to Recommend to Council the Rezoning of the Westview Development Owned by Dickson and Luann Jensen. Development is 40 acres northwest of town. There will be three different zones within development: R-1/80 foot wide lots and ½ acre estate lots, R-1A/74 foot wide lots, and R-2/twin homes. Residents from Centennial West subdivision had following comments/concerns:

- Traffic flow – large number of new homes will be adding traffic to area. Could there be another entrance added to development?
- Water flow – currently there are drainage issues in development – will this be resolved?
- Construction path – could there be one set specifically to avoid heavy construction vehicles on existing roads?
- Will a park be added to development/area?
- Is city keeping up with the growth?
- Advantage Homes builds the same looking houses – need diversity, more custom built homes.

Roll Call: Scott, Schonhorst, Wilson, Patterson voted yes. Motion carried.

4.04) Motion – Patterson, Second - Scott to Recommend to Council the Approval of the Annexation Request for the Westview Development from Dickson and LuAnn Jensen. There was discussion regarding preliminary plat process and steps to continue to voice concerns/comments from public. Roll Call: Scott, Schonhorst, Wilson, Patterson voted yes. Motion carried.

5.01) Next meeting scheduled for May 13th.

7.0) Motion – Scott, Second – Wilson to adjourn at 7:33pm. 4 ayes.

Submitted by: Jolene R. Lettow, City Clerk



VEENSTRA & KIMM, INC.

3000 Westown Parkway • West Des Moines, Iowa 50266-1320

515-225-8000 • 515-225-7848 (FAX) • 800-241-8000 (WATS)

April 12, 2019

M E M O R A N D U M

To: Huxley Planning & Zoning

Fr: Forrest Aldrich, Veenstra & Kimm, Inc.

Re: 508 East First Street

Chris Gardner, the owner of the property at 508 East First Street, will be at the Planning & Zoning meeting on April 16, 2019 to make a presentation.

The property is currently used as a mini-storage facility with three buildings. Chris is proposing to construct a fourth building at the north end of the property. The use of the property is not proposed to be changed. The property is zoned M-1.

Attached is the approved site plan for the site from December 1999. Chris is essentially wanting to complete Phase 3 of the site plan. The proposed building would have a similar footprint to the north building shown on the site plan.

The paving of the drives around the mini-storage buildings as described in Phase 2 was never completed. Currently there is gravel around the buildings.

Phase 3 describes the construction of a second driveway entrance, parking spaces at the north end of the site, and the installation of a sanitary lift station and water service. The sewer and water services are not needed as the building is proposed to be used for storage with internal access and not to be used for an office/warehouse.

Chris will present additional information on the proposed building and site layout.

The discussion with Planning & Zoning will focus on providing some direction for the site plan. Is the site plan still valid? Do all of the phasing requirements of the site plan need to be followed, or just some of the phasing requirements? Which ones? Assuming the existing site plan is still valid, at what point are there enough changes that a new site plan needs to be submitted?

If a new site plan were submitted, what is the thought of obtaining a waiver for not paving and leaving the site gravel? What would be the stormwater management requirements?

There is an existing sidewalk to the west but no sidewalk to the east. Will a sidewalk be required?

Both Chris Gardner and the writer will be at the meeting to answer questions.

END

45229-039
Attachment

SITE PLAN FOR HUXLEY MINI-STORAGE 508 E. FIRST STREET HUXLEY, IOWA

PROPERTY DESCRIPTION

LOT 2 FJORD SUBDIVISION, AN OFFICIAL PLAT, HUXLEY, IOWA, AND LOT 3 RAILROAD SUBDIVISION NO. 1, AN OFFICIAL PLAT, HUXLEY, IOWA.
SAID TRACT OF LAND CONTAINS 1.205 ACRES MORE OR LESS

GENERAL NOTES

1. THE SITE PLAN IS A PRELIMINARY DESIGN AND IS NOT TO BE USED FOR CONSTRUCTION WITHOUT THE APPROVAL OF THE CITY ENGINEER.
2. THE SITE PLAN IS BASED ON THE FOLLOWING ASSUMPTIONS: (a) THE EXISTING UTILITIES ARE SHOWN AS THEY ARE, AND THE ENGINEER HAS NO KNOWLEDGE OF ANY CHANGES SINCE THEY WERE LAYED OUT. (b) THE EXISTING UTILITIES ARE SHOWN AS THEY ARE, AND THE ENGINEER HAS NO KNOWLEDGE OF ANY CHANGES SINCE THEY WERE LAYED OUT.
3. THE SITE PLAN IS BASED ON THE FOLLOWING ASSUMPTIONS: (a) THE EXISTING UTILITIES ARE SHOWN AS THEY ARE, AND THE ENGINEER HAS NO KNOWLEDGE OF ANY CHANGES SINCE THEY WERE LAYED OUT. (b) THE EXISTING UTILITIES ARE SHOWN AS THEY ARE, AND THE ENGINEER HAS NO KNOWLEDGE OF ANY CHANGES SINCE THEY WERE LAYED OUT.
4. THE SITE PLAN IS BASED ON THE FOLLOWING ASSUMPTIONS: (a) THE EXISTING UTILITIES ARE SHOWN AS THEY ARE, AND THE ENGINEER HAS NO KNOWLEDGE OF ANY CHANGES SINCE THEY WERE LAYED OUT. (b) THE EXISTING UTILITIES ARE SHOWN AS THEY ARE, AND THE ENGINEER HAS NO KNOWLEDGE OF ANY CHANGES SINCE THEY WERE LAYED OUT.
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CONSTRUCTION PLANS

PHASE 1: January 1, 2001 to July 1, 2001

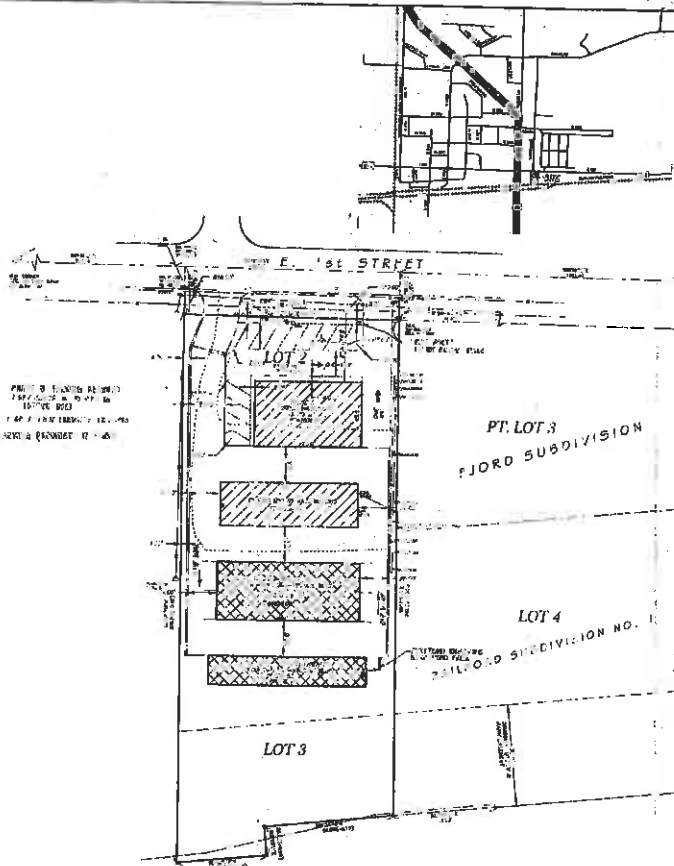
Phase 1 includes the existing site and the new building to be constructed on the site. The building will be constructed on the site and will be used for the purpose of the site. The building will be constructed on the site and will be used for the purpose of the site.

PHASE 2: January 1, 2001 to July 1, 2001

Phase 2 includes the existing site and the new building to be constructed on the site. The building will be constructed on the site and will be used for the purpose of the site. The building will be constructed on the site and will be used for the purpose of the site.

PHASE 3: January 1, 2001 to July 1, 2001

Phase 3 includes the existing site and the new building to be constructed on the site. The building will be constructed on the site and will be used for the purpose of the site. The building will be constructed on the site and will be used for the purpose of the site.



UTILITY SYMBOLS

WATER MAIN
SEWER MAIN
GAS MAIN
ELECTRIC MAIN
TELEPHONE MAIN
RAILROAD MAIN
FENCE LINE

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SITE PLAN
HUXLEY MINI-STORAGE
508 E. FIRST AVENUE

193-S
1/22

Bishop Engineering Company
1501 10th Street
Des Moines, Iowa 50319

193-5

Traffic Impact Letter

Draft Letter

Kum & Go Site #0131

Huxley, Iowa


Prepared for:

Iowa Department of Transportation

Submitted to:

Iowa Department of Transportation

January 29, 2019

	<p>I hereby certify that this engineering document was prepared by me or under my direct personal supervision and that I am a duly licensed Professional Engineer under the laws of the State of Iowa.</p> <p>Date: _____</p> <p>KIMBERLEY L. ROUSE, P.E. License No. 14865 My renewal date is December 31, 2020 Pages or sheets covered by this seal: _____</p>
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Analysis of Existing Conditions

The site of the proposed new Kum & Go 0131 is near the interchange of Hwy. 210 and Interstate 35 in rural Huxley. The site is located on the south side of the Hwy. to the east of the northbound off ramp. The site is surrounded by agricultural land uses. Monsanto Company is located approximately 2400' to the west of the site. Hwy. 210 is a rural highway with a speed limit of 55 mph near the site.



Figure 1 – Site Location

Proposed Development

The proposed development is a 5,975 square foot Kum & Go convenience store. It is proposed to have 12 gas pumps for passenger cars and 6 pumps for trucks. There is one access proposed on the east side of the development off of Hwy 210. The proposed entrance is approximately 610' from the northbound I-35 off ramp.

Existing Traffic Counts

November 2018 traffic counts were provided by Civil Design Advantage for Hwy. 210 near the proposed site. Traffic counts from the Iowa Department of Transportation were also reviewed. It was determined that the growth rate for the area is approximately 3% per year.

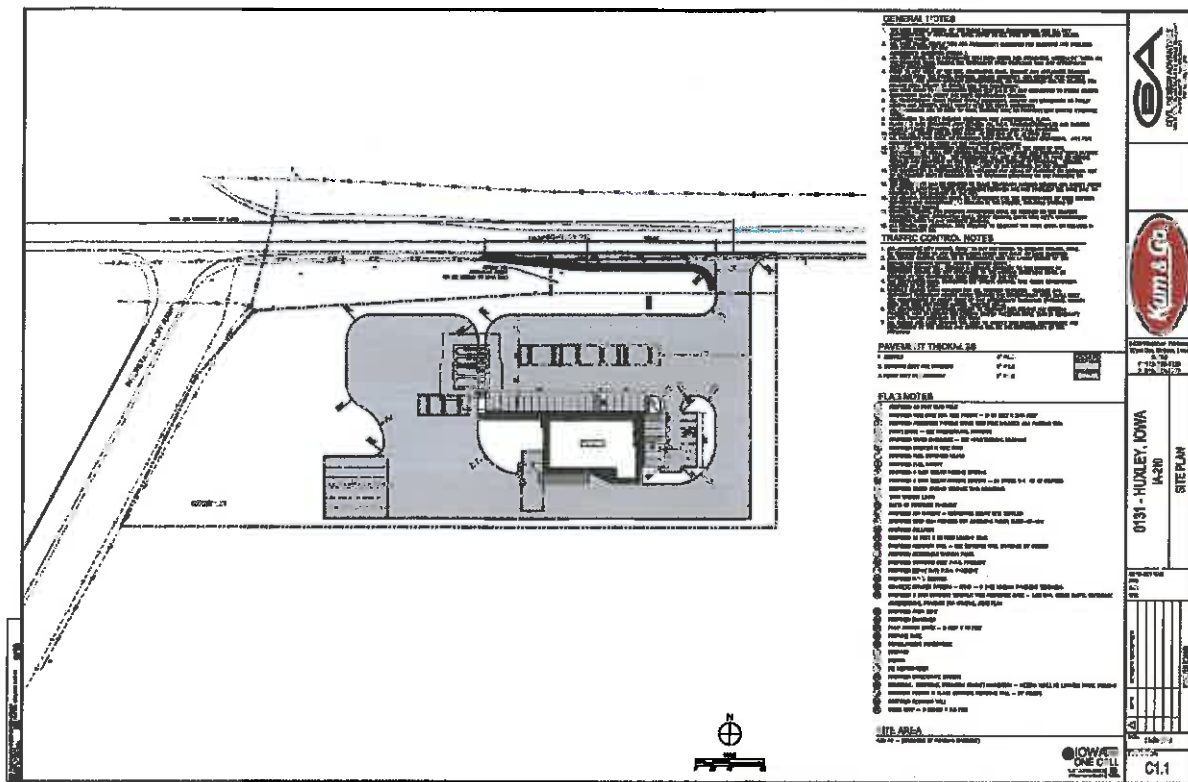


Figure 2 – Site Plan

Trip Generation

Trip generation rates recommended in the *Institute of Transportation Engineers' (ITE) Trip Generation, 9th Edition*, were used to develop estimates of trips to and from the site based on the proposed land use. **Table 1** shows the daily, AM peak hour, and PM peak hour trip generation for the proposed land use. According to the trip generation manual, 66% pass-by trips were calculated for the convenience store with gas pumps land use. Pass-by trips are made by traffic already using the adjacent roadway and enter the site as an intermediate stop on the way to another destination. The trip may not necessarily be “generated” by the land use under study and thus, is not a new trip added to the transportation system. **Table 1** shows the trip generation for the site at full build-out.

Table 1 – Trip Generation

Trip Generation									
Land Use Code	Use	Total SF/Units/Fuel Pos.	Factor	Percent	Entering	Percent	Exit	Pass By	
Daily									
853	Convenience store with gas pumps	18.00	542.6	50%	4883	50%	4883	0	
					4883		4883		
AM									
853	Convenience store with gas pumps	18.00	16.57	50%	51	50%	51	197	
					51		51		
PM									
853	Convenience store with gas pumps	18.00	19.02	50%	58	50%	58	226	
					58		58		

Trip Distribution and Assignments

Based on the trip generation of the proposed land use, the trip ends were assigned to the site entrance. Assignments were based on assumed travel behaviors, location of trip destinations, and accessibility from/to various routes considering normal overall travel patterns.

Using the existing split of traffic calculated from the 2018 traffic counts on Hwy. 210, the trips and pass-by trips were distributed at the intersection. It was assumed that during the AM peak 75% of the traffic travels to/from the east and 25% to/from the west. During the PM peak the assumption is 30% to/from the east and 70% to/from the west. **Figures 3 and 4** show the AM and PM peaks at the new proposed entrance into the proposed Kum & Go 0131 site. **Figures 5 and 6** show the AM and PM peaks at year 2029.

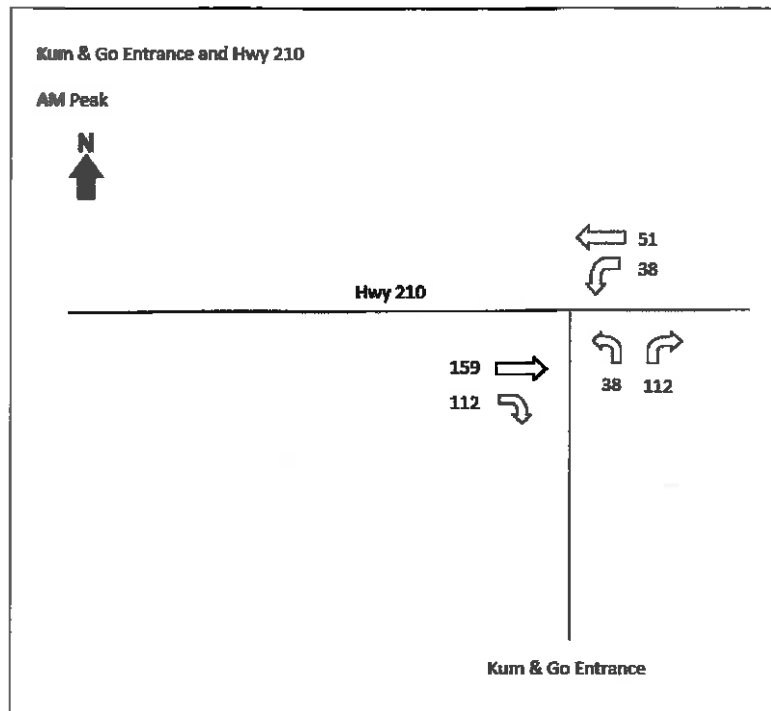


Figure 3 – AM Peak

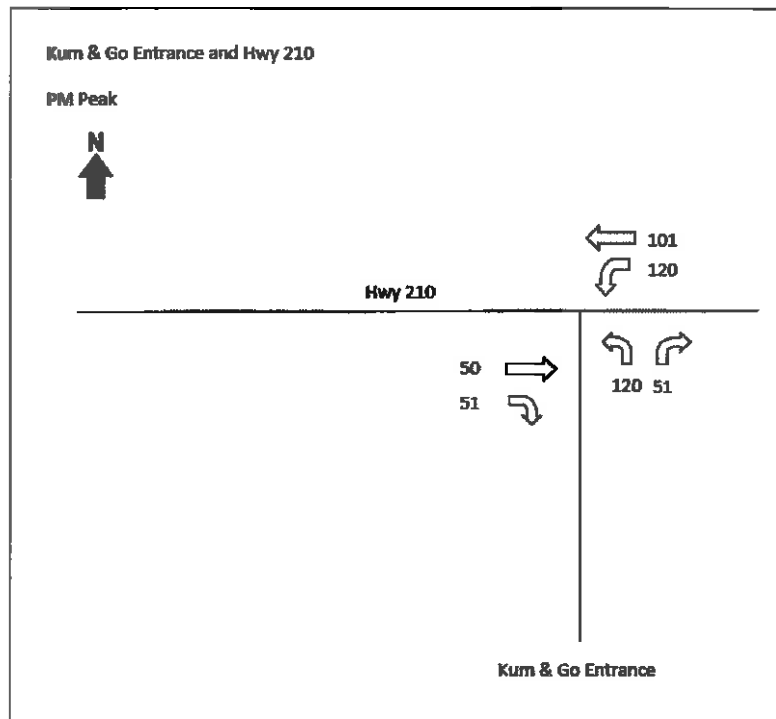


Figure 4 – PM Peak

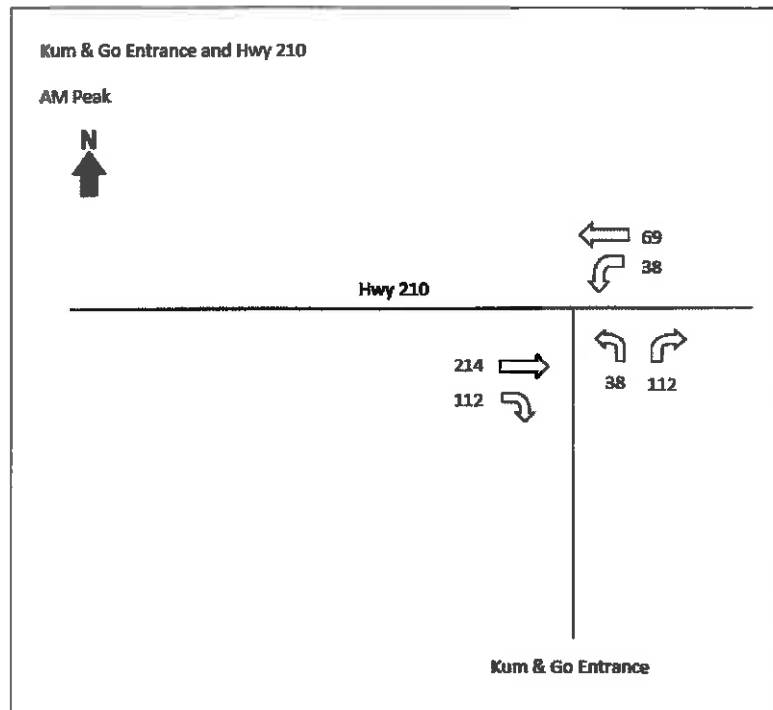


Figure 5 – AM Peak – 2029

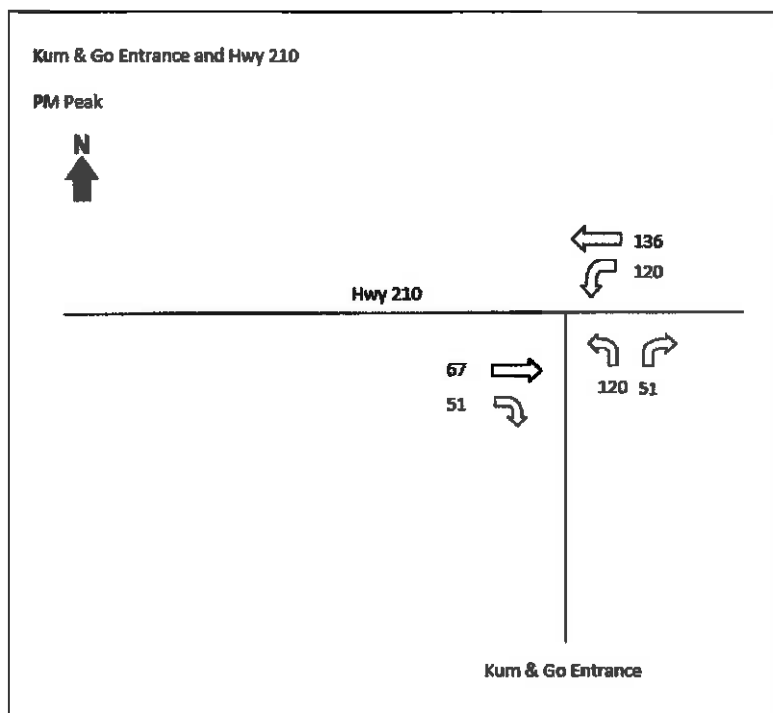


Figure 6 – PM Peak – 2029

Turn Lane Warrants

“NCHRP Report 457: Evaluating Intersection Improvements: An Engineering Study Guide” was used to evaluate the need for right and left turning bays at the proposed site entrance. Figure 7 shows that during the PM peak a right-turn lane would be warranted into the proposed Kum & Go site. Figure 8 shows that a left-turn lane is not warranted at this time. Figure 9 shows that by 2029 a left-turn lane would likely be warranted at the Kum & Go site entrance assuming the 3% annual growth rate.

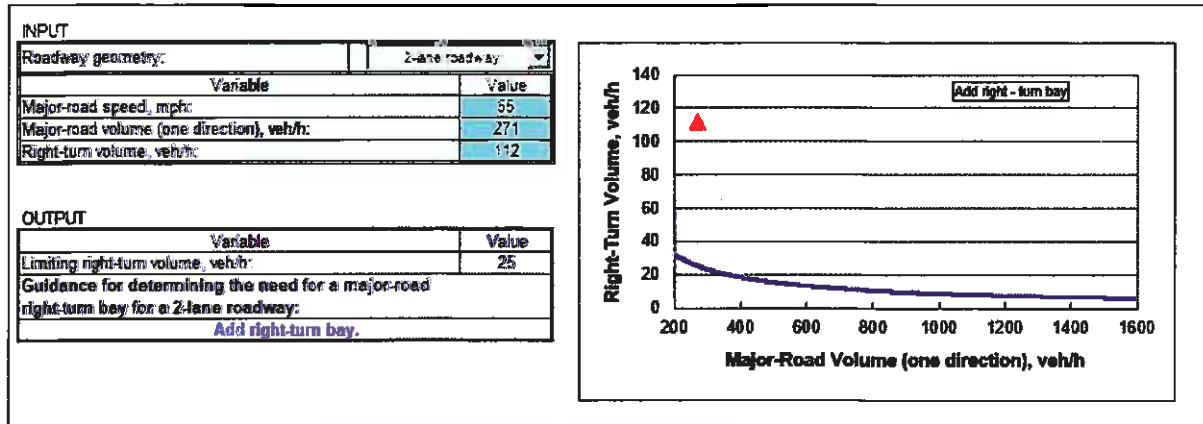


Figure 7 – Guideline for Determining the Need for a Major Road Right Turn Bay

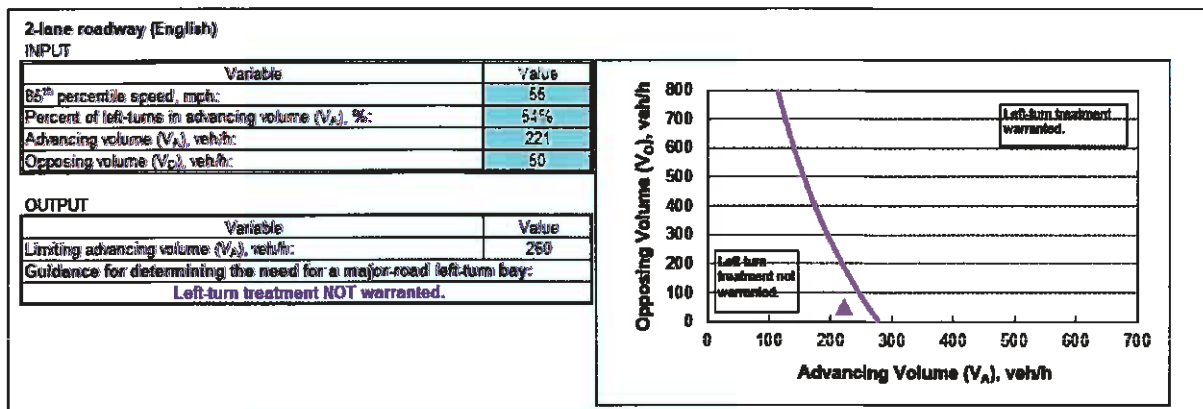


Figure 8 – Guideline for Determining the Need for a Major Road Left Turn Bay

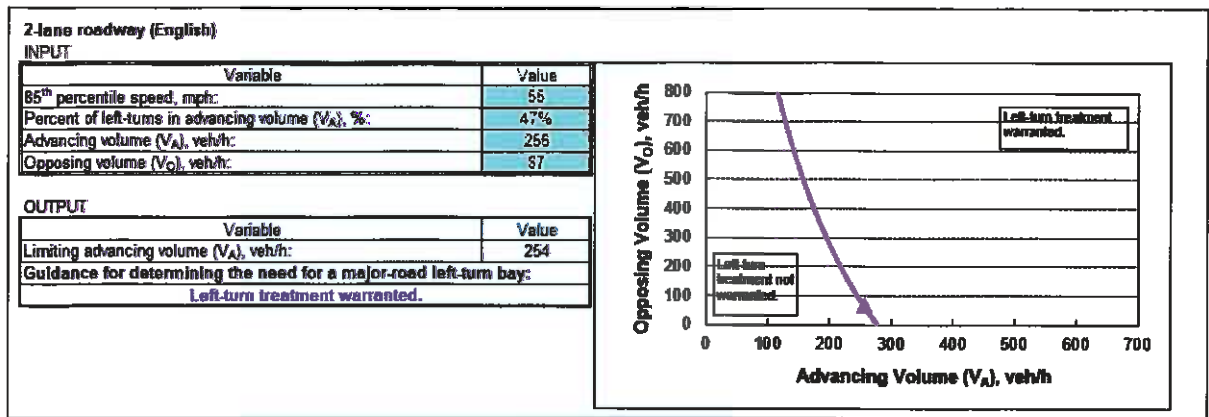


Figure 9 – Guideline for Determining the Need for a Major Road Left Turn Bay

Conclusion and Recommendation

Based on the assumptions stated in the report and resulting analysis, it is recommended that an eastbound right-turn lane on Hwy 210 should be installed when Kum & Go 0131 is developed. A left-turn lane is not warranted at this time. It is estimated that a left-turn lane may be warranted by 2029. It may be necessary to install a left-turn lane earlier if traffic volumes near the site increase at a faster rate than assumed in the analysis, or if traffic slowing down to enter the site starts to cause safety issues for westbound Hwy. 210.

KUM & GO #0131

STORM WATER MANAGEMENT PLAN HUXLEY, IOWA

CDA PROJECT NO. 1811.616



CIVIL DESIGN ADVANTAGE
3405 SE Crossroads Drive, Suite G
GRIMES, IOWA 50111
(515) 369-4400

PREPARED BY: CIVIL DESIGN ADVANTAGE, LLC
PREPARED ON: MARCH 19, 2019
REVISED ON: APRIL 5, 2019

KUM & GO #0131

Summary **1**

Assumptions **2**

Existing & Allowable Runoff Analysis **3**

Post-Development Runoff Analysis **4**

Storm Sewer Design **5**





CIVIL DESIGN ADVANTAGE

3405 SE Crossroads Dr., SUITE G GRIMES, IA 50111

PROJECT: Kum & Go 0131 JOB NO. 1811.616 Page of Pages
SUBJECT: Stormwater Calculations DATE: 04/05/19 COMP. BY: DSH OK'D BY: RAH

Project Description:

Existing Site Conditions

The Kum & Go site is located east of the I-35 ramp intercepting IA-210 in Huxley, Iowa. The existing site consists of 4.30 acres of land utilized for agricultural purposes (row crops) and is slated for a commercial use as a Kum & Go. Refer to the existing drainage map and Hydraflow Hydrographs for detailed analysis of the existing site conditions.

Proposed Site Conditions

The site will be developed as a new 5,975 sf Kum & Go convenience store with a detached gas canopy and associated access drives, parking and utilities. Proposed storm water detention will be provided in a dry bottom detention basin west of the proposed building. (Refer to the Post-Developed Drainage Map and Hydraflow hydrographs).

Storm Water Analysis:

Storm Sewer Analysis

Storm sewer pipes were designed to convey the 100-year post-developed storm event at all critical locations and overflow paths have been provided. The Rational Method was used to determine the flow rate for each drainage area and the Manning's equation was used to size the pipes.

Detention Analysis

Detention for the Kum & Go site will be provided in one dry bottom detention basin located on the west side of the property. The pond was designed with Hydraflow Hydrographs which utilizes the SCS Unit Hydrograph Method for computation of hydrographs. The drainage basin was analyzed for the 2, 5 and 100-year rainfall events. Runoff curve numbers used to determine peak flow rates are listed in the assumptions. The detention basin was designed to limit the 2 and 5-year post-developed runoff to the 2 and 5-year existing peak runoff rate and to limit the 100-year post-developed release rate to the 5-year existing release rate.



CIVIL DESIGN ADVANTAGE

3405 SE Crossroads Dr., SUITE G GRIMES, IA 50111

PROJECT: Kum & Go 0131 JOB NO. 1811.616 Page of Pages
 SUBJECT: Stormwater Calculations DATE: 04/05/19 COMP. BY: DSH OK'D BY: RAH

Assumptions:

- * A time of concentration of 15 minutes was assumed for post developed detention calculations.
- * A USDA Hydrologic Soil Map was prepared for the site. Hydrologic Soil Group B was assumed for storm water runoff calculations. Refer to the attached Hydrologic Soil Map report for soils information.
- * The runoff coefficients used to determine flow rates for the site were taken from SUDAS Section 2B-4.03 are listed in the following table.

Land Use or Surface Characteristics	B Soils	
	5-year	100-year
Impervious Area, (Drives, Walks, and Roofs)	0.95	0.98
Open Space -Grass, >75% (Good Condition)	0.15	0.35

- * The curve numbers used to determine flow rates for the site were taken from SUDAS Section 2B-4.04 and are listed in the following table.

Land Use or Surface Characteristics	Curve Number
Impervious Area, (Drives, Walks, and Roofs)	98
Open Space -Grass, >75% (Good Condition)	61
Row Crops (Contoured)	75

Storm Water Runoff Summary: Drainage Basin 1 (DB 1)

Storm Event	Post-Developed Pond Release, cfs	Detention Elevation	Detention Provided, ft ³	Detention Overflow Elevation	Top of Pond Elevation	Freeboard, ft
2-Year	3.99	999.30	3,319	1001.00	1002.00	2.70
5-Year	4.30	999.75	6,553	1001.00	1002.00	2.25
100-Year	4.92	1000.72	25,499	1001.00	1002.00	1.28

Detention will be provided in a dry-bottom pond (Pond 1). The outlet pipe will consist of a 15" RCP culvert with a 9.60" orifice plate installed in the outlet north side of structure 4 (SW-501) at an elevation of 996.19.

Rainfall Return Frequency (Yrs)	Existing Runoff, cfs	Allowable Release, cfs	Post-Developed Runoff Release, cfs
2-Year	4.00	4.00	3.99
5-Year	6.22	6.22	4.30
100-Year	17.82	6.22	4.92



CIVIL DESIGN ADVANTAGE

3405 SE Crossroads Dr., SUITE G GRIMES, IA 50111

PROJECT: Kum & Go 0131 JOB NO. 1811.616 Page of Pages

SUBJECT: Stormwater Calculations DATE: 03/18/19 COMP. BY: DSH OK'D BY: RAH

**Storm Sewer
Post-Developed Composite C-factor Calculations
100-year**

Drainage Area ID	Lawn B	Lawn Area, SF	Imperv. B	Imperv. Area, SF	Total Area SF	Total Area Acres	Composite C
DA 4	0.35	3,118	0.98	21,764	24,882	0.57	0.90
DA 5	0.35	0	0.98	14,810	14,810	0.34	0.98
DA 6	0.35	0	0.98	20,475	20,475	0.47	0.98
DA 9	0.35	0	0.98	10,064	10,064	0.23	0.98

**Detention
Post-Developed Composite CN Calculations**

Drainage Area ID	Lawn B	Lawn Area, SF	Imperv. B	Imperv. Area, SF	Total Area SF	Total Area Acres	Composite CN
DB 1 POST	61	78,851	98	108,457	187,308	4.30	82



CIVIL DESIGN ADVANTAGE

3405 SE Crossroads Dr., SUITE G GRIMES, IA 50111

PROJECT: Kum & Go 0131 JOB NO. 1811.616 Page of Pages
 SUBJECT: Storm Water Calculations DATE: 02/20/19 COMP. BY: DSH OK'D BY: RAH

Pre-Developed Time of Concentration:Drainage Area: DB 1 EXISTING**Sheet Flow:**

Flow length, L_1 = 100 feet
 Land slope, s_1 = 0.52 %
 Manning's n = 0.17
 2-Year 24-hr p_2 = 3.08
 Travel time, t_1 = 18.9 minutes

Design Equation:

$$t_1 = \frac{0.007[(n)(L_1)]^{0.8}}{\sqrt{p_2(s)}^{0.4}}$$

Shallow Concentrated Flow:

Flow length, L_2 = 342 feet
 Land slope, s_2 = 1.48 %
 Ground Cover No. = 4 Table 1

Flow velocity, v_2 = 1.06 ft/sec
 Travel time, t_2 = 5.4 minutes

Table 1:

Ground Cover:

Forest w/ heavy ground litter & meadow
 Minimum tillage cultivation and woodlands
 Short grass pasture & lawns
 Cultivated straight row crops
 Nearly bare ground
 Grassed waterway
 Paved area & shallow gutter flow

No.	Equation
1	$v_2 = s_2^{1/2} \times 2.516$
2	$v_2 = s_2^{1/2} \times 5.032$
3	$v_2 = s_2^{1/2} \times 6.962$
4	$v_2 = s_2^{1/2} \times 8.726$
5	$v_2 = s_2^{1/2} \times 9.965$
6	$v_2 = s_2^{1/2} \times 16.135$
7	$v_2 = s_2^{1/2} \times 20.238$

Channel Flow:

Flow length, L_3 = 0 feet
 Land slope, s_3 = 1.2 %
 Manning's n = 0.025
 Left Slope = 4:1
 Bottom Width = 5 feet
 Right Slope = 4:1
 Flow depth = 1 feet
 Flow area, a = 9 ft²
 Wetted perim., P_w = 13.25 ft
 Flow velocity, v_3 = 5.03 ft/sec
 Travel time, t_3 = 0.0 minutes

Design Equation:

$$v_3 = \frac{1.486(a/P_w)^{2/3} s_3^{1/2}}{n}$$

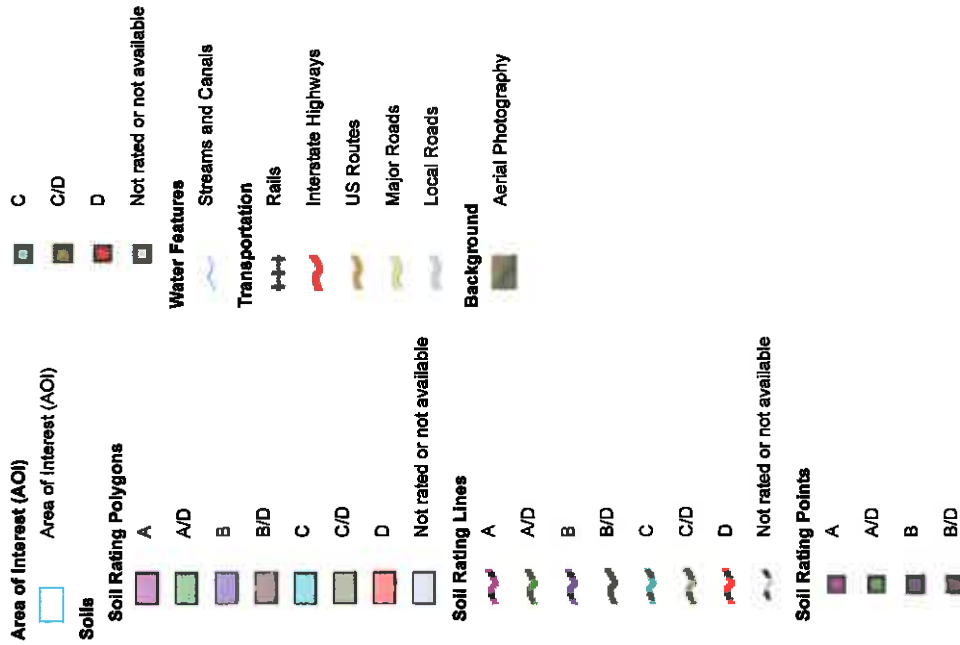
 $q = 45.2911$

Time of Concentration, t_c = 24.3 minutes $t_c = t_1 + t_2 + t_3$

Hydrologic Soil Group—Story County, Iowa



MAP LEGEND



MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Story County, Iowa
Survey Area Data: Version 29, Sep 7, 2018

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jul 26, 2012—Sep 28, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
L55	Nicollet loam, 1 to 3 percent slopes	B/D	14.5	49.4%
L107	Webster clay loam, Bemis moraine, 0 to 2 percent slopes	C/D	7.4	25.2%
L138B	Clarion loam, Bemis moraine, 2 to 6 percent slopes	B	4.5	15.2%
L138C2	Clarion loam, Bemis moraine, 6 to 10 percent slopes, moderately eroded	B	3.0	10.3%
Totals for Area of Interest			29.4	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

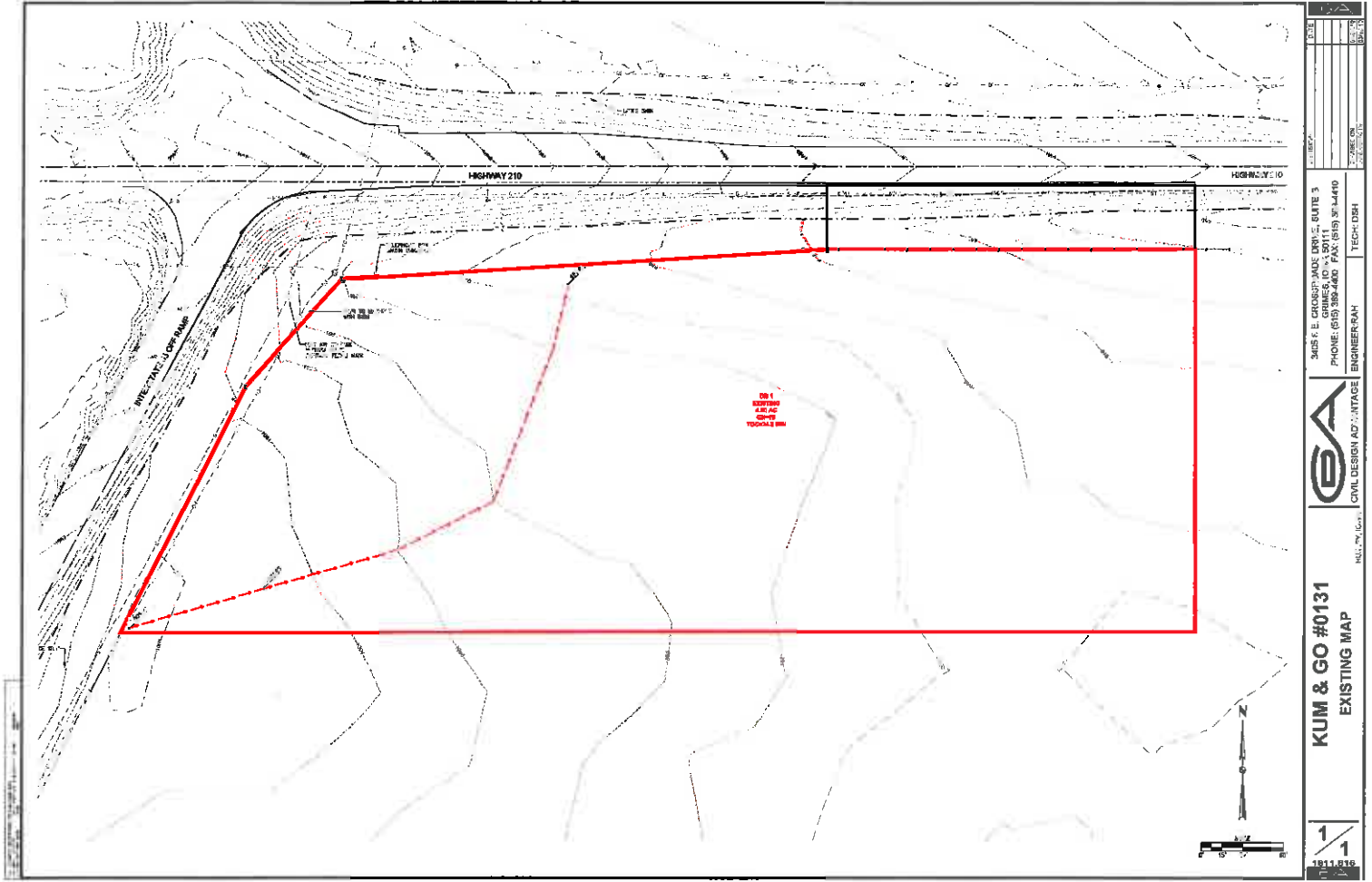
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

Tie-break Rule: Higher



KUM & GO #0131 EXISTING MAP			3405 E. CROSSROADS DRIVE, SUITE 3 PHOENIX, AZ 85044 PHONE: (602) 389-4400 FAX: (602) 389-4401 ENGINEER/AN	TECH: DBN
1 1	100 0 100 FEET	NORTH	100 0 100 FEET	100 0 100 FEET

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Existing.gpw

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Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

1 - DB 1 EXISTING



Legend

<u>Hyd. Origin</u>	<u>Description</u>
1	SCS Runoff DB 1 EXISTING

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	4.003	2	730	15,572	-----	-----	-----	DB 1 EXISTING
Existing.gpw					Return Period: 2 Year			Monday, 03 / 18 / 2019	

Hydrograph Report

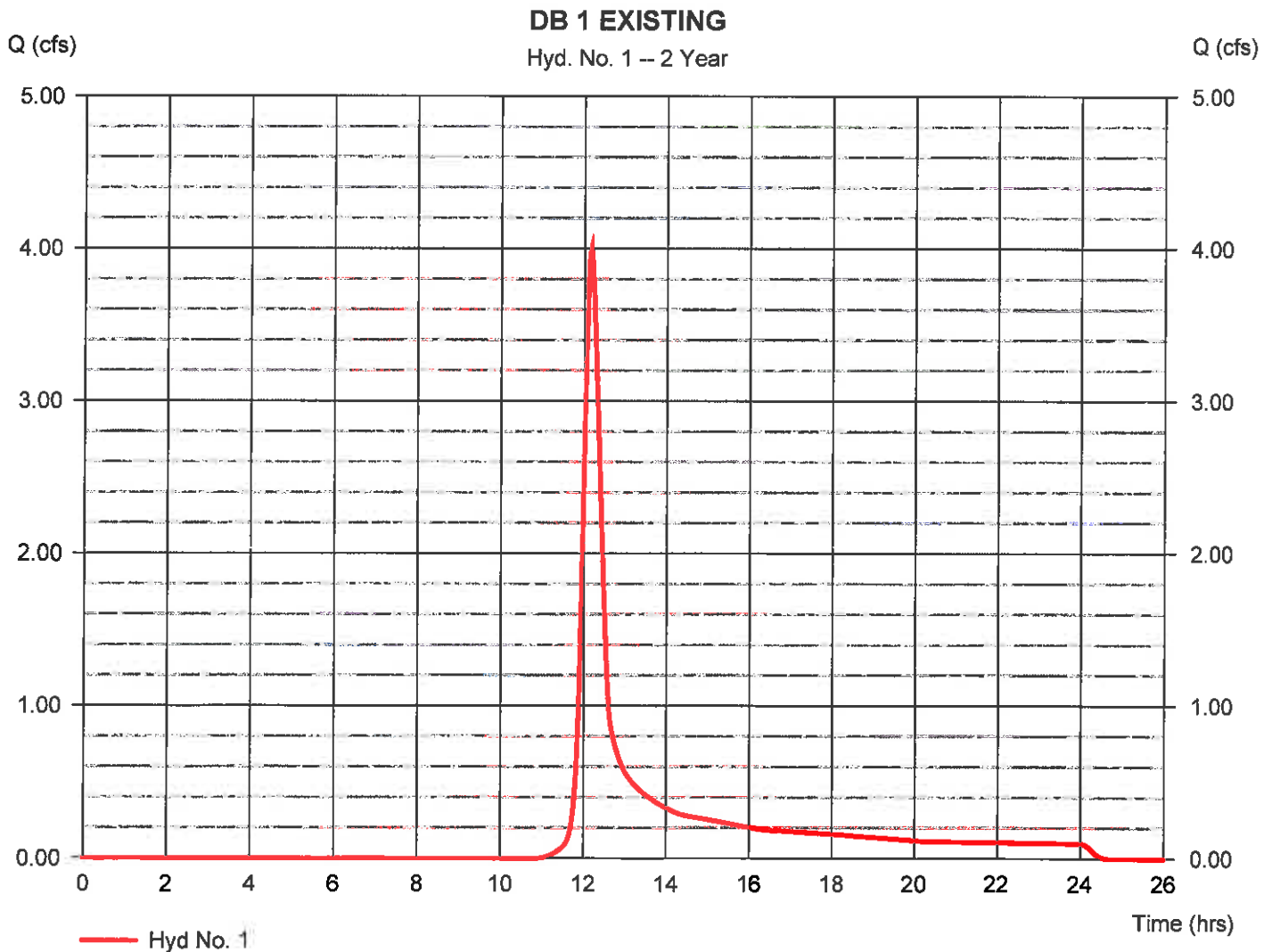
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Monday, 03 / 18 / 2019

Hyd. No. 1

DB 1 EXISTING

Hydrograph type	= SCS Runoff	Peak discharge	= 4.003 cfs
Storm frequency	= 2 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 15,572 cuft
Drainage area	= 4.300 ac	Curve number	= 75
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 24.30 min
Total precip.	= 3.08 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time Interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	6.215	2	730	23,440	----	----	----	DB 1 EXISTING
Existing.gpw					Return Period: 5 Year			Monday, 03 / 18 / 2019	

Hydrograph Report

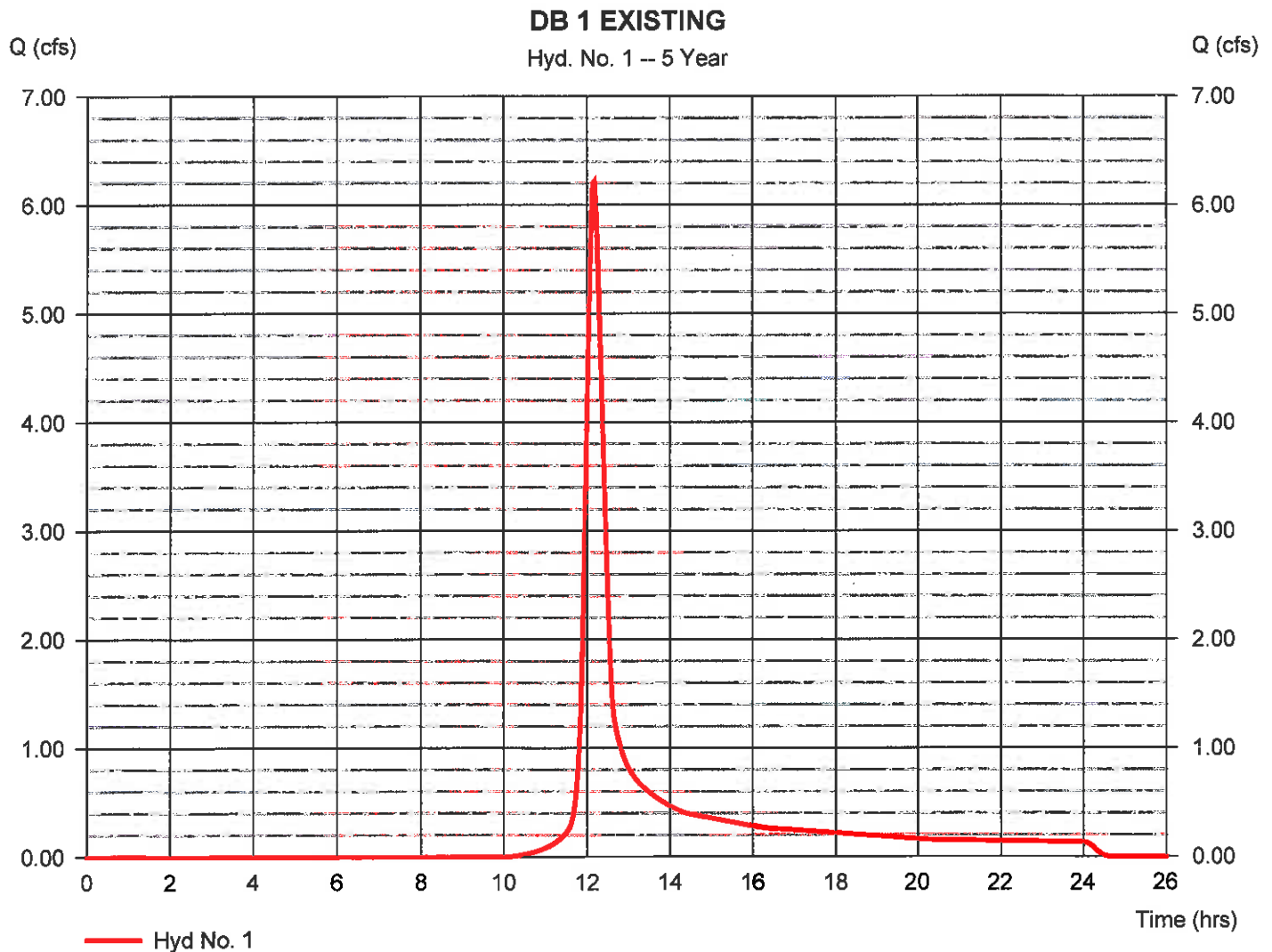
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Monday, 03 / 18 / 2019

Hyd. No. 1

DB 1 EXISTING

Hydrograph type	= SCS Runoff	Peak discharge	= 6.215 cfs
Storm frequency	= 5 yrs	Time to peak	= 12.17 hrs
Time interval	= 2 min	Hyd. volume	= 23,440 cuft
Drainage area	= 4.300 ac	Curve number	= 75
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 24.30 min
Total precip.	= 3.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	17.82	2	728	65,384	-----	-----	-----	DB 1 EXISTING
Existing.gpw					Return Period: 100 Year			Monday, 03 / 18 / 2019	

Hydrograph Report

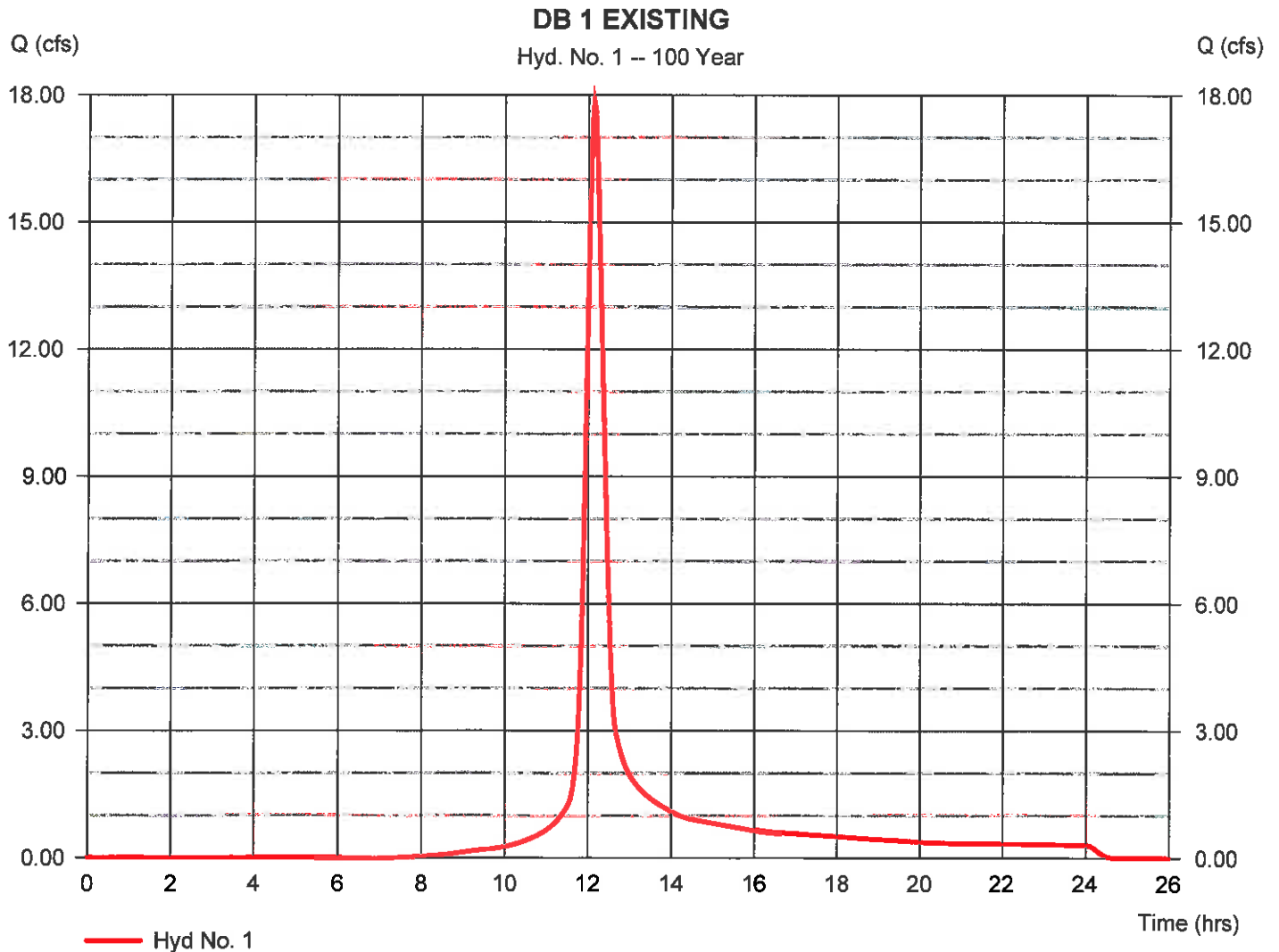
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

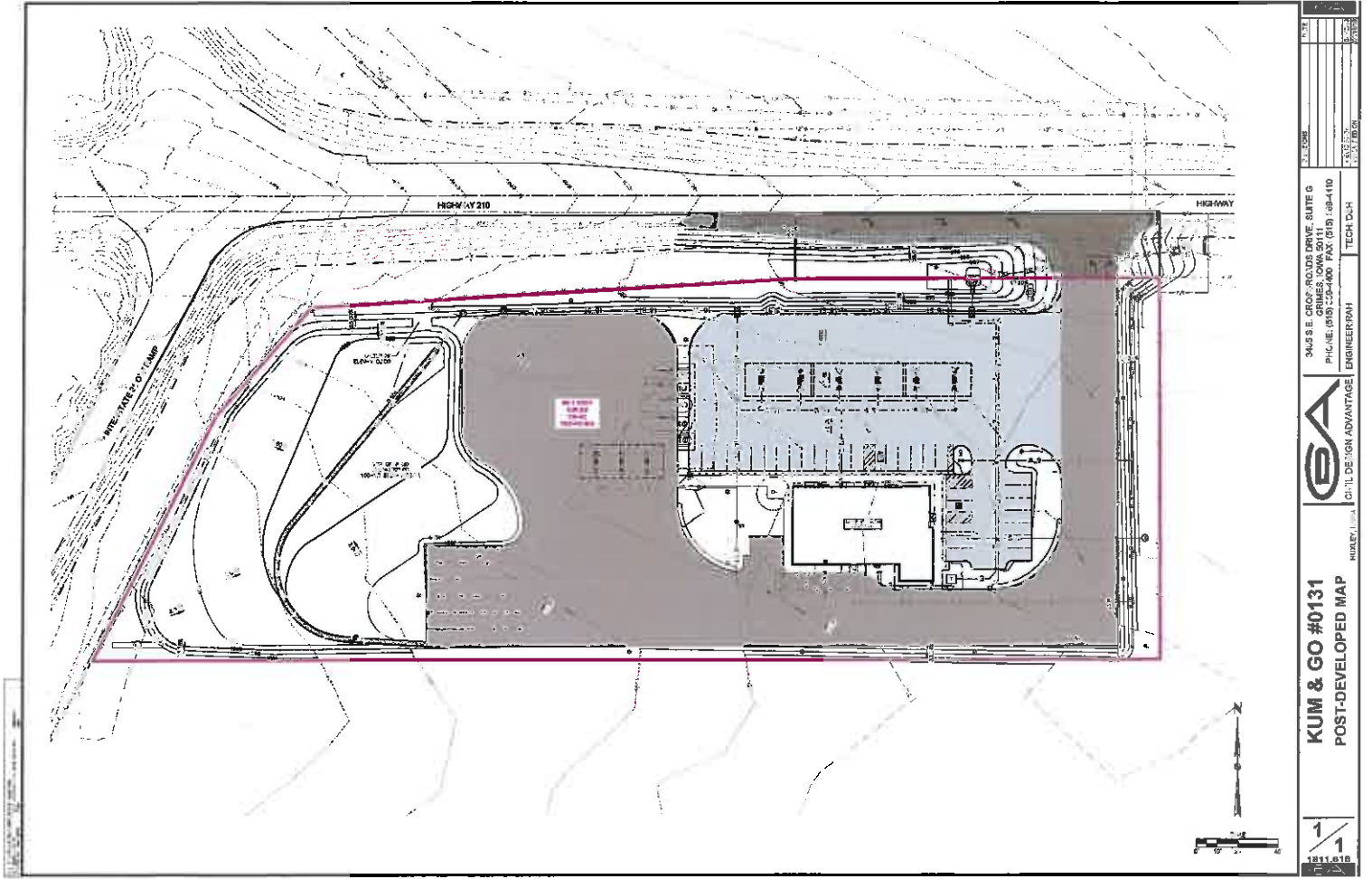
Monday, 03 / 18 / 2019

Hyd. No. 1

DB 1 EXISTING

Hydrograph type	= SCS Runoff	Peak discharge	= 17.82 cfs
Storm frequency	= 100 yrs	Time to peak	= 12.13 hrs
Time interval	= 2 min	Hyd. volume	= 65,384 cuft
Drainage area	= 4.300 ac	Curve number	= 75
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 24.30 min
Total precip.	= 7.12 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484





KUM & GO #0131 POST-DEVELOPED MAP			MASS E. GROUP ARCHITECTURE, SUITE 6 CRIMM, IOWA 50111 PHONE: (515) 225-4000 FAX: (515) 225-4110 ENGINEER/PAH		1" = 40'
1" = 40'			CIVIL DESIGN ADVANTAGE ENGINEER/PAH		1" = 40'

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Post-Developed.gpw

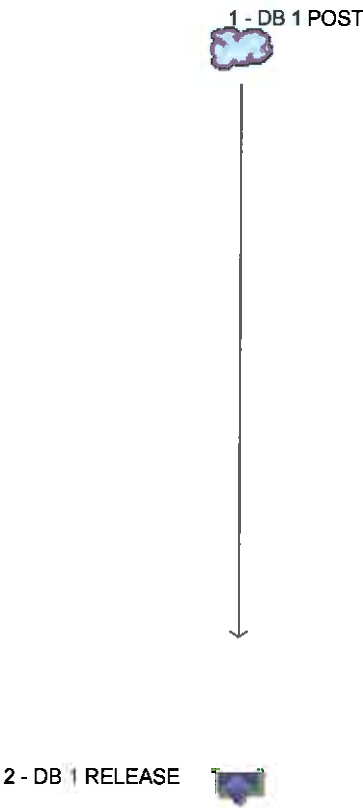
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

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Watershed Model Schematic

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020



Legend

Hyd.	Origin	Description
1	SCS Runoff	DB 1 POST
2	Reservoir	DB 1 RELEASE

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time Interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	7.798	2	722	21,949	---	---	---	DB 1 POST
2	Reservoir	3.986	2	732	21,949	1	999.31	3,361	DB 1 RELEASE
Post-Developed.gpw					Return Period: 2 Year			Wednesday, 04 / 3 / 2019	

Hydrograph Report

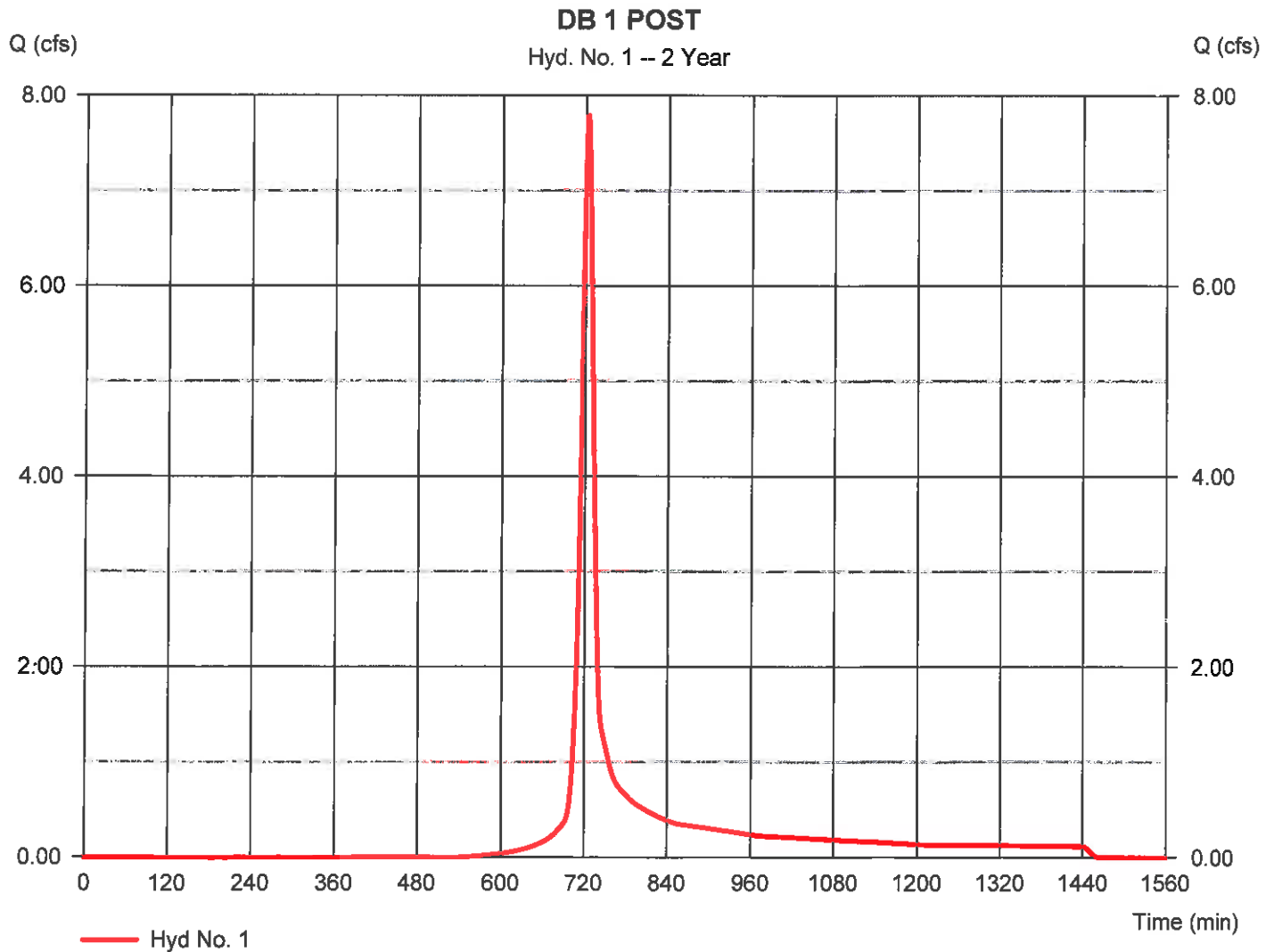
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Wednesday, 04 / 3 / 2019

Hyd. No. 1

DB 1 POST

Hydrograph type	= SCS Runoff	Peak discharge	= 7.798 cfs
Storm frequency	= 2 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 21,949 cuft
Drainage area	= 4.300 ac	Curve number	= 82
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 3.08 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

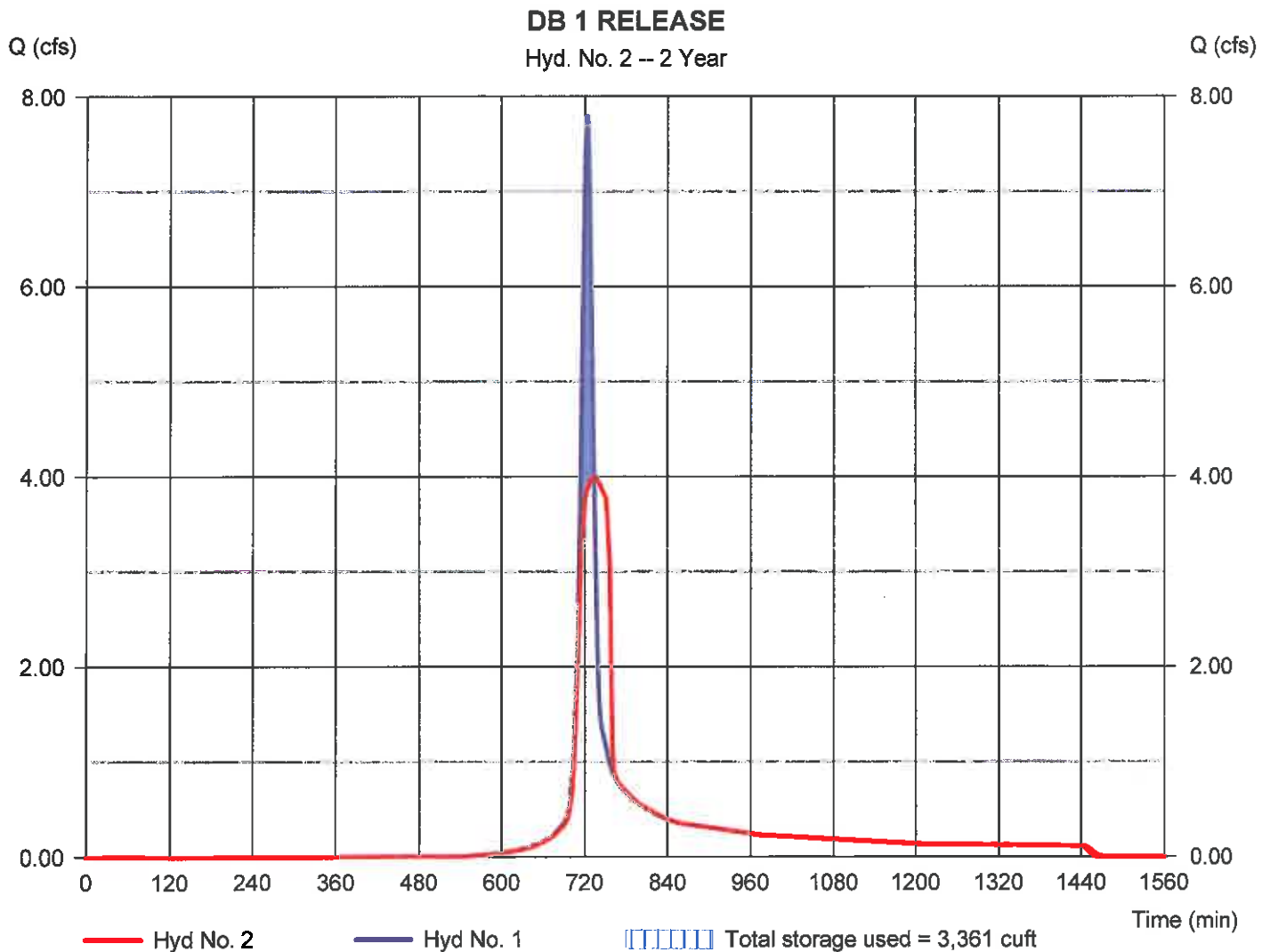
Wednesday, 04 / 3 / 2019

Hyd. No. 2

DB 1 RELEASE

Hydrograph type	= Reservoir	Peak discharge	= 3.986 cfs
Storm frequency	= 2 yrs	Time to peak	= 732 min
Time interval	= 2 min	Hyd. volume	= 21,949 cuft
Inflow hyd. No.	= 1 - DB 1 POST	Max. Elevation	= 999.31 ft
Reservoir name	= POND 1	Max. Storage	= 3,361 cuft

Storage Indication method used.



Pond Report

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Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Wednesday, 04 / 3 / 2019

Pond No. 1 - POND 1

Pond Data

Contours -User-defined contour areas. Average end area method used for volume calculation. Beginning Elevation = 996.19 ft

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	996.19	00	0	0
1.81	998.00	425	385	385
1.96	998.15	425	64	448
2.81	999.00	1,288	728	1,176
3.81	1000.00	13,139	7,214	8,390
4.81	1001.00	34,433	23,786	32,176
5.81	1002.00	46,836	40,634	72,810

Culvert / Orifice Structures

	[A]	[B]	[C]	[PrfRsr]
Rise (in)	= 9.60	0.00	0.00	0.00
Span (in)	= 9.60	0.00	0.00	0.00
No. Barrels	= 1	0	0	0
Invert El. (ft)	= 996.19	0.00	0.00	0.00
Length (ft)	= 17.00	0.00	0.00	0.00
Slope (%)	= 0.50	0.00	0.00	n/a
N-Value	= .013	.013	.013	n/a
Orifice Coeff.	= 0.60	0.60	0.60	0.60
Multi-Stage	= n/a	No	No	No

Weir Structures

	[A]	[B]	[C]	[D]
Crest Len (ft)	= 10.00	0.00	0.00	0.00
Crest El. (ft)	= 1001.00	0.00	0.00	0.00
Weir Coeff.	= 2.60	3.33	3.33	3.33
Weir Type	= Broad	---	---	---
Multi-Stage	= No	No	No	No
Exfil.(in/hr)	= 0.000 (by Wet area)			
TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PrfRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
0.00	0	996.19	0.00	---	---	---	0.00	---	---	---	---	---	0.000
0.18	38	996.37	0.11 oc	---	---	---	0.00	---	---	---	---	---	0.114
0.36	77	996.55	0.34 oc	---	---	---	0.00	---	---	---	---	---	0.343
0.54	115	996.73	0.59 oc	---	---	---	0.00	---	---	---	---	---	0.590
0.72	154	996.91	0.78 oc	---	---	---	0.00	---	---	---	---	---	0.780
0.90	192	997.10	1.18 oc	---	---	---	0.00	---	---	---	---	---	1.184
1.09	231	997.28	1.65 oc	---	---	---	0.00	---	---	---	---	---	1.653
1.27	269	997.46	2.02 oc	---	---	---	0.00	---	---	---	---	---	2.017
1.45	308	997.64	2.32 oc	---	---	---	0.00	---	---	---	---	---	2.324
1.63	346	997.82	2.60 oc	---	---	---	0.00	---	---	---	---	---	2.595
1.81	385	998.00	2.84 oc	---	---	---	0.00	---	---	---	---	---	2.840
1.83	391	998.02	2.86 oc	---	---	---	0.00	---	---	---	---	---	2.859
1.84	397	998.03	2.88 oc	---	---	---	0.00	---	---	---	---	---	2.879
1.86	404	998.05	2.90 oc	---	---	---	0.00	---	---	---	---	---	2.898
1.87	410	998.06	2.92 oc	---	---	---	0.00	---	---	---	---	---	2.917
1.89	417	998.08	2.94 oc	---	---	---	0.00	---	---	---	---	---	2.936
1.90	423	998.09	2.95 oc	---	---	---	0.00	---	---	---	---	---	2.954
1.92	429	998.11	2.97 oc	---	---	---	0.00	---	---	---	---	---	2.973
1.93	436	998.12	2.99 oc	---	---	---	0.00	---	---	---	---	---	2.992
1.95	442	998.14	3.01 ic	---	---	---	0.00	---	---	---	---	---	3.008
1.96	448	998.15	3.02 ic	---	---	---	0.00	---	---	---	---	---	3.023
2.05	521	998.24	3.10 ic	---	---	---	0.00	---	---	---	---	---	3.104
2.13	594	998.32	3.18 ic	---	---	---	0.00	---	---	---	---	---	3.183
2.22	667	998.41	3.26 ic	---	---	---	0.00	---	---	---	---	---	3.260
2.30	740	998.49	3.34 ic	---	---	---	0.00	---	---	---	---	---	3.336
2.39	812	998.58	3.41 ic	---	---	---	0.00	---	---	---	---	---	3.410
2.47	885	998.66	3.48 ic	---	---	---	0.00	---	---	---	---	---	3.482
2.56	958	998.75	3.55 ic	---	---	---	0.00	---	---	---	---	---	3.553
2.64	1,031	998.83	3.62 ic	---	---	---	0.00	---	---	---	---	---	3.622
2.73	1,104	998.92	3.69 ic	---	---	---	0.00	---	---	---	---	---	3.690
2.81	1,176	999.00	3.76 ic	---	---	---	0.00	---	---	---	---	---	3.757
2.91	1,898	999.10	3.83 ic	---	---	---	0.00	---	---	---	---	---	3.834
3.01	2,619	999.20	3.91 ic	---	---	---	0.00	---	---	---	---	---	3.910
3.11	3,340	999.30	3.98 ic	---	---	---	0.00	---	---	---	---	---	3.984
3.21	4,062	999.40	4.06 ic	---	---	---	0.00	---	---	---	---	---	4.057
3.31	4,783	999.50	4.13 ic	---	---	---	0.00	---	---	---	---	---	4.128

Continues on next page...

POND 1

Stage / Storage / Discharge Table

Stage ft	Storage cuft	Elevation ft	Clv A cfs	Clv B cfs	Clv C cfs	PriRsr cfs	Wr A cfs	Wr B cfs	Wr C cfs	Wr D cfs	Exfil cfs	User cfs	Total cfs
3.41	5,504	999.60	4.20 ic	---	---	---	0.00	---	---	---	---	---	4.198
3.51	6,226	999.70	4.27 ic	---	---	---	0.00	---	---	---	---	---	4.268
3.61	6,947	999.80	4.34 ic	---	---	---	0.00	---	---	---	---	---	4.336
3.71	7,669	999.90	4.40 ic	---	---	---	0.00	---	---	---	---	---	4.403
3.81	8,390	1000.00	4.47 ic	---	---	---	0.00	---	---	---	---	---	4.469
3.91	10,768	1000.10	4.53 ic	---	---	---	0.00	---	---	---	---	---	4.534
4.01	13,147	1000.20	4.60 ic	---	---	---	0.00	---	---	---	---	---	4.598
4.11	15,526	1000.30	4.66 ic	---	---	---	0.00	---	---	---	---	---	4.661
4.21	17,904	1000.40	4.72 ic	---	---	---	0.00	---	---	---	---	---	4.724
4.31	20,283	1000.50	4.79 ic	---	---	---	0.00	---	---	---	---	---	4.785
4.41	22,661	1000.60	4.85 ic	---	---	---	0.00	---	---	---	---	---	4.846
4.51	25,040	1000.70	4.91 ic	---	---	---	0.00	---	---	---	---	---	4.906
4.61	27,419	1000.80	4.97 ic	---	---	---	0.00	---	---	---	---	---	4.965
4.71	29,797	1000.90	5.02 ic	---	---	---	0.00	---	---	---	---	---	5.024
4.81	32,176	1001.00	5.08 ic	---	---	---	0.00	---	---	---	---	---	5.082
4.91	36,239	1001.10	5.14 ic	---	---	---	0.82	---	---	---	---	---	5.961
5.01	40,303	1001.20	5.20 ic	---	---	---	2.32	---	---	---	---	---	7.521
5.11	44,366	1001.30	5.25 ic	---	---	---	4.27	---	---	---	---	---	9.523
5.21	48,430	1001.40	5.31 ic	---	---	---	6.58	---	---	---	---	---	11.88
5.31	52,493	1001.50	5.36 ic	---	---	---	9.19	---	---	---	---	---	14.55
5.41	56,557	1001.60	5.42 ic	---	---	---	12.08	---	---	---	---	---	17.50
5.51	60,620	1001.70	5.47 ic	---	---	---	15.22	---	---	---	---	---	20.69
5.61	64,683	1001.80	5.52 ic	---	---	---	18.60	---	---	---	---	---	24.12
5.71	68,747	1001.90	5.58 ic	---	---	---	22.19	---	---	---	---	---	27.77
5.81	72,810	1002.00	5.63 ic	---	---	---	26.00	---	---	---	---	---	31.63

...End

Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	11.08	2	722	31,070	-----	-----	-----	DB 1 POST
2	Reservoir	4.298	2	734	31,070	1	999.75	6,553	DB 1 RELEASE
					</				

Hydrograph Report

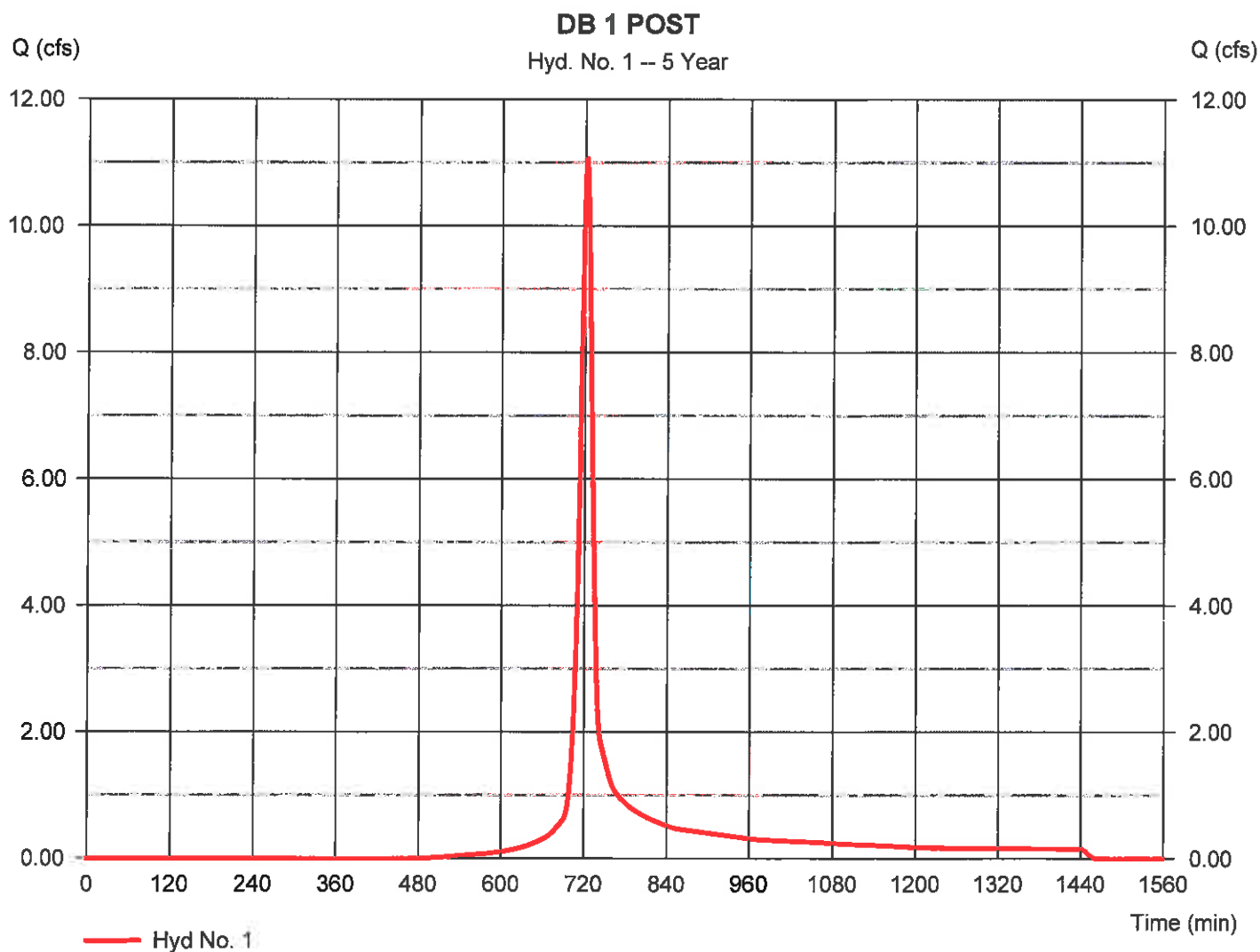
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Wednesday, 04 / 3 / 2019

Hyd. No. 1

DB 1 POST

Hydrograph type	= SCS Runoff	Peak discharge	= 11.08 cfs
Storm frequency	= 5 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 31,070 cuft
Drainage area	= 4.300 ac	Curve number	= 82
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 3.81 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

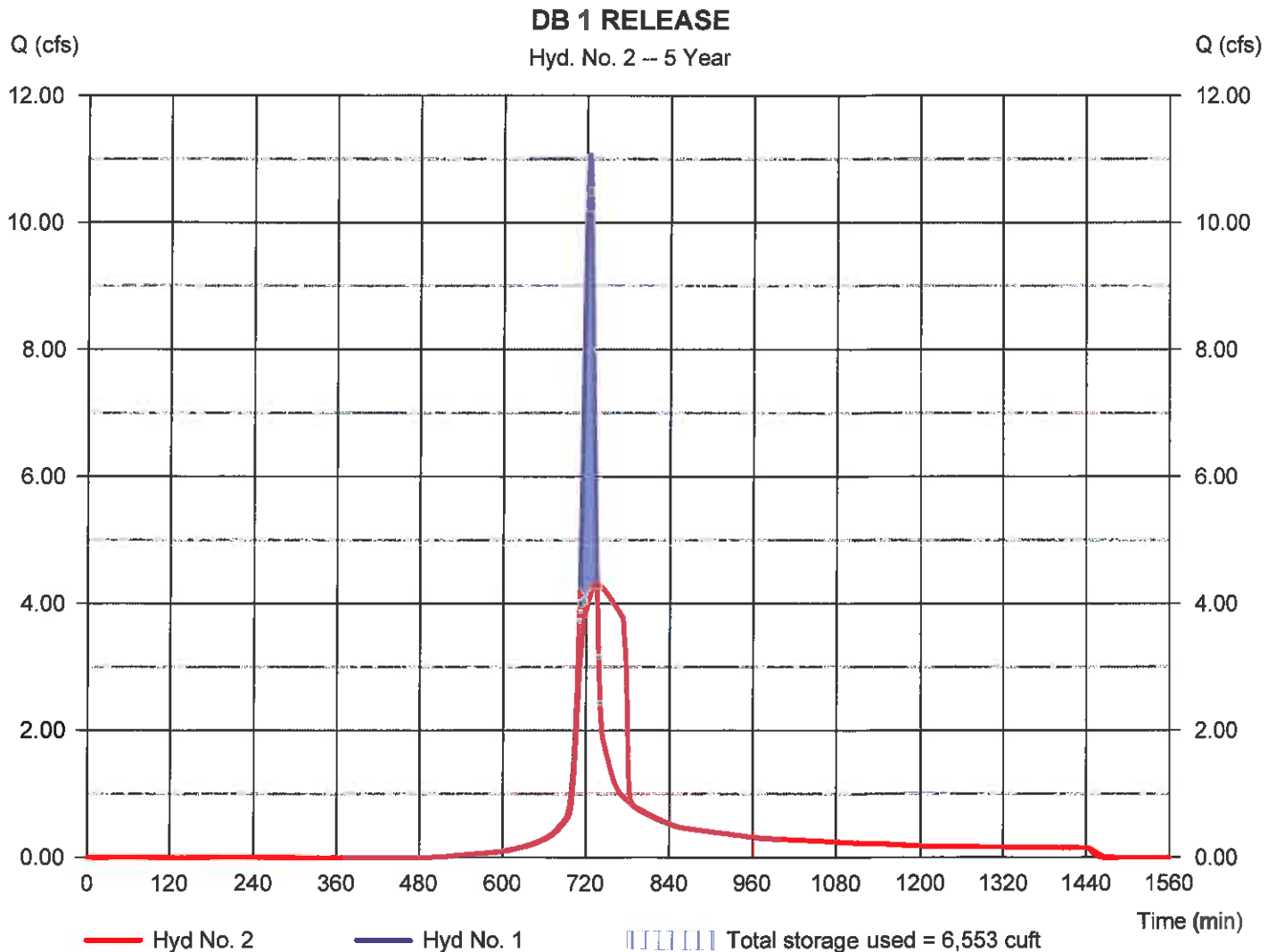
Wednesday, 04 / 3 / 2019

Hyd. No. 2

DB 1 RELEASE

Hydrograph type	= Reservoir	Peak discharge	= 4.298 cfs
Storm frequency	= 5 yrs	Time to peak	= 734 min
Time interval	= 2 min	Hyd. volume	= 31,070 cuft
Inflow hyd. No.	= 1 - DB 1 POST	Max. Elevation	= 999.75 ft
Reservoir name	= POND 1	Max. Storage	= 6,553 cuft

Storage Indication method used.



Hydrograph Summary Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	SCS Runoff	26.78	2	722	76,531	-----	-----	-----	DB 1 POST
2	Reservoir	4.917	2	740	76,531	1	1000.72	25,483	DB 1 RELEASE

Hydrograph Report

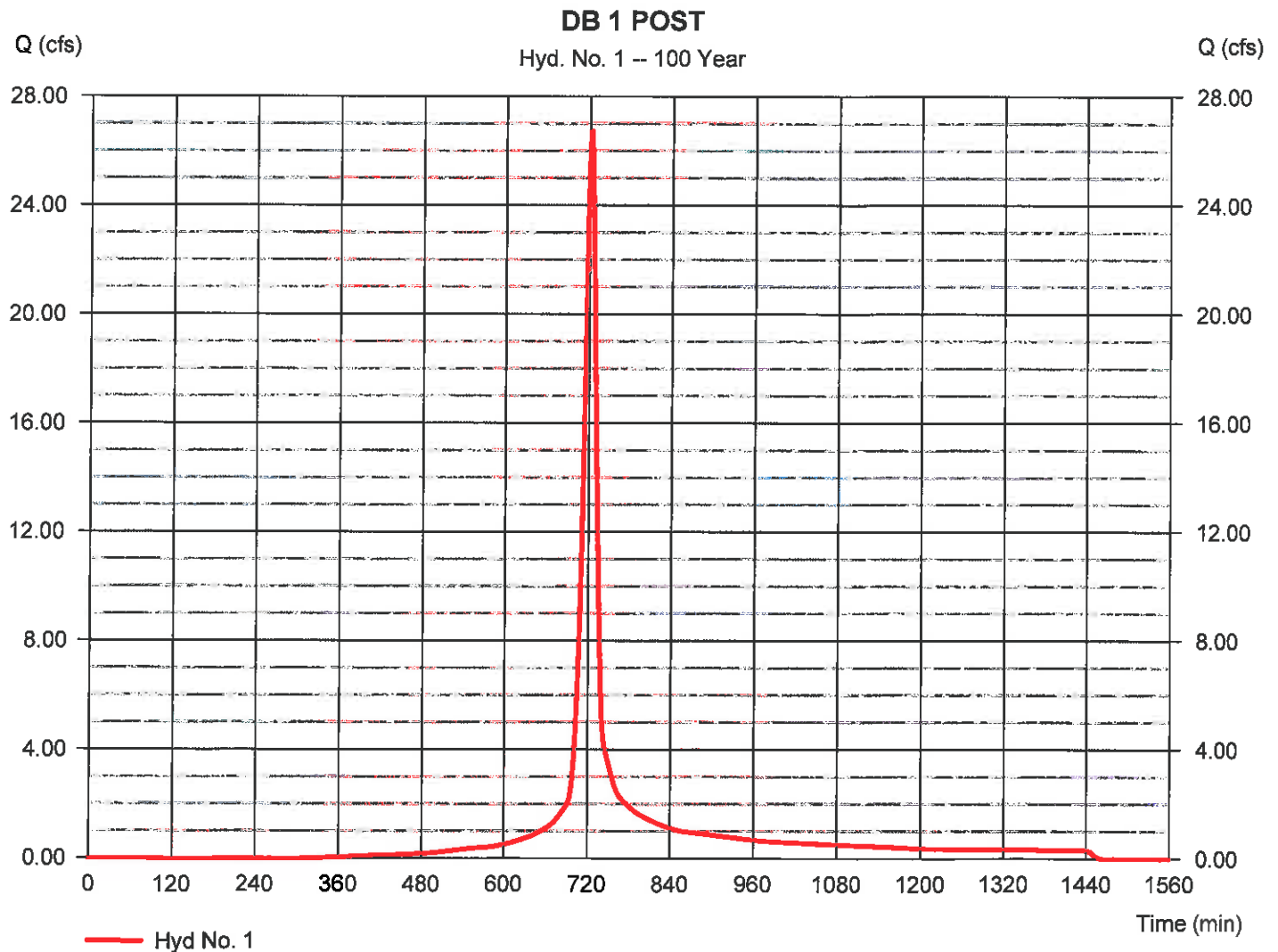
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Wednesday, 04 / 3 / 2019

Hyd. No. 1

DB 1 POST

Hydrograph type	= SCS Runoff	Peak discharge	= 26.78 cfs
Storm frequency	= 100 yrs	Time to peak	= 722 min
Time interval	= 2 min	Hyd. volume	= 76,531 cuft
Drainage area	= 4.300 ac	Curve number	= 82
Basin Slope	= 0.0 %	Hydraulic length	= 0 ft
Tc method	= User	Time of conc. (Tc)	= 15.00 min
Total precip.	= 7.12 in	Distribution	= Type II
Storm duration	= 24 hrs	Shape factor	= 484



Hydrograph Report

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

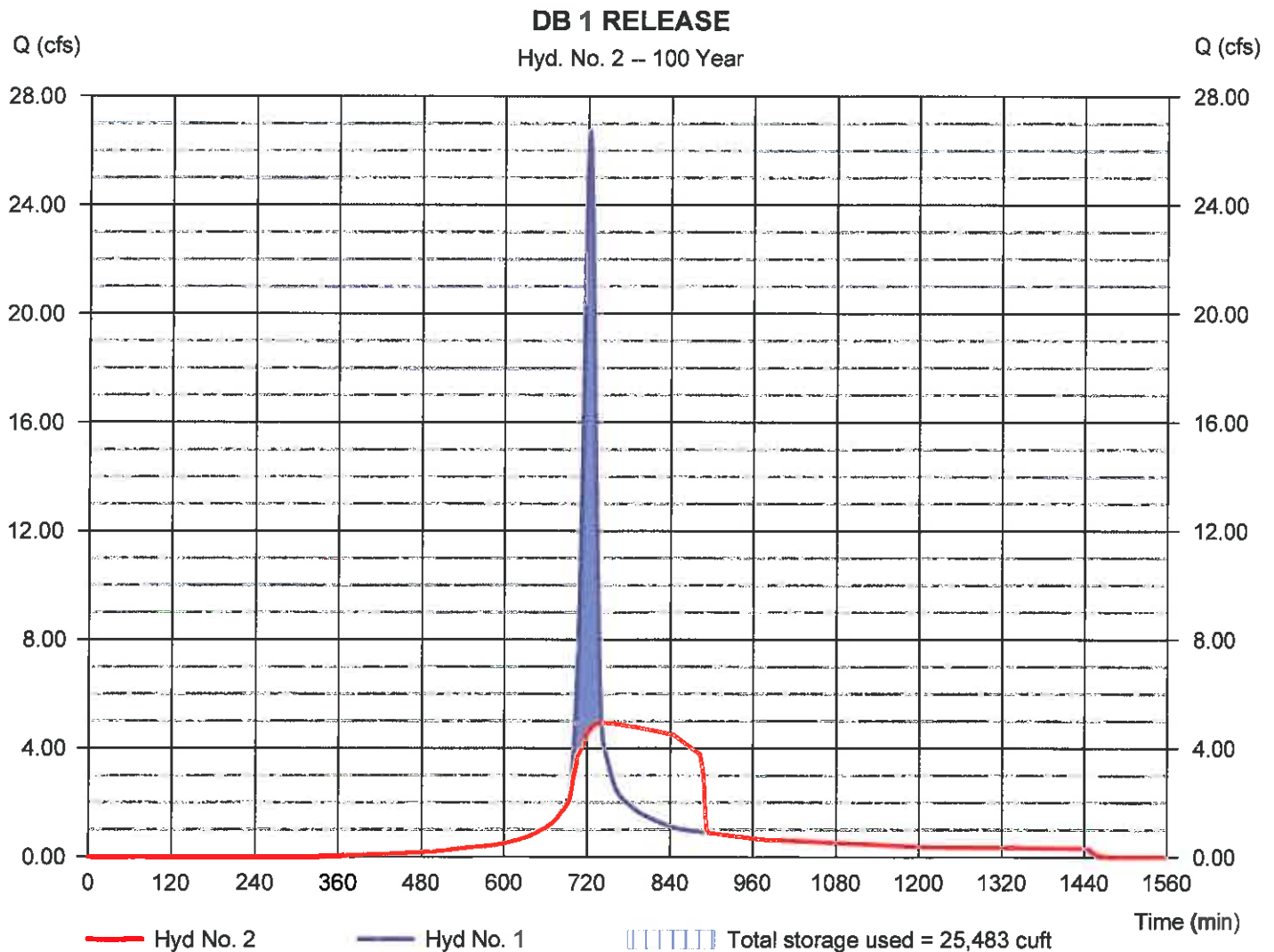
Wednesday, 04 / 3 / 2019

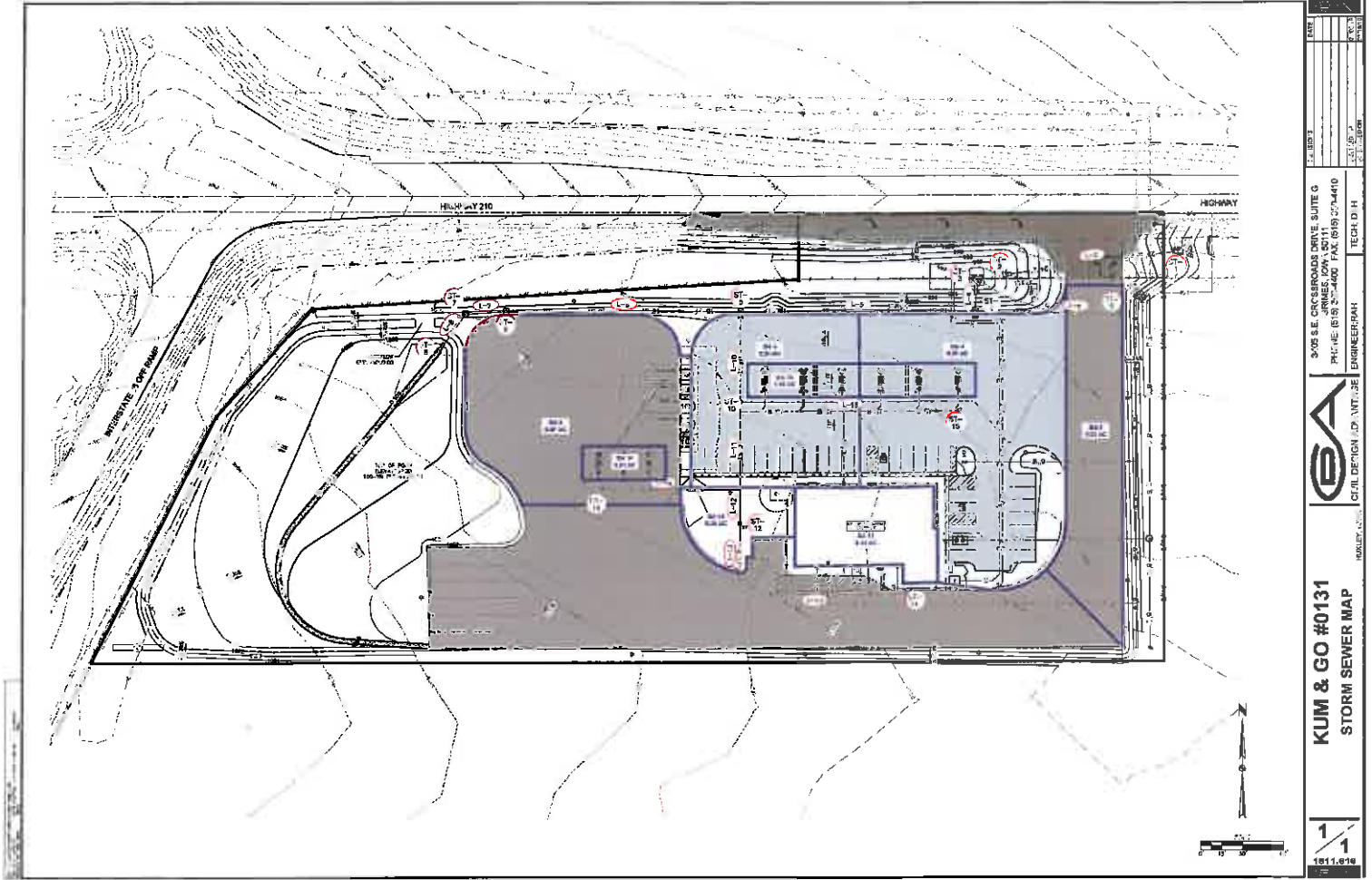
Hyd. No. 2

DB 1 RELEASE

Hydrograph type	= Reservoir	Peak discharge	= 4.917 cfs
Storm frequency	= 100 yrs	Time to peak	= 740 min
Time interval	= 2 min	Hyd. volume	= 76,531 cuft
Inflow hyd. No.	= 1 - DB 1 POST	Max. Elevation	= 1000.72 ft
Reservoir name	= POND 1	Max. Storage	= 25,483 cuft

Storage Indication method used.





List of Intakes and Utility Accesses				
Structure Number	Location	Type of Structure	FL TO / RIM ELEVATION	Note
ST-1		12" R.P. MANHOLE	FL= 882.55	
ST-2		12" R.P. MANHOLE	FL= 882.55	
ST-3		12" R.P. MANHOLE	FL= 882.55	
ST-4		12" R.P. MANHOLE	FL= 882.55	
ST-5		12" R.P. MANHOLE	FL= 882.55	
ST-6		12" R.P. MANHOLE	FL= 882.55	
ST-7		12" R.P. MANHOLE	FL= 882.55	
ST-8		12" R.P. MANHOLE	FL= 882.55	
ST-9		12" R.P. MANHOLE	FL= 882.55	
ST-10		12" R.P. MANHOLE	FL= 882.55	
ST-11		12" R.P. MANHOLE	FL= 882.55	
ST-12		12" R.P. MANHOLE	FL= 882.55	
ST-13		12" R.P. MANHOLE	FL= 882.55	
ST-14		12" R.P. MANHOLE	FL= 882.55	
ST-15		12" R.P. MANHOLE	FL= 882.55	
ST-16		12" R.P. MANHOLE	FL= 882.55	
ST-17		12" R.P. MANHOLE	FL= 882.55	
ST-18		12" R.P. MANHOLE	FL= 882.55	
ST-19		12" R.P. MANHOLE	FL= 882.55	
ST-20		12" R.P. MANHOLE	FL= 882.55	

Notes:

List of Storm Sewer Pipe									
Pipe Number	From Station	To Station	Length (ft)	Material	Flow (cfs)	Velocity (ft/s)	Head Loss (ft)	Notes	Remarks
ST-1	0+00	0+10	10	R.P.	0.00	0.00	0.00		
ST-2	0+10	0+20	10	R.P.	0.00	0.00	0.00		
ST-3	0+20	0+30	10	R.P.	0.00	0.00	0.00		
ST-4	0+30	0+40	10	R.P.	0.00	0.00	0.00		
ST-5	0+40	0+50	10	R.P.	0.00	0.00	0.00		
ST-6	0+50	0+60	10	R.P.	0.00	0.00	0.00		
ST-7	0+60	0+70	10	R.P.	0.00	0.00	0.00		
ST-8	0+70	0+80	10	R.P.	0.00	0.00	0.00		
ST-9	0+80	0+90	10	R.P.	0.00	0.00	0.00		
ST-10	0+90	1+00	10	R.P.	0.00	0.00	0.00		
ST-11	1+00	1+10	10	R.P.	0.00	0.00	0.00		
ST-12	1+10	1+20	10	R.P.	0.00	0.00	0.00		
ST-13	1+20	1+30	10	R.P.	0.00	0.00	0.00		
ST-14	1+30	1+40	10	R.P.	0.00	0.00	0.00		
ST-15	1+40	1+50	10	R.P.	0.00	0.00	0.00		
ST-16	1+50	1+60	10	R.P.	0.00	0.00	0.00		
ST-17	1+60	1+70	10	R.P.	0.00	0.00	0.00		
ST-18	1+70	1+80	10	R.P.	0.00	0.00	0.00		
ST-19	1+80	1+90	10	R.P.	0.00	0.00	0.00		
ST-20	1+90	2+00	10	R.P.	0.00	0.00	0.00		

Notes:
1. INCLUDE APPROPRIATE LENGTH

Storm Sewer Pipe Design Information														
Station	Flow (cfs)	Velocity (ft/s)	Head Loss (ft)	Time (min)	Time (hr)	Time (day)	Time (week)	Time (month)	Time (year)	Time (decade)	Time (century)	Time (millennium)	Time (billion years)	Time (trillion years)
ST-1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-16	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-17	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-18	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ST-20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Notes:
1. PRELIMINARY DESIGN IS A CULVERT WITH HY-1
2. REFER TO DETENTION COMPUTATION (PLEASE Q.10.1.2.2)



CIVIL DESIGN ADVANTAGE

3405 SE CROSSROADS DR., SUITE G GRIMES, IA 50111

PROJECT: Kum & Go 0131 JOB NO. 1811.616 Page of PagesSUBJECT: Storm Water Calculations DATE: 04/04/19 DESIGNED: DSH CHECKED: **INTAKE ST-4 CAPACITY CALCUALTIONS****EQUATIONS**

1. ORIFICE: $Q = 0.6 A (2gh)^{1/2}$

$Q_{100} = C_{100} I_{100} A$

Assume a Time of Concentration = 15 min.

WHERE - Q = flow, cfs

A = area of opening, ft²g = gravity (32.2 ft/s²)

h = headwater from center of opening, ft

$C_{100} = 0.98$

$I_{100} = 7.44 \text{ in/hr}$

$A = 0.57 \text{ acres}$

$Q_{100} = 0.70 * 7.44 * 0.47$

$Q_{100} = 4.16 \text{ cfs}$

2. WEIR: $Q = 3.3 * P * h^{1.5}$

WHERE - Q = flow, cfs

P = Perimeter of grate in feet

h = headwater from center of opening, ft

CALCULATIONS**1. Solve for required head given flow and open area for casting using Orifice Equation:**LOCATION: **ST-4**INPUT: $Q_{100} = 4.16 \text{ cfs}$ (From Rational Equation) $A = 1.95 \text{ sq. ft.}$ (Open Area of Casting)

Type 3B, 24" Beehive grate

Required Head at Grate: $h = 0.196 \text{ ft.}$ **2. Solve for required head given flow and open perimeter of casting using Weir Equation:**LOCATION: **ST-4**INPUT: $Q_{100} = 4.16 \text{ cfs}$ (From Rational Equation) $P = 5.86 \text{ ft.}$ (Open Perimeter of Casting)

Type R, grate

Required Head at Grate: $h = 0.359 \text{ ft.}$ GOVERNING EQUATION: **Weir Equation**Required Head = **0.359 ft = 4.3 inches**The 100-year elevation is $1002.13 + 0.359 = 1002.49$

The 100-year elevation is less than the overflow elevation of 1002.50; therefore, ponding depth is ok.



CIVIL DESIGN ADVANTAGE

3405 SE CROSSROADS DR., SUITE G GRIMES, IA 50111

PROJECT: Kum & Go 0131 JOB NO. 1811.616 Page of Pages
 SUBJECT: Storm Water Calculations DATE: 04/04/19 DESIGNED: DSH CHECKED:

INTAKE ST-5 CAPACITY CALCUALTIONS**EQUATIONS**

1. ORIFICE: $Q = 0.6 A (2gh)^{1/2}$

$$Q_{100} = C_{100} I_{100} A$$

Assume a Time of Concentration = 15 min.

WHERE - Q = flow, cfs

A = area of opening, ft²

g = gravity (32.2 ft/s²)

h = headwater from center of opening, ft

$$C_{100} = 0.98$$

$$I_{100} = 7.44 \text{ in/hr}$$

$$A = 0.34 \text{ acres}$$

$$Q_{100} = 0.70 * 7.44 * 0.47$$

$$Q_{100} = 2.48 \text{ cfs}$$

2. WEIR: $Q = 3.3 * P * h^{1.5}$

WHERE - Q = flow, cfs

P = Perimeter of grate in feet

h = headwater from center of opening, ft

CALCULATIONS**1. Solve for required head given flow and open area for casting using Orifice Equation:**

LOCATION: **ST-5**

INPUT: $Q_{100} = 2.48 \text{ cfs}$ (From Rational Equation)

$A = 1.95 \text{ sq. ft.}$ (Open Area of Casting)

Type 3B, 24" Beehive grate

Required Head at Grate: $h = 0.070 \text{ ft.}$

2. Solve for required head given flow and open perimeter of casting using Weir Equation:

LOCATION: **ST-5**

INPUT: $Q_{100} = 2.48 \text{ cfs}$ (From Rational Equation)

$P = 5.86 \text{ ft.}$ (Open Perimeter of Casting)

Type R, grate

Required Head at Grate: $h = 0.254 \text{ ft.}$

GOVERNING EQUATION: **Weir Equation**

Required Head = **0.254 ft = 3.1 inches**

The 100-year elevation is $1002.13 + 0.254 = 1002.38$

The 100-year elevation is less than the overflow elevation of 1002.50; therefore, ponding depth is ok.



CIVIL DESIGN ADVANTAGE

3405 SE CROSSROADS DR., SUITE G GRIMES, IA 50111

PROJECT: Kum & Go 0131 JOB NO. 1811.616 Page of Pages
 SUBJECT: Storm Water Calculations DATE: 04/04/19 DESIGNED: DSH CHECKED:

INTAKE ST-6 CAPACITY CALCUALTIONS**EQUATIONS**

1. ORIFICE: $Q = 0.6 A (2gh)^{1/2}$

$$Q_{100} = C_{100} I_{100} A$$

Assume a Time of Concentration = 15 min.

WHERE - Q = flow, cfs

A = area of opening, ft²

g = gravity (32.2 ft/s²)

h = headwater from center of opening, ft

$$C_{100} = 0.98$$

$$I_{100} = 7.44 \text{ in/hr}$$

$$A = 0.47 \text{ acres}$$

$$Q_{100} = 0.70 * 7.44 * 0.47$$

$$Q_{100} = 3.43 \text{ cfs}$$

2. WEIR: $Q = 3.3 * P * h^{1.5}$

WHERE - Q = flow, cfs

P = Perimeter of grate in feet

h = headwater from center of opening, ft

CALCULATIONS**1. Solve for required head given flow and open area for casting using Orifice Equation:**

LOCATION: **ST-6**

INPUT: $Q_{100} = 3.43 \text{ cfs}$ (From Rational Equation)

$A = 1.95 \text{ sq. ft.}$ (Open Area of Casting)

Type 3B, 24" Beehive grate

Required Head at Grate: $h = 0.133 \text{ ft.}$

2. Solve for required head given flow and open perimeter of casting using Weir Equation:

LOCATION: **ST-6**

INPUT: $Q_{100} = 3.43 \text{ cfs}$ (From Rational Equation)

$P = 5.86 \text{ ft.}$ (Open Perimeter of Casting)

Type R, grate

Required Head at Grate: $h = 0.315 \text{ ft.}$

GOVERNING EQUATION: **Weir Equation**

Required Head = 0.315 ft = 3.8 inches

The 100-year elevation is $1001.50 + 0.315 = 1001.82$

The 100-year elevation is less than the overflow elevation of 1002.00; therefore, ponding depth is ok.



CIVIL DESIGN ADVANTAGE

3405 SE CROSSROADS DR., SUITE G GRIMES, IA 50111

PROJECT: Kum & Go 0131 JOB NO. 1811.616 Page of Pages
 SUBJECT: Storm Water Calculations DATE: 04/04/19 DESIGNED: DSH CHECKED:

INTAKE ST-9 CAPACITY CALCUALTIONS**EQUATIONS**

1. ORIFICE: $Q = 0.6 A (2gh)^{1/2}$

$$Q_{100} = C_{100} I_{100} A$$

Assume a Time of Concentration = 15 min.

WHERE - Q = flow, cfs

A = area of opening, ft²

g = gravity (32.2 ft/s²)

h = headwater from center of opening, ft

$$C_{100} = 0.98$$

$$I_{100} = 7.44 \text{ in/hr}$$

$$A = 0.23 \text{ acres}$$

$$Q_{100} = 0.70 * 7.44 * 0.47$$

$$Q_{100} = 1.68 \text{ cfs}$$

2. WEIR: $Q = 3.3 * P * h^{1.5}$

WHERE - Q = flow, cfs

P = Perimeter of grate in feet

h = headwater from center of opening, ft

CALCULATIONS**1. Solve for required head given flow and open area for casting using Orifice Equation:**

LOCATION: **ST-9**

INPUT: $Q_{100} = 1.68$ cfs (From Rational Equation)

$A = 1.95$ sq. ft. (Open Area of Casting)

Type R, grate

Required Head at Grate: $h = 0.032$ ft.

2. Solve for required head given flow and open perimeter of casting using Weir Equation:

LOCATION: **ST-9**

INPUT: $Q_{100} = 1.68$ cfs (From Rational Equation)

$P = 5.86$ ft. (Open Perimeter of Casting)

Type 3B, 24" Beehive grate

Required Head at Grate: $h = 0.196$ ft.

GOVERNING EQUATION: **Weir Equation**

Required Head = **0.196** ft = **2.4** inches

The 100-year elevation is $1002.38 + 0.196 = 1002.58$

The 100-year elevation is less than the overflow elevation of 1002.58; therefore, ponding depth is ok.



CIVIL DESIGN ADVANTAGE

3405 SE Crossroads Dr., SUITE G GRIMES, IA 50111

PROJECT: Kum & Go 0131 JOB NO. 1811.616 Page ____ of ____ Pages

SUBJECT: Stormwater Calculations DATE: 04/03/19 COMP. BY: DSH OK'D BY: RAH

Culvert Design

Crossing Data - Pipe L-2

Crossing Properties
Name: Pipe L-2

Parameter	Value	Units
DISCHARGE DATA		
Discharge Method	Residuals	
Discharge Rate	Define...	
TAILWATER DATA		
Channel Type	Rectangular Channel	
Bottom Width	5.000	ft
Channel Slope	0.6800	ft/ft
Manning's n (channel)	0.030	
Channel Inlet Elevation	995.430	ft
Rising Curve	view	
ROADWAY DATA		
Roadway Profile Shape	Constant Roadway Elevation	
First Roadway Station	0.000	ft
Crest Length	15.000	ft
Crest Elevation	1002.583	ft
Roadway Surface	Paved	
Top Width	41.000	ft

Culvert Properties

Culvert 1

Add Culvert
Duplicate Culvert
Delete Culvert

Parameter	Value	Units
CULVERT DATA		
Name	Culvert 1	
Shape	Circular	
Material	Concrete	
Diameter	2.000	ft
Reinforcement Depth	0.000	ft
Manning's n	0.012	
Culvert Type	Straight	
Inlet Configuration	Square Edge with headwall	
Inlet Depression	No	
SITE DATA		
Site Data Input Option	Culvert Invert Data	
Inlet Station	0.000	ft
Inlet Elevation	996.000	ft
Outlet Station	113.000	ft
Outlet Elevation	995.350	ft

Help Click on any icon for help on a specific tool Low Flow ACP Energy Dissipation Analyze Crossing OK Cancel

Culvert Summary Table - Culvert 1

Discharge Name	Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
10 year	3.70	3.70	996.93	0.93	0.46	1-52n	0.59	0.67	0.59	0.09	4.63	6.09
100 year	8.56	8.56	997.54	1.54	0.70	1-52n	0.93	1.04	0.93	0.15	5.80	11.21

Display
☐ Crossing Summary Table
☒ Culvert Summary Table
☐ Water Surface Profiles
☐ Tapered Inlet Table
☐ Customized Table

Geometry
Inlet Elevation: 996.00 ft
Outlet Elevation: 995.35 ft
Culvert Length: 113.00 ft
Culvert Slope: 0.0058
Inlet Control: 0.00 ft
Inlet Threshold: 0.00 ft

Outlet Control: Profiles

Plot
Crossing Summary Curve
Culvert Performance Curve
Water Surface Profile
Water Surface Profile (Long)

Help Flow Types Edit Input Data Energy Dissipation ACP Low Flow Export Report Adobe PDF (*.pdf) Close

Table 2B-4.01: Runoff Coefficients for the Rational Method

Cover Type and Hydrologic Condition	Runoff Coefficients for Hydrologic Soil Group											
	A			B			C			D		
	5	10	100	5	10	100	5	10	100	5	10	100
Open Space (lawns, parks, golf courses, cemeteries, etc.)												
Poor condition (grass cover < 50%)	.25	.30	.50	.45	.55	.65	.65	.70	.80	.70	.75	.85
Fair condition (grass cover 50% to 75%)	.10	.10	.15	.25	.30	.50	.45	.55	.65	.60	.65	.75
Good condition (grass cover > 75%)	.05	.05	.10	.15	.20	.35	.35	.40	.55	.50	.55	.65
Impervious Areas												
Parking lots, roofs, driveways, etc. (excluding ROW)	.95	.95	.98	.95	.95	.98	.95	.95	.98	.95	.95	.98
Streets and roads:												
Paved; curbs & storm sewers (excluding ROW)	.95	.95	.98	.95	.95	.98	.95	.95	.98	.95	.95	.98
Paved; open ditches (including ROW)	---	---	---	.70	.75	.85	.80	.85	.90	.80	.85	.90
Gravel (including ROW)	---	---	---	.60	.65	.75	.70	.75	.85	.75	.80	.85
Dirt (including ROW)	---	---	---	.55	.60	.70	.65	.70	.80	.70	.75	.85
Urban Districts (excluding ROW)												
Commercial and business (85% impervious)	---	---	---	---	---	---	.85	.85	.90	.90	.90	.95
Industrial (72% impervious)	---	---	---	---	---	---	.80	.80	.85	.80	.85	.90
Residential Districts by Average Lot Size (excluding ROW)¹												
1/8 acre (36% impervious)	---	---	---	---	---	---	.55	.60	.70	.65	.70	.75
1/4 acre (36% impervious)	---	---	---	---	---	---	.55	.60	.70	.65	.70	.75
1/3 acre (33% impervious)	---	---	---	---	---	---	.55	.60	.70	.65	.70	.75
1/2 acre (20% impervious)	---	---	---	---	---	---	.45	.50	.65	.60	.65	.70
1 acre (11% impervious)	---	---	---	---	---	---	.40	.45	.60	.55	.60	.65
2 acres (11% impervious)	---	---	---	---	---	---	.40	.45	.60	.55	.60	.65
Newly Graded Areas (pervious areas only, no vegetation)												
Agricultural and Undeveloped												
Meadow - protected from grazing (pre-settlement)	.10	.10	.25	.10	.15	.30	.30	.35	.55	.45	.50	.65
Straight Row Crops												
Straight Row (SR)	Poor Condition	.33	.39	.55	.52	.58	.71	.70	.74	.84	.78	.89
	Good Condition	.24	.30	.46	.45	.51	.66	.62	.67	.78	.73	.86
SR + Crop Residue (CR)	Poor Condition	.31	.37	.54	.50	.56	.70	.67	.72	.82	.75	.87
	Good Condition	.19	.25	.41	.38	.45	.61	.55	.60	.73	.62	.78
Contoured (C)	Poor Condition	.29	.35	.52	.47	.53	.70	.60	.65	.77	.70	.84
	Good Condition	.21	.26	.43	.38	.45	.61	.55	.60	.73	.65	.80
C+CR	Poor Condition	.27	.33	.50	.45	.51	.66	.57	.63	.75	.67	.82
	Good Condition	.19	.25	.41	.36	.43	.59	.52	.58	.71	.62	.78
Contoured & Terraced (C&T)	Poor Condition	.22	.28	.45	.36	.43	.59	.50	.56	.70	.55	.73
	Good Condition	.16	.22	.38	.31	.37	.54	.45	.51	.66	.52	.71
C&T + CR	Poor Condition	.13	.19	.35	.31	.37	.54	.45	.51	.66	.52	.71
	Good Condition	.10	.16	.32	.27	.33	.50	.43	.49	.65	.50	.70

¹ The average percent impervious area shown was used to develop composite coefficients.

Note: Rational coefficients were derived from SCS CN method

- b. **Composite Runoff Analysis:** Care should be taken not to average runoff coefficients for large segments that have multiple land uses of a wide variety (i.e., business to agriculture). However, within similar land uses, it is often desirable to develop a composite runoff coefficient based on the percentage of different types of surface in the drainage area. The composite procedure can be applied to an entire drainage area, or to typical sample blocks as a guide to selection of reasonable values of the coefficient for an entire area.

Table 2B-4.03: Runoff Curve Numbers for Urban Areas¹

Cover Type and Hydrologic Condition	Average Percent Impervious Area ²	CN's for Hydrologic Soil Group			
		A	B	C	D
Fully Developed Urban Areas (vegetation established)					
Open space (lawns, parks, golf courses, cemeteries, etc.): ³					
Poor condition (grass cover < 50%)	-----	68	79	86	89
Fair condition (grass cover 50% to 75%)	-----	49	69	79	84
Good condition (grass cover > 75%)	-----	39	61	74	80
Impervious areas:					
Paved parking lots, roofs, driveways, etc. (excluding right-of-way)	-----	98	98	98	98
Streets and roads:					
Paved; curbs and storm sewers (excluding right-of-way)	-----	98	98	98	98
Paved; open ditches (including right-of-way)	-----	83	89	92	93
Gravel (including right-of-way)	-----	76	85	89	91
Dirt (including right-of-way)	-----	72	82	87	89
Urban districts:					
Commercial and business	85	89	92	94	95
Industrial	72	81	88	91	93
Residential districts by average lot size:					
1/8 acre or less (town homes)	65	77	85	90	92
1/4 acre	38	61	75	83	87
1/3 acre	30	57	72	81	86
1/2 acre	25	54	70	80	85
1 acre	20	51	68	79	84
2 acres	12	46	65	77	82
Developing Urban Areas					
Newly graded areas (pervious areas only, no vegetation) ⁴	-----	77	86	91	94
Idle lands (CN's are determined using cover types similar to those in Table 2B-4.01)					

¹ Average runoff condition and $I_a=0.2S$ ² The average percent impervious area shown was used to develop the composite CN's. Other assumptions are as follows: impervious areas are directly connected to the drainage system, impervious areas have a CN of 98, and pervious areas are considered equivalent to open space in good hydrologic condition. CN's for other combinations of conditions may be computed using Figures 2B-4.01 or 2B-4.02.³ CN's shown are equivalent to those of pasture. Composite CN's may be computed for other combinations of open space cover type.⁴ Composite CN's to use for the design of temporary measures during grading and construction should be computed using Figures 2B-4.01 or 2B-4.02 based upon the degree of development (impervious area percentage) and the CN's for the newly graded pervious areas.

Source: NRCS National Engineering Handbook, Part 630, Chapter 9

Table 2B-4.04: Runoff Curve Numbers for Cultivated Agricultural Lands¹

Cover Description			CN's for Hydrologic Soil Group			
Cover Type	Treatment ²	Hydrologic Condition ³	A	B	C	D
Fallow	Bare Soil	---	77	86	91	94
	Crop residue cover (CR)	Poor	76	85	90	93
		Good	74	83	88	90
Row Crops	Straight Row (SR)	Poor	72	81	88	91
		Good	67	78	85	89
	SR + CR	Poor	71	80	87	90
		Good	64	75	82	85
	Contoured (C)	Poor	70	79	84	88
		Good	65	75	82	86
	C + CR	Poor	69	78	83	87
		Good	64	74	81	85
	Contoured & terraced (C&T)	Poor	66	74	80	82
		Good	62	71	78	81
	C&T + CR	Poor	65	73	79	81
		Good	61	70	77	80
Small Grain	Straight Row (SR)	Poor	65	76	84	88
		Good	63	75	83	87
	SR + CR	Poor	64	75	83	86
		Good	60	72	80	84
	Contoured (C)	Poor	63	74	82	85
		Good	61	73	81	84
	C + CR	Poor	62	73	81	84
		Good	60	72	80	83
	Contoured & terraced (C&T)	Poor	61	72	79	82
		Good	59	70	78	81
	C&T + CR	Poor	60	71	78	81
		Good	58	69	77	80
Close Seeded or Broadcast Legumes or Rotation Meadow	SR	Poor	66	77	85	89
		Good	58	72	81	85
	C	Poor	64	75	83	85
		Good	55	69	78	83
	C&T	Poor	63	73	80	83
		Good	51	67	76	80

¹ Average runoff condition and $I_a=0.2S$ ² Crop residue cover applies only if residue is on at least 5% of the surface throughout the year.³ Hydraulic condition is based on combination factors that affect infiltration and runoff, including (a) density and canopy of vegetative areas, (b) amount of year-round cover, (c) amount of grass or close-seeded legumes, (d) percent of residue cover on the land surface (good $\geq 20\%$), and (e) degree of surface roughness.

Poor: Factors impair infiltration and tend to increase runoff

Good: Factors encourage average and better than average infiltration and tend to decrease runoff.

Source: NRCS National Engineering Handbook, Part 630, Chapter 9



VEENSTRA & KIMM, INC.

3000 Westown Parkway • West Des Moines, Iowa 50266-1320

515-225-8000 • 515-225-7848 (FAX) • 800-241-8000 (TATS)

April 12, 2019

John Haldeman
City Administrator
City of Huxley
515 N. Main Avenue
Huxley, Iowa 50124

HUXLEY, IOWA
KUM & GO
SITE PLAN REVIEW

We have reviewed the site plan for Kum & Go located at Highway 210 and Interstate 35 and find it acceptable provided the following items are completed:

1. The detention basin berm needs to have a side slope of 4:1 or flatter in accordance with SUDAS Design Manual Section 2G-1.F.1.a. The slopes on Sheet Nos. C2.1 and C2.3 are labeled as being 3:1 (33.33%).
2. The overflow spillway on the north side of the detention basin needs to be dimensioned and spot elevations provided on Sheet No. C2.1.

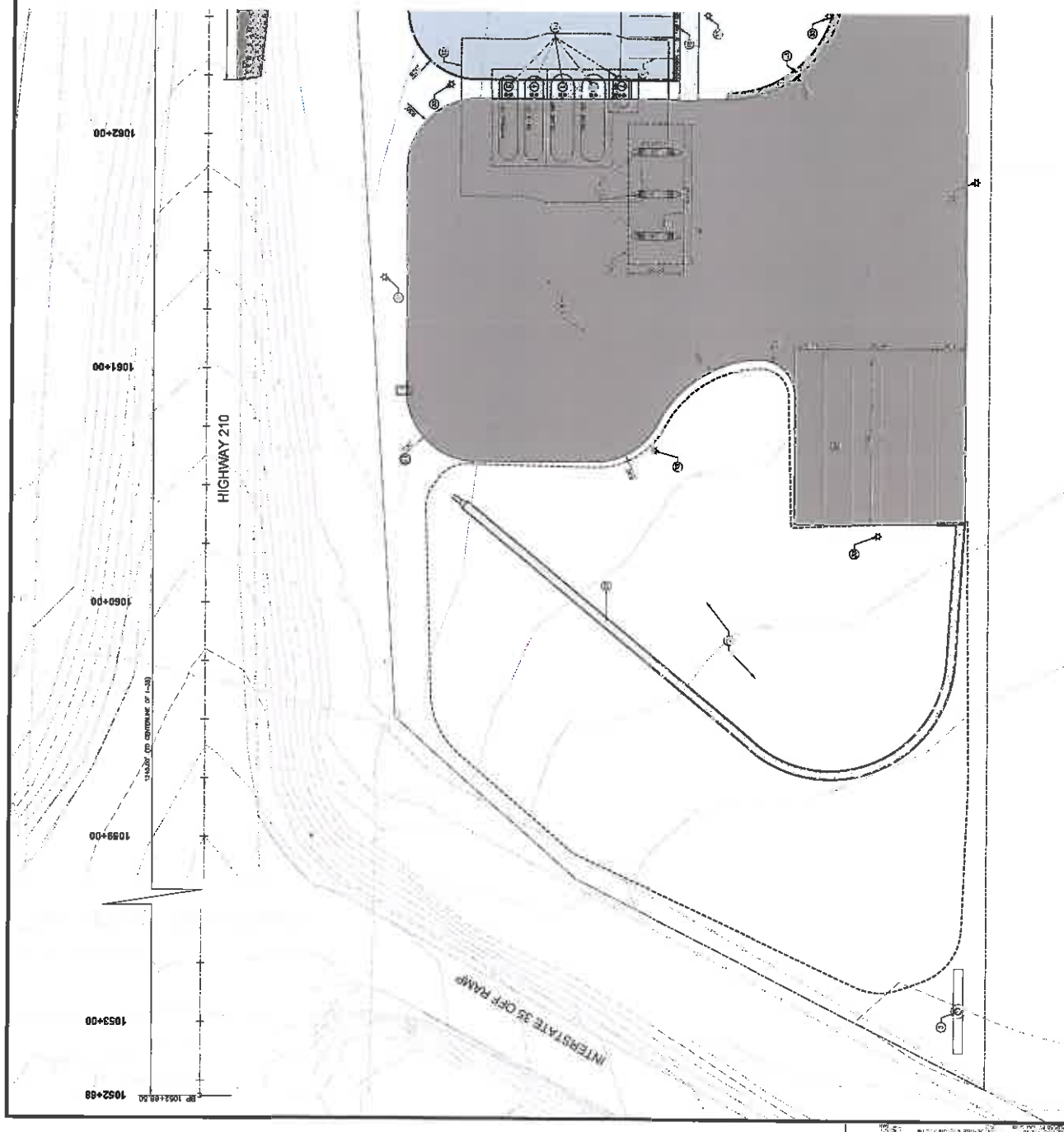
If you have any questions or comments, please contact us at 515-225-8000.

VEENSTRA & KIMM, INC.

Forrest S. Aldrich

FSA:dml
45229-037

cc: Jeff Peterson, City of Huxley (e-mail)
Britni Andreassen, Kum & Go (e-mail)
Keith Weggen, Civil Design Advantage (e-mail)



GENERAL NOTES

- 1 THE ABOVE-REPRODUCED PORTION OF THE "BIDDING INSTRUCTIONS" OF THE CITY OF
2 PITTSBURGH, PA., IS BEING REPRODUCED HEREIN FOR THE INFORMATION OF ALL CITY
3 EMPLOYEES AND ALL PERSONS INTERESTED IN THE PROJECT. THE CITY OF
4 PITTSBURGH, PA., HAS NO RESPONSIBILITY FOR THE ACCURACY OF THE REPRODUCED
5 INFORMATION. ANY PERSONS WHO WISH TO OBTAIN THE ORIGINAL DOCUMENTS SHOULD
6 CONTACT THE CITY OF PITTSBURGH, PA., AT THE ADDRESS LISTED BELOW.
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TRAFFIC CONTROL NOTES

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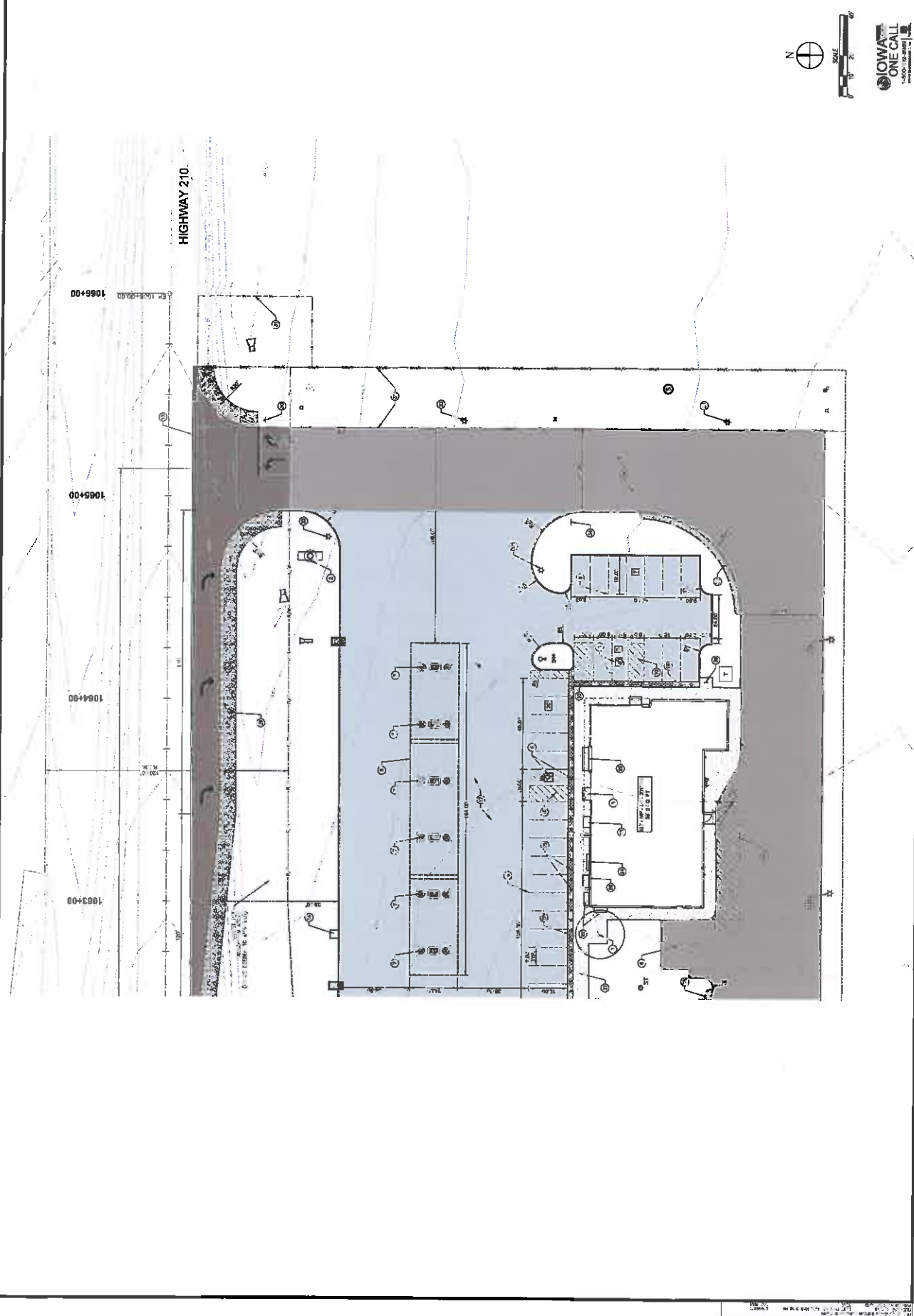
PAVEMENT THICKNESS

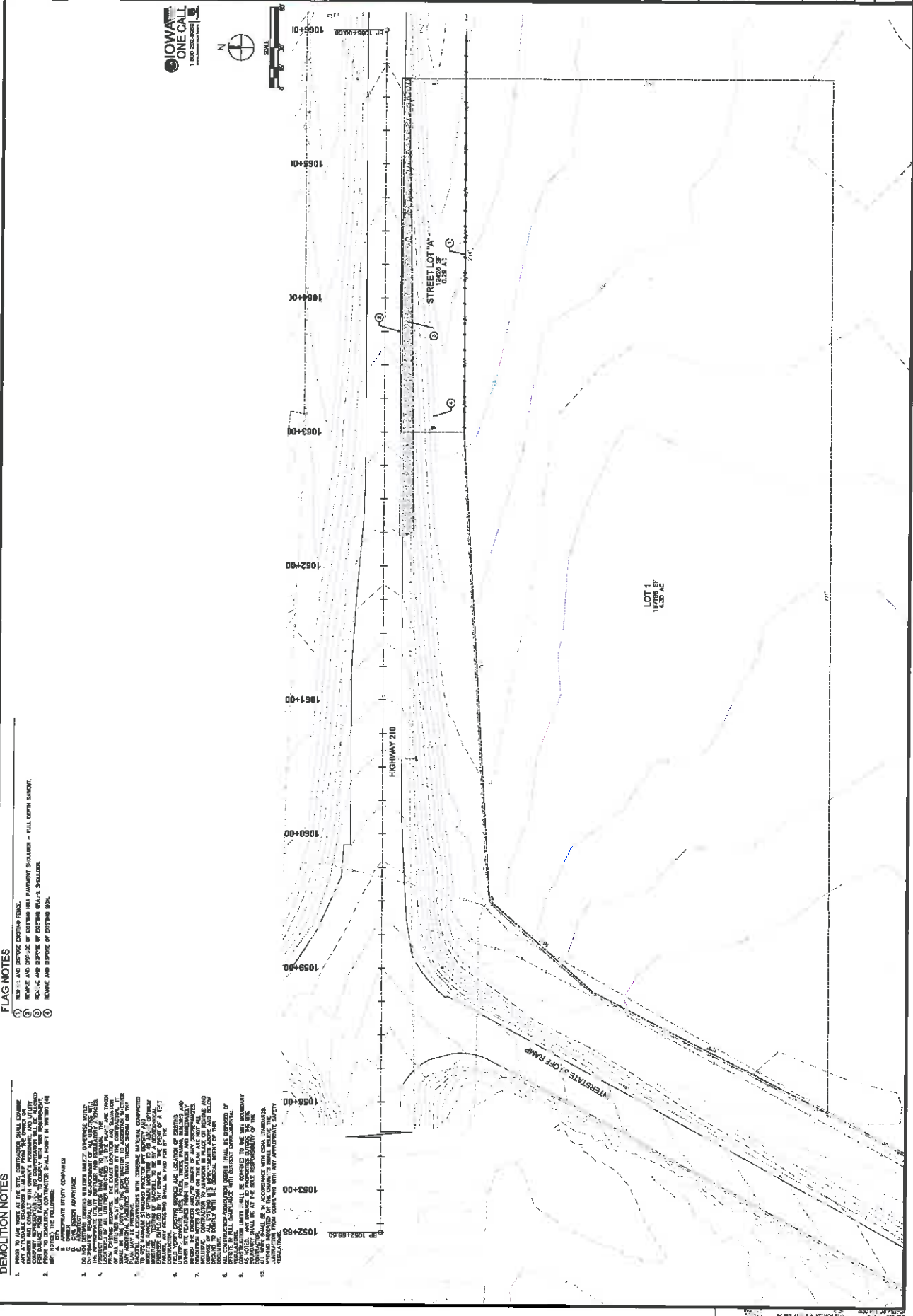
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|-------------------------------|--|--|
| SEINFALK | 4" P.C.C. | |
| STANDARD DUTY P.C.C. PAVEMENT | 6" P.C.C. | |
| HEAVY DUTY P.C.C. PAVEMENT | 8" P.C.C. | |
| R.O.G. P.C.C. PAVEMENT | 8" P.C.C. WITH 1/2" REINFORCED SURFACE | |
| STAMPED CONCRETE | 6" P.C.C. | |

FLAG NOTES

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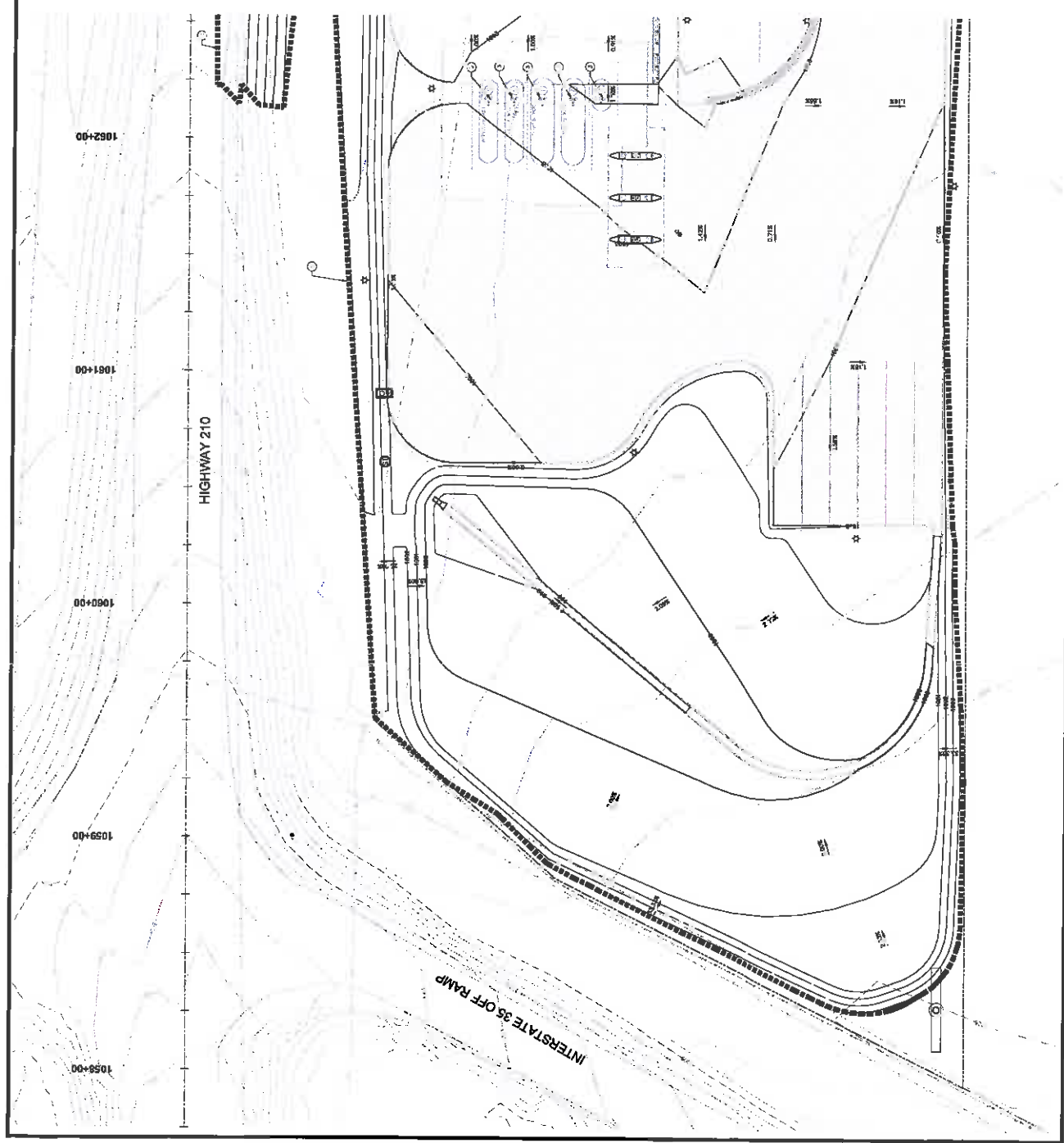
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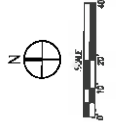




DEMOLITION NOTES

1. PRIOR TO ANY WORK AT THE SITE, CONTRACTOR SHALL EXAMINE ALL EXISTING RECORDS AND FIELD SURVEY DATA TO DETERMINE THE LOCATION AND DEPTH OF ALL EXISTING UTILITIES AND STRUCTURES. CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND FOR PROTECTING ALL UTILITIES AND STRUCTURES. CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL NECESSARY PERMITS AND FOR PROTECTING ALL UTILITIES AND STRUCTURES.
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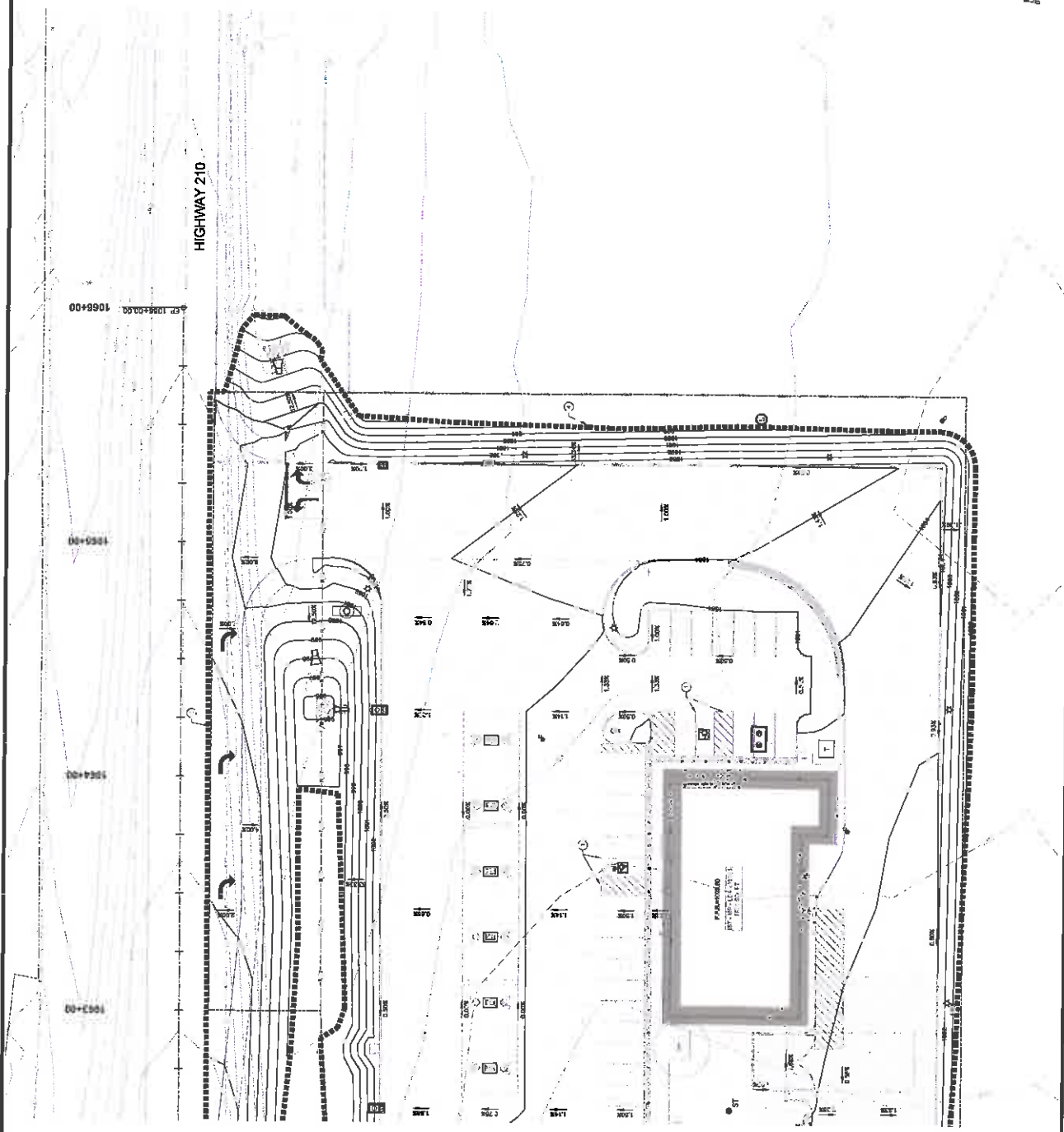


REVISIONS	
NO.	DESCRIPTION

0131 - HUXLEY, IOWA
I-35 & IA-210
GRADING PLAN



CIVIL DESIGN ADVANTAGE
3411 13th St. SE
P.O. Box 1000
Grand Rapids, MI 49501
Tel: 616-941-1111
Fax: 616-941-1112
www.civiladv.com



SWPPP LEGEND

- CONCRETE WALKOUT PIT
- UNSTURBED AREA
- GRAVEL ENTRANCE
- STAGNANT AREA
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STABILIZATION QUANTITIES

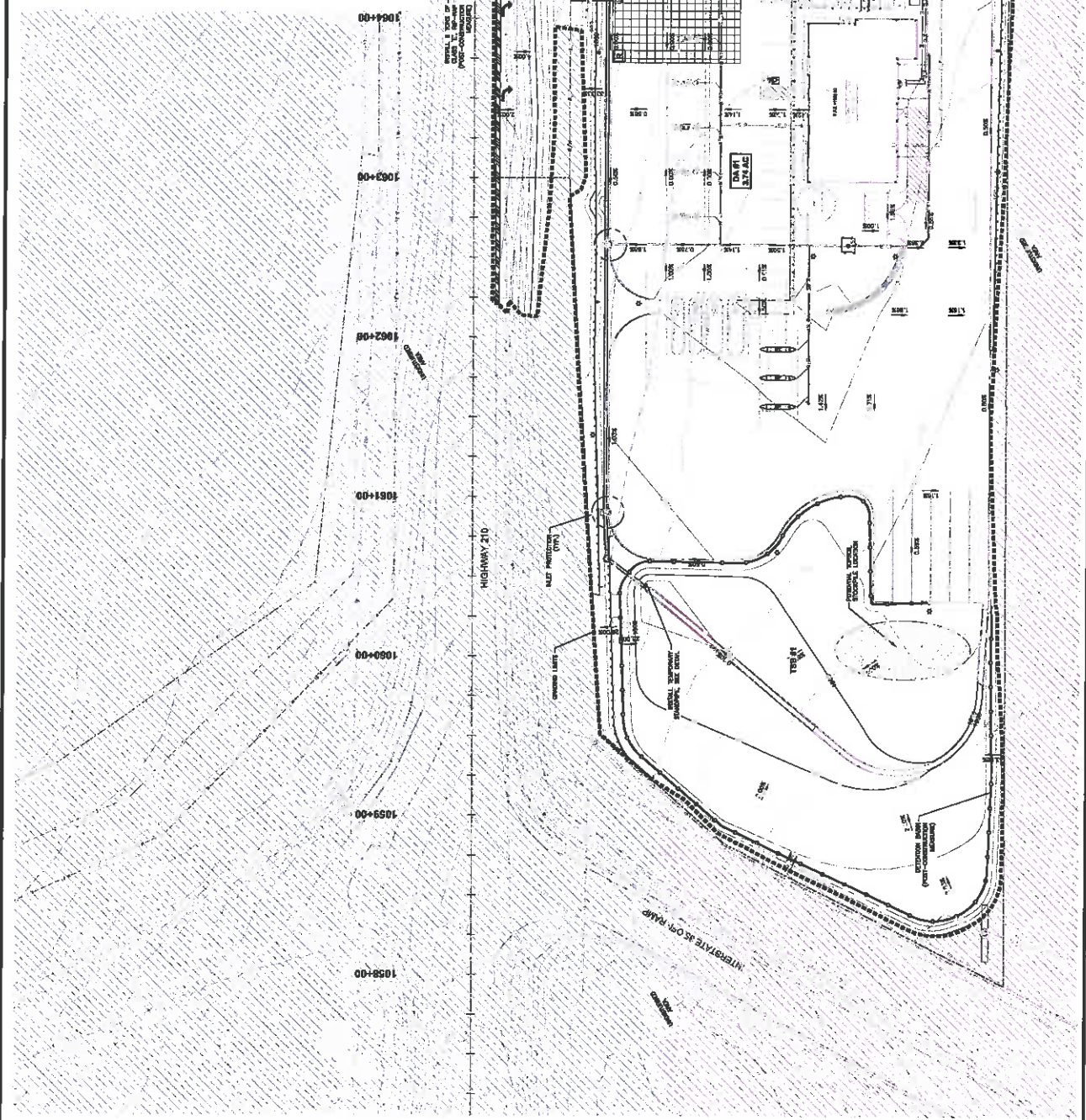
ITEM NO.	ITEM	UNIT	TOTAL
1	SEED	LB	1,200
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3	EROSION CONTROL MAT	CU YD	1.00
4	CONCRETE WALKOUT PIT	EA	1
5	GRAVEL ENTRANCE	EA	1
6	STAGNANT AREA	EA	1

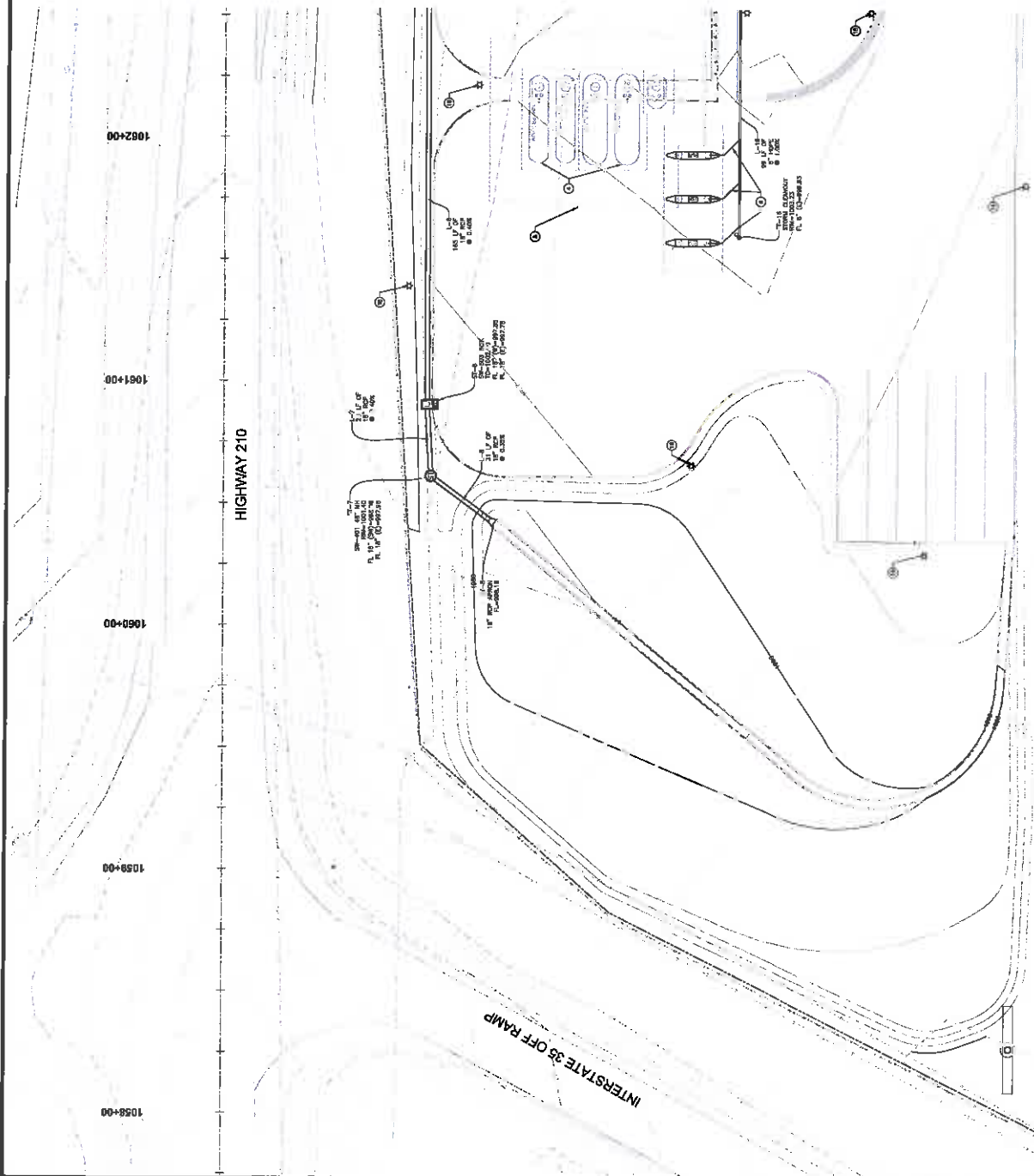
DISCHARGE POINT SUMMARY

DISCHARGE POINT: 1000+00
 STORAGE VOLUME REQUIRED (IF OF 1000+00 TO 1000+00)
 1. VOLUME PROVIDED IN FILTER PITS: 1000+00 TO 1000+00
 2. VOLUME PROVIDED IN SILT PITS: 1000+00 TO 1000+00
 TOTAL VOLUME PROVIDED: 1000+00 TO 1000+00

EROSION CONTROL NOTES

- THE EROSION CONTROL MEASURES SHOWN ON THIS PLAN SHALL BE INSTALLED AND MAINTAINED TO PREVENT THE EROSION OF THE EROSION CONTROL MEASURES. THE EROSION CONTROL MEASURES SHALL BE INSTALLED AND MAINTAINED TO PREVENT THE EROSION OF THE EROSION CONTROL MEASURES.
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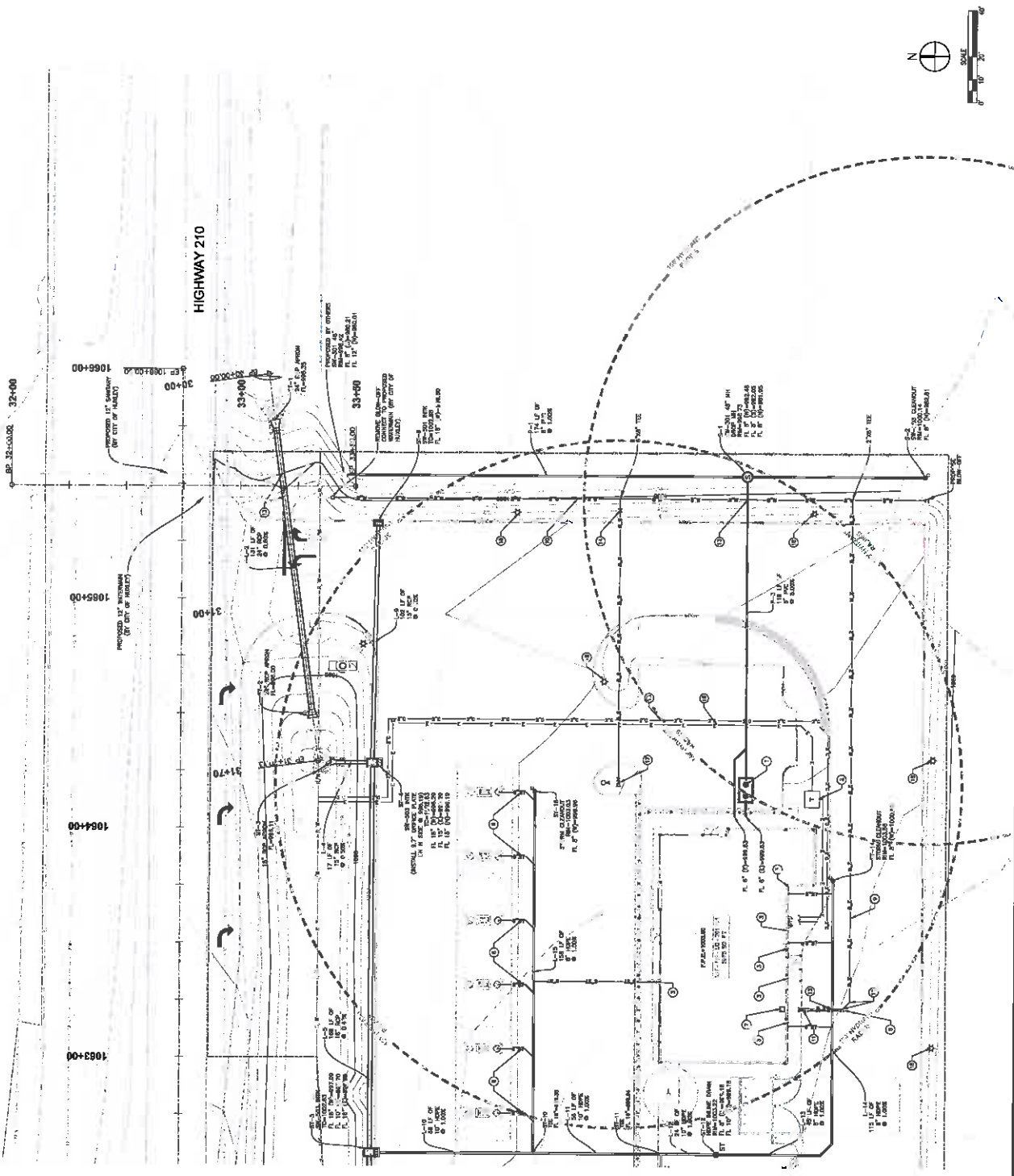


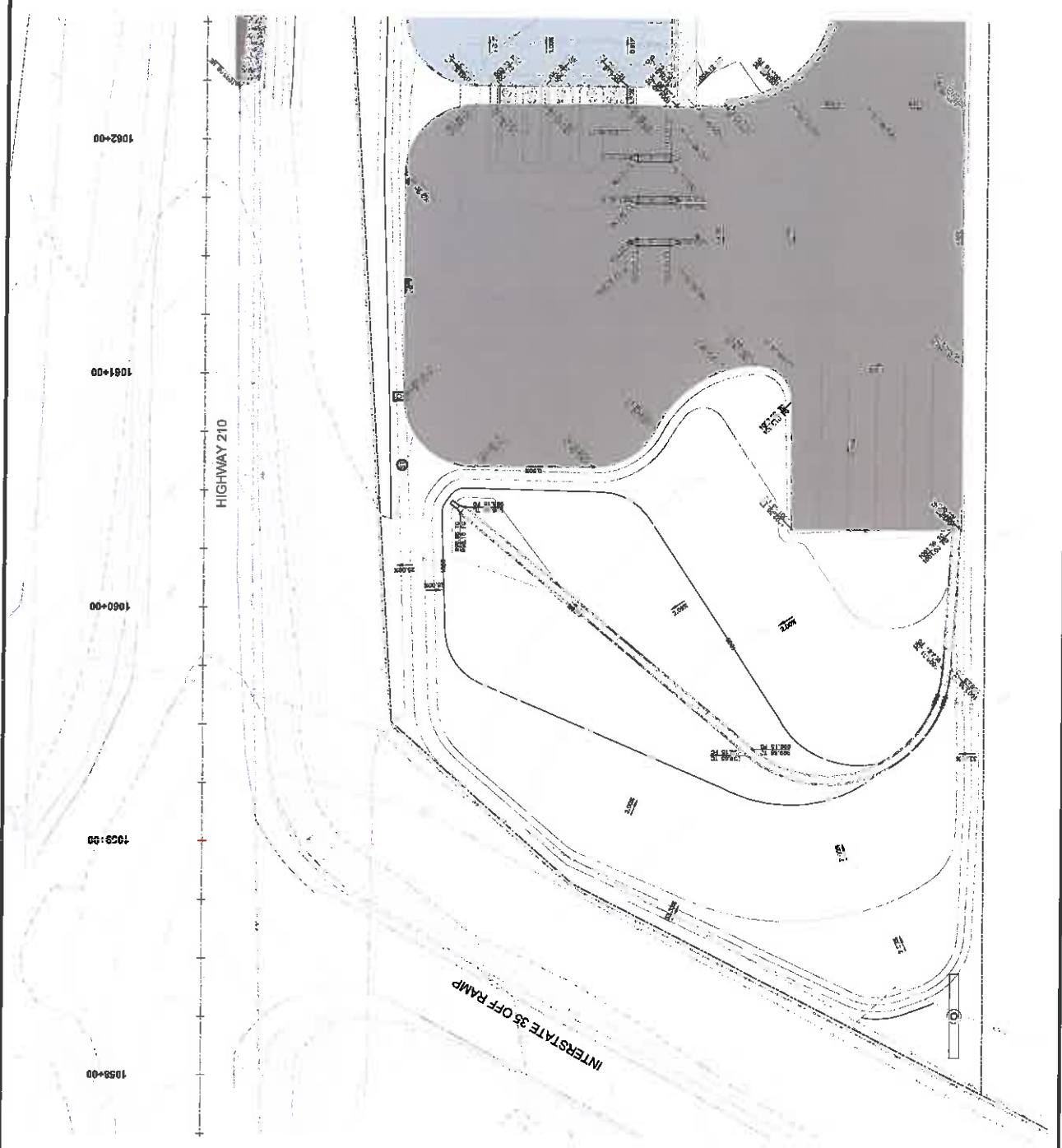
UTILITY NOTES

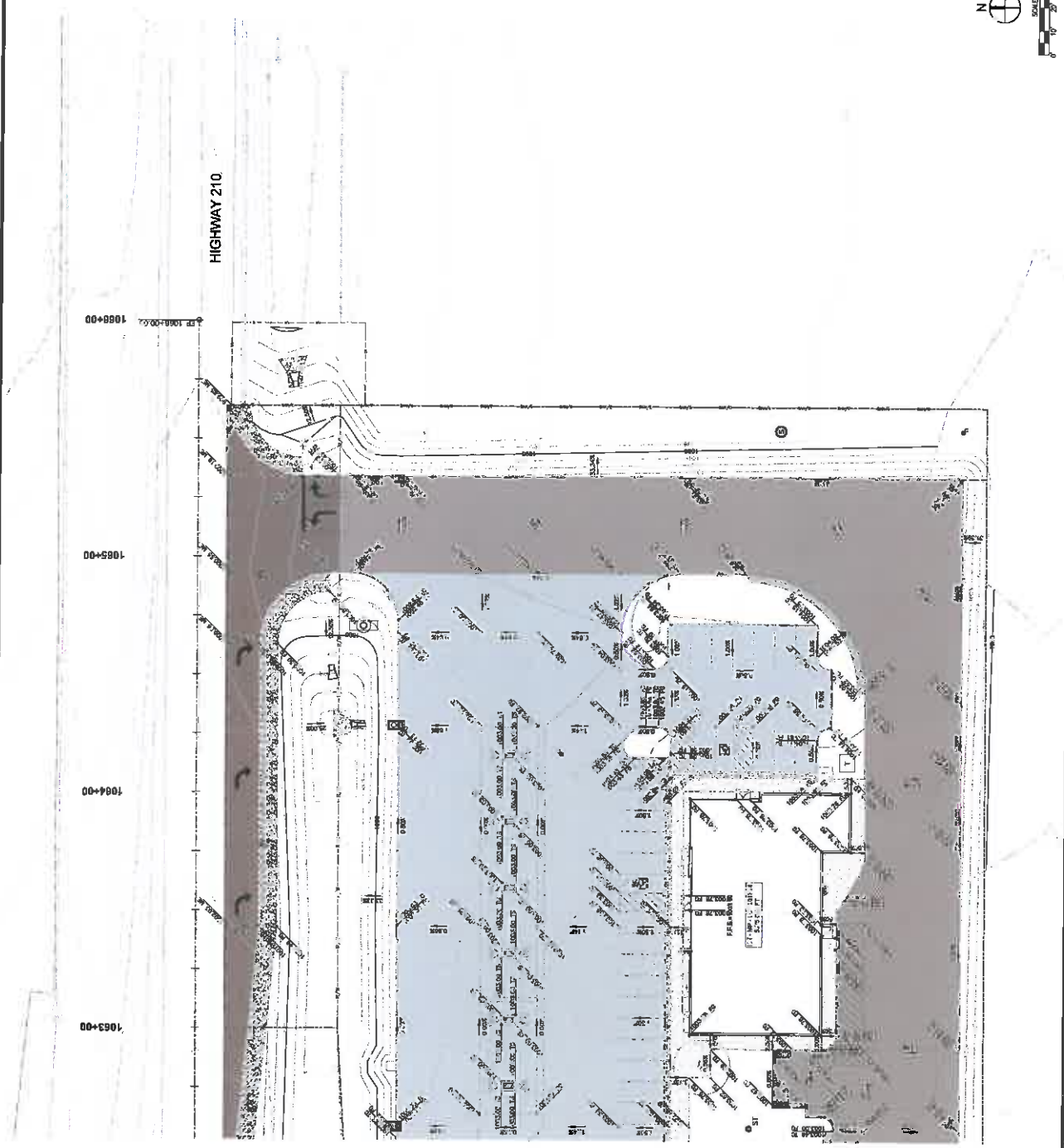
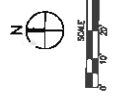
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FLAG NOTES

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LANDSCAPE NOTES

1. LOCATE ALL UTILITIES BEFORE ANY PLANTING BEGINS.
2. ALL PLANTING SHALL BE DONE IN ACCORDANCE WITH THE IOWA DEPARTMENT OF TRANSPORTATION (DOT) SPECIFICATIONS.
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OPEN SPACE

NET AREA
12,188 SF (A30 AREA)
27,433 SF (TOTAL)
15,245 SF (NET)

PLANT SCHEDULE	PLANT NAME	PLANT TYPE	PLANT SIZE	PLANT QUANTITY
1	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE
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3	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE
4	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE
5	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE
6	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE
7	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE
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9	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE
10	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE	DOUGLASS SPRUCE

